

AUTOMOTIVE INDUSTRY STANDARD

**Test Method, Testing Equipment and Related
Procedures for Type Approval and
Conformity of Production (CoP) Testing of
M & N Category Vehicles having GVW
exceeding 3500 kg for Bharat Stage VI
(BS-VI) Emission Norms as per
CMV Rules 115, 116 and 126**

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ON BEHALF OF
AUTOMOTIVE INDUSTRY STANDARDS COMMITTEE

UNDER
CENTRAL MOTOR VEHICLE RULES – TECHNICAL STANDING COMMITTEE

SET-UP BY
MINISTRY OF ROAD TRANSPORT & HIGHWAYS
(DEPARTMENT OF ROAD TRANSPORT & HIGHWAYS)
GOVERNMENT OF INDIA

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INTRODUCTION

In India, the mass emission norms based on Indian Driving Cycle (IDC) were notified under CMVR in 1989. The first mass emission norms for vehicles were enforced from 1st April 1991 for Gasoline vehicles and from 1st April 1992 for Diesel vehicles. Since then, progressively emission norms have been tightened.

Government of India has notified migration to Bharat Stage VI (BS VI) emissions norms for 2, 3 and 4 wheeled vehicles from 1st April 2020. For Agricultural Tractors, Construction Equipment Vehicles and Combine Harvesters (vehicles having power exceeding 37 kW) next stage emission norms Bharat Stage (CEV/TREM) – IV) are notified from 1st October 2020 and Bharat Stage (CEV/TREM) – V) from 1st April 2024. Test procedure for Type Approval and COP for above emission norms shall be as per various Parts of AIS-137, as applicable.

This Part 4 of AIS-137 prescribes Test Method, Testing Equipment and Related Procedures for Type Approval and Conformity of Production (Cop) Testing of M & N Category Vehicles having GVW exceeding 3500 kg for Bharat Stage VI (BS-VI) Emission Norms as per CMV Rules 115, 116 and 126.

While preparing this standard, considerable assistance has been taken from following regulations/documents:

UN Regulation 49 (Supplement 3 to the 06 series of Amendment date of Entry into Force 20.01.2016) Uniform provisions concerning the measures to be taken against the emission of gaseous and particulate pollutants from compression-ignition engines and positive ignition engines for use in vehicles

The Committee Composition for formulation of this standard is given in Annexure 1. AISC composition is given in Annexure 2.

After approval of the standard by SCOE, The Automotive Research Association of India, (ARAI), Pune, being the Secretariat of the AIS Committee, has published this standard. For better dissemination of this information ARAI may publish this standard on their web site.

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CHAPTER 1

OVERALL REQUIREMENTS

1.0 SCOPE

- 1.1 This Part of AIS-137 standard applies to the engines fitted in all M and N Category vehicles with GVW above 3,500 kg for Bharat Stage VI.
 - 1.1.1 This Part of AIS-137 applies to the control of gaseous and particulate pollutants, useful life of emission control devices, Off-cycle emissions (OCE), In-Service emission measurement, and on-board diagnostic (OBD) systems of all motor vehicles equipped with compression-ignition engines and /or positive-ignition engines fuelled with natural gas or LPG or any other alternate fuel or combination of fuels thereof approved through gazette notification for automotive use with the exception of those vehicles of category M1, with a technically permissible maximum laden mass less than or equal to 3,500 kg and of compression-ignition engines of those vehicles of category N1, N2 and M2 and of positive-ignition engines fuelled with natural gas or LPG of those vehicles of category N1 for which type-approval has been granted under AIS-137 (Part 3).
- 1.2 If a vehicle is tested for type approval on Chassis Dynamometer having reference mass up to 2,610 kg, manufacturer may seek type approval extensions up to reference mass of 2,840 kg for its variants exceeding GVW of 3,500 kg. In such cases mass emission testing on Engine Dynamometer shall not be required.
- 1.3 This Part should be read in conjunction with applicable Gazette Notification for which the engines is subjected to test.

1.4 APPLICABILITY

The applicability of AIS-137 (Part 3) and AIS-137 (Part 4) for various vehicle categories using different fuels covered in this Part is summarized in the Table 1 below:

Table 1 Test Applicability					
Vehicle category	Positive - ignition engines			Compression - ignition engines	
	Petrol	NG ^a	LPG ^b	Diesel	Ethanol
M1	AIS-137 (Part 4) or AIS-137 (Part 3) ^c	AIS-137 (Part 4) or AIS-137 (Part 3) ^c	AIS-137 (Part 4) or AIS-137 (Part 3) ^c	AIS-137 (Part 4) or AIS-137 (Part 3) ^c	AIS-137 (Part 4) or AIS-137 (Part 3) ^c
M2	AIS-137 (Part 4) or AIS-137 (Part 3) ^c	AIS-137 (Part 4) or AIS-137 (Part 3) ^c	AIS-137 (Part 4) or AIS-137 (Part 3) ^c	AIS-137 (Part 4) or AIS-137 (Part 3) ^c	AIS-137 (Part 4) or AIS-137 (Part 3) ^c
M3	AIS-137 (Part 4)	AIS-137 (Part 4)	AIS-137 (Part 4)	AIS-137 (Part 4)	AIS-137 (Part 4)
N1	AIS-137 (Part 4) or AIS-137 (Part 3) ^c	AIS-137 (Part 4) or AIS-137 (Part 3) ^c	AIS-137 (Part 4) or AIS-137 (Part 3) ^c	AIS-137 (Part 4) or AIS-137 (Part 3) ^c	AIS-137 (Part 4) or AIS-137 (Part 3) ^c
N2	AIS-137 (Part 4) or AIS-137 (Part 3) ^c	AIS-137 (Part 4) or AIS-137 (Part 3) ^c	AIS-137 (Part 4) or AIS-137 (Part 3) ^c	AIS-137 (Part 4) or AIS-137 (Part 3) ^c	AIS-137 (Part 4) or AIS-137 (Part 3) ^c
N3	AIS-137 (Part 4)	AIS-137 (Part 4)	AIS-137 (Part 4)	AIS-137 (Part 4)	AIS-137 (Part 4)
^a Natural Gas. ^b Liquefied Petroleum Gas. ^c AIS-137 (Part 3) applies for vehicles with a reference mass $\leq 2,610$ kg and by extension of an approval for vehicles with a reference mass $\leq 2,840$ kg					

1.5 TEST APPLICABILITY

Applicability of test requirements for engine type approval and post-type approval are given in the Table 2 below, as specified in Gazette Notification GSR-889(E) dated 16th September 2016 published by Ministry of Road Transport and Highways (MoRTH).

Table 2
Test Requirements of BSVI Emission Norms

	Positive-Ignition Engines					Compression-Ignition Engine			Dual Fuel
	Gasoline (E5)	CNG/Bio-methane/Biogas/LNG	LPG	E85	HCNG (Hydrogen + CNG)	Diesel (B7)	Ethanol (ED95)	Bio - Diesel (B100) ⁽¹⁾	Diesel +CNG/ LNG
Gaseous pollutants	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes ⁽²⁾
Particulate Mass	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes ⁽²⁾
PM Number	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes ⁽²⁾
Durability	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes ⁽²⁾
OBD	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes ⁽²⁾
Off-Cycle Emissions (WNET)	---	--	---	--	--	Yes	Yes	Yes	Yes ⁽²⁾
PEMS Demonstration at Type Approval	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes ⁽²⁾
In Service Conformity	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes ⁽²⁾

Notes:

- (1) The vehicle /engines fuelled with bio diesel blends up to 7% shall be tested with reference diesel (B7) and vehicles fuelled with Bio diesel above 7% will be tested with respective blends.
- (2) The test applicability requirements for dual fuel engine depends on the Gas Energy Ratio (GER) measured over the hot part of the WHTC test cycle. GER Classification shall be as defined in Chapter -14 of this Part and as amended from time to time by Govt. of India.

2.0 DEFINITIONS

For the purposes of this Part the following definitions shall apply:

- 2.1 **"Ageing cycle"** means the vehicle or engine operation (speed, load, power) to be executed during the service accumulation period
- 2.2 **"Approval of an engine (engine family)"** means the approval of an engine type (engine family) with regard to the level of the emission of gaseous and particulate pollutants, smoke and the on-board diagnostic (OBD) system.
- 2.3 **"Approval of a vehicle"** means the approval of vehicle type with regard to the level of the emission of gaseous and particulate pollutants and smoke by its engine as well as the on-board diagnostic (OBD) system and the engine installation on the vehicle.
- 2.4 **"Auxiliary Emission Strategy" (AES)** means an emission strategy that becomes active and replaces or modifies a base emission strategy for a specific purpose and in response to a specific set of ambient and/or operating conditions and only remains operational as long as those conditions exist.
- 2.5 **"Base Emission Strategy" (BES)** means an emission strategy that is active throughout the speed and load operating range of the engine unless an AES is activated.
- 2.6 **"Continuous regeneration"** means the regeneration process of an exhaust after-treatment system that occurs either permanently or at least once per World Harmonised Transient Driving Cycle (WHTC) hot start test.
- 2.7 **"Crankcase"** means the spaces in, or external to, an engine which are connected to the oil sump by internal or external ducts through which gases and vapours can be emitted.
- 2.8 **"Critical emission-related components"** means the following components which are designed primarily for emission control: any exhaust after treatment system, the ECU and its associated sensors and actuators, and the exhaust gas recirculation (EGR) system including all related filters, coolers, control valves and tubing.
- 2.9 **"Critical emission-related maintenance"** means the maintenance to be performed on critical emission-related components.
- 2.10 **"Defeat strategy"** means an emission strategy that does not meet the performance requirements for a base and/or auxiliary emission strategy as specified in this Chapter.
- 2.11 **"deNOx system"** means an exhaust after-treatment system designed to reduce emissions of oxides of nitrogen (NOx) (e.g. passive and active lean NOx catalysts, NOx absorbers and selective catalytic reduction (SCR) systems).

- 2.12 **"Diagnostic trouble code"** (DTC) means a numeric or alphanumeric identifier which identifies or labels a malfunction;
- 2.13 **"Diesel Mode"** means the normal operating mode of a dual-fuel engine during which the engine does not use any gaseous fuel for any engine operating condition.
- 2.14 **"Driving cycle"** means a sequence consisting of an engine start, an operating period (of the vehicle), an engine shut-off, and the time until the next engine start
- 2.15 **"Dual-fuel engine"** means an engine system that is designed to simultaneously operate with diesel fuel and a gaseous fuel, both fuels being metered separately, where the consumed amount of one of the fuels relative to the other one may vary depending on the operation.
- 2.16 **"Dual-fuel mode"** means the normal operating mode of a dual-fuel engine during which the engine simultaneously uses diesel fuel and a gaseous fuel at some engine operating conditions.
- 2.17 **"Dual-fuel vehicle"** means a vehicle that is powered by a dual-fuel engine and that supplies the fuels used by the engine from separate on-board storage systems.
- 2.18 **"Element of design"** means in respect of a vehicle or engine:
- (a) Any element of the engine system;
 - (b) Any control system, including: computer software; electronic control systems; and computer logic;
 - (c) Any control system calibration; or
 - (d) The results of any interaction of systems
- 2.19 **"Emission control monitoring system"** means the system that ensures correct operation of the NO_x control measures implemented in the engine system according to the requirements of clause 5.5 of this Chapter.
- "Emission control system"** means the elements of design and emission strategies developed or calibrated for the purpose of controlling emissions.
- 2.20 **"Emission related maintenance"** means the maintenance which substantially affects emissions or which is likely to affect emissions deterioration of the vehicle or the engine during normal in-use operation.
- 2.21 **"Emission strategy"** means an element or set of elements of design that is incorporated into the overall design of an engine system or vehicle and used in controlling emissions.
- 2.22 **"Engine after-treatment system family"** means a manufacturer's grouping of engines that comply with the definition of engine family, but which are further grouped into engines utilising a similar exhaust after-treatment system.

- 2.23 **"Engine family"** means a manufacturer's grouping of engines which through their design, as defined in clause 7. of this Chapter, have similar exhaust emission characteristics.
- 2.24 **"Engine system"** means the engine, the emission control system and the communication interface (hardware and messages) between the engine system electronic control unit or units (ECU) and any other powertrain or vehicle control unit.
- 2.25 **"Engine start"** consists of the Ignition-On, cranking and start of combustion, and is completed when the engine speed reaches 150 min⁻¹ below the normal, warmed-up idle speed.
- 2.26 **"Engine type" or Engine model"** means a category of engines which do not differ in essential engine characteristics as set out in Chapter 2 of this Part.
- 2.27 **"Exhaust after-treatment system"** means a catalyst (oxidation, 3-way or another), particulate filter, deNOx system, combined deNOx particulate filter, or any other emission reducing device, that is installed downstream of the engine;
- 2.28 **Gaseous pollutants"** means the exhaust gas emissions of carbon monoxide, NOx, expressed in NO₂ equivalent, hydrocarbons (i.e. total hydrocarbons, non-methane hydrocarbons and methane).
- 2.29 **"General Denominator"** means a counter indicating the number of times a vehicle has been operated, taking into account general conditions.
- 2.30 **Group of monitors"** means, for the purpose of assessing the in-use performance of an OBD engine family, a set of OBD monitors used for determining the correct operation of the emission control system
- 2.31 **"Ignition cycle counter"** means a counter indicating the number of engine starts a vehicle has experienced.
- 2.32 **"In-Use performance ratio" (IUPR)** means the ratio of the number of times that the conditions have existed under which a monitor, or group of monitors, should have detected a malfunction relative to the number of driving cycles relevant for the operation of that monitor or group of monitors.
- 2.33 **"Low speed (n_{lo})"** means the lowest engine speed where 55 per cent of the declared maximum power occurs.
- 2.34 **"Malfunction"** means a failure or deterioration of an engine system, including the OBD system, that might reasonably be expected to lead either to an increase in any of the regulated pollutants emitted by the engine system or to a reduction in the effectiveness of the OBD system.
- 2.35 **"Malfunction indicator" (MI)** means an indicator which is part of the alert system and which clearly informs the driver of the vehicle in the event of a malfunction;

- 2.36 **"Manufacturer"** means the person or body who is responsible to the Test Agency for all aspects of the type approval or authorisation process and for ensuring conformity of production. It is not essential that the person or body be directly involved in all stages of the construction of the vehicle, system, component or separate technical unit which is the subject of the approval process;
- 2.37 **"Maximum net power"** means the maximum value of the net power measured at full engine load;
- 2.38 **"Net power"** means the power obtained on a test bench at the end of the crankshaft or its equivalent at the corresponding engine or motor speed with the auxiliaries according to AIS-137 (Part 5) and determined under reference atmospheric conditions.
- 2.39 **"Non-emission-related maintenance"** means the maintenance which does not substantially affect emissions and which does not have a lasting effect on the emissions deterioration of the vehicle or the engine during normal in-use operation once the maintenance is performed
- 2.40 **"On-board diagnostic system"** (OBD system) means a system on-board of a vehicle or engine which has the capability of:
- (a) Detecting malfunctions, affecting the emission performance of the engine system;
 - (b) Indicating their occurrence by means of an alert system.
 - (c) Identifying the likely area of the malfunction by means of information stored in computer memory and communicating that information off board.
- 2.41 **"OBD engine family"** means a manufacturer's grouping of engine systems having common methods of monitoring and diagnosing emission-related malfunctions;
- 2.42 **"Operating sequence"** means a sequence consisting of an engine start, an operating period (of the engine), an engine shut-off, and the time until the next start, where a specific OBD monitor runs to completion and a malfunction would be detected if present.
- 2.43 **"Original pollution control device"** means a pollution control device or an assembly of such devices covered by the type approval granted for the vehicle concerned.
- 2.44 **"Parent engine"** means an engine selected from an engine family in such a way that its emissions characteristics will be representative for that engine family.
- 2.45 **"Particulate after-treatment device"** means an exhaust after-treatment system designed to reduce emissions of particulate pollutants (PT) through a mechanical, aerodynamic, diffusional or inertial separation.

- 2.46 **"Particulate matter (PM)"** means any material collected on a specified filter medium after diluting exhaust with a clean filtered diluent to a temperature between 315 K (42°C) and 325 K (52°C); this is primarily carbon, condensed hydrocarbons, and sulphates with associated water;
- 2.47 **"Per cent load"** means the fraction of the maximum available torque at an engine speed;
- 2.48 **"Performance monitoring"** means malfunction monitoring, that consists of functionality checks and the monitoring of parameters that are not directly correlated to emission thresholds, and that is done on components or systems to verify that they are operating within the proper range.
- 2.49 **"Periodic regeneration"** means the regeneration process of an emission control device that occurs periodically in less than 100 hours of normal engine operation.
- 2.50 **"Portable emissions measurement system" (PEMS)** means a portable emissions measurement system meeting the requirements specified in Appendix 2 of Chapter 7 of this Part.
- 2.51 **"Power take-off unit"** means an engine driven output device for the purposes of powering auxiliary, vehicle mounted, equipment;
- 2.52 **"Qualified deteriorated component or system" (QDC)** means a component or system that has been intentionally deteriorated such as by accelerated ageing or by having been manipulated in a controlled manner and which has been accepted by the Test Agency according to the provisions set out in Chapter 8B of this Part for use when demonstrating the OBD performance of the engine system;
- 2.53 **"Reagent"** means any medium that is stored on-board the vehicle in a tank and provided to the exhaust after-treatment system (if required) upon request of the emission control system
- 2.54 **"Recalibration"** means a fine tuning of a natural gas engine in order to provide the same performance (power, fuel consumption) in a different range of natural gas
- 2.55 **"Reference mass"** means the "unladen mass" of the vehicle increased by a uniform figure of 150 kg;
- 2.56 **"Replacement pollution control device"** means a pollution control device or an assembly of such devices intended to replace an original pollution control device and which can be approved as a separate technical unit;
- 2.57 **"Scan-tool"** means external test equipment used for standardised off-board communication with the OBD system in accordance with the requirements of this Part.

- 2.58 **"Service accumulation schedule"** means the ageing cycle and the service accumulation period for determining the deterioration factors for the engine after- treatment system family;
- 2.59 **"Service mode"** means a special mode of a dual-fuel engine that is activated for the purpose of repairing, or of moving the vehicle from the traffic when operation in the dual-fuel mode is not possible ⁽¹⁾
- (1) For example in case of an empty gas tank.
- 2.60 **"Tailpipe emissions"** means the emission of gaseous and particulate pollutants.
- 2.61 **"Tampering"** means inactivation, adjustment or modification of the vehicle emissions control or propulsion system, including any software or other logical control elements of those systems, that has the effect, whether intended or not, of worsening the emissions performance of the vehicle.
- 2.62 **"Unladen mass"** "Unladen mass" means the mass of the vehicle in running order without the uniform mass of the driver of 75kg, passengers or load, but with the fuel tank 90 per cent full and the usual set of tools and spare wheel on board, where applicable;
- 2.63 **"Useful life"** means the relevant period of distance and/or time over which compliance with the relevant gaseous and particulate emission limits has to be assured.
- 2.64 **"Vehicle type or vehicle model with regard to emissions"** means a group of vehicles which do not differ in essential engine and vehicle characteristics as set out in Chapter 2 of this Part;
- 2.65 **"Wall flow Diesel Particulate Filter"** means a Diesel Particulate Filter ("DPF") in which all the exhaust gas is forced to flow through a wall which filters out the solid matter;
- 2.66 **"Wobbe index (lower Wl; or upper Wu)"** means the ratio of the corresponding calorific value of a gas per unit volume and the square root of its relative density under the same reference conditions:

$$W = H_{gas} \times \sqrt{\rho_{air} / \rho_{gas}}$$

- 2.67 **"λ-shift factor (Sλ)"** means an expression that describes the required flexibility of the engine management system regarding a change of the excess-air ratio λ if the engine is fuelled with a gas composition different from pure methane (see Appendix 5 of Chapter 3 of this Part for the calculation of Sλ).

3.0 APPLICATION FOR APPROVAL

3.1 Application for type approval of an engine system or engine family as a separate technical unit.

3.1.1 The manufacturer or his authorized representative shall submit to the Test Agency an application for type approval of an engine system or engine family as a separate technical unit;

3.1.2 The application referred to in clause 3.1.1. above shall have technical specifications set out in Chapter 2 of this Part.

3.1.3 Together with the application, the manufacturer shall provide a documentation package that fully explains any element of design which affects emissions, the emission control strategy of the engine system, the means by which the engine system controls the output variables which have a bearing upon emissions, whether that control is direct or indirect, and fully explains the warning and inducement system required by clauses 4 and 5 of Chapter 10 of this Part. The documentation package shall consist of the following parts including the information set out in clause 5.1.4 of this Chapter.

(a) A formal documentation package that shall be retained by the Test Agency. Formal documentation package shall be in two parts; the first part shall be the brief technical specifications as per Table 7 of the standard AIS-007 and the second part shall be the detailed technical specifications as per Table 4F of the standard AIS-007. The first part of formal documentation may be made available to the interested parties upon request. The second part of formal documentation shall be retained by the Test Agency as confidential information.

(b) An extended documentation package that shall remain confidential. The extended documentation package may be kept by the Test Agency or be retained by the manufacturer, at the discretion of the Test Agency, but shall be made available for inspection by the Test Agency at the time of approval or at any time during the validity of the approval. When the documentation package is retained by the manufacturer, the Test Agency shall take the necessary measures to ensure that the documentation is not being altered after approval.

3.1.4 In addition to the information referred to in clause 3.1.3. of this Chapter the manufacturer shall submit the following information:

(a) In the case of positive-ignition engines, a declaration by the manufacturer of the minimum percentage of misfires out of a total number of firing events that either would result in emissions exceeding the limits set out in Chapter 8A of this Part if that percentage of misfire had been present from the start of the emission test as set out in Chapter 3 of this Part or could lead to an exhaust catalyst, or catalysts, overheating prior to causing irreversible damage

- (b) A description of the provisions taken to prevent tampering with and modification of the emission control computer(s), including the facility for updating using a manufacturer-approved programme or calibration;
 - (c) Documentation of the OBD system, in accordance with the requirements set out in clause 8. of Chapter 8B of this Part;
 - (d) OBD related information for the purpose of access to OBD, in accordance with the requirements of Chapter 13 of this Part.
 - (e) A Statement of off-cycle emission compliance, with the requirements of clause 5.1.3. and clause 10. of Chapter 9 of this Part;
 - (f) A Statement of OBD in-use performance compliance, with the requirements of Appendix 2 of Chapter 8A of this Part;
 - (g) The initial plan for in-service testing according to clause 2.4. of Chapter 7 of this Part;
 - (h) Where appropriate, copies of other type approvals with the relevant data to enable extension of approvals and establishment of deterioration factors.
 - (i) Where appropriate, the documentation packages required by this Part for the correct installation of the engine type-approved as separate technical unit
- 3.1.5 The manufacturer shall submit to the Test Agency for the type approval tests an engine or, as appropriate, a parent engine representative of the type to be approved.
- 3.1.6 Changes to the make of a system, component or separate technical unit that occur after a type approval shall not automatically invalidate a type approval, unless its original characteristics or technical parameters are changed in such a way that the functionality of the engine or pollution control system is affected.
- 3.2 Application for type approval of a vehicle with an approved engine system with regard to emissions.**
- 3.2.1 The manufacturer or his authorized representative shall submit to the Test Agency an application for type approval of a vehicle with an approved engine system with regard to emissions.
- 3.2.2 The application referred to in clause 3.2.1. above shall have technical specifications set out in Chapter 2 of this Part. This application shall be accompanied by a copy of the type approval certificate for the engine system or engine family as a separate technical unit.
- 3.2.3 The manufacturer shall provide a documentation package that fully explains the elements of the warning and inducement system that is on board of the vehicle and required by Chapter 10 of this Part. This documentation package shall be provided in accordance with clause 3.1.3 of this Chapter.

- 3.2.4 In addition to the information referred to in clause 3.2.3. of this Chapter, the manufacturer shall submit the following information:
- (a) A description of the measures taken to prevent tampering with and modification of the vehicle control units covered by this Part, including the facility for updating using a manufacturer-approved programme or calibration;
 - (b) A description of the OBD components on board of the vehicle, in accordance with the requirements of clause 8. of Chapter 8B of this Part;
 - (c) Information related to the OBD components on board of the vehicle for the purpose of access to OBD;
 - (d) Where appropriate, copies of other type approvals with the relevant data to enable extension of approvals.
- 3.2.5 Changes to the make of a system, component or separate technical unit that occur after a type approval shall not automatically invalidate a type approval, unless its original characteristics or technical parameters are changed in such a way that the functionality of the engine or pollution control system is affected.
- 3.3 Application for type approval of a vehicle with regard to emissions**
- 3.3.1 The manufacturer or his authorized representative shall submit to the Test Agency an application for type approval of a vehicle with regard to emissions.
- 3.3.2 The application referred to in clause 3.3.1. above shall have technical specifications set out in Chapter 2 of this Part.
- 3.3.3 The manufacturer shall provide a documentation package that fully explains any element of design which affects emissions, the emission control strategy of the engine system, the means by which the engine system controls the output variables which have a bearing upon emissions, whether that control is direct or indirect, and fully explains the warning and inducement system required by Chapter 10 of this Part. This documentation package shall be provided in accordance with clause 3.1.3. of this Chapter.
- 3.3.4 In addition to the information referred to in clause 3.3.3. of this Chapter, the manufacturer shall submit the information required by clause 3.1.4. (a) to (h) and clause 3.2.4. (a) to (d) of this Chapter.
- 3.3.5 The manufacturer shall submit to the Test Agency responsible for the type approval tests an engine representative of the type to be approved.
- 3.3.6 Changes to the make of a system, component or separate technical unit that occur after a type approval shall not automatically invalidate a type approval, unless its original characteristics or technical parameters are changed in such a way that the functionality of the engine or pollution control system is affected.

3.4. Application for type approval of a type of replacement pollution control device as a separate technical unit.

- 3.4.1 The manufacturer shall submit to the Test Agency an application for type approval of a type of replacement pollution control device as a separate technical unit.
- 3.4.2 The application shall have technical specifications set out in Chapter 2 of this Part .
- 3.4.3 The manufacturer shall submit a Statement of compliance with the requirements on access to OBD information.
- 3.4.4 The manufacturer shall submit to the Test Agency responsible for the type approval test the following:
 - (a) An engine system or engine systems of a type approved in accordance with this Part equipped with a new original equipment pollution control device;
 - (b) One sample of the type of the replacement pollution control device;
 - (c) An additional sample of the type of the replacement pollution control device, in the case of a replacement pollution control device intended to be fitted to a vehicle equipped with an OBD system.
- 3.4.5 For the purposes of point (a) of clause 3.4.4. above, the test engines shall be selected by the applicant with the agreement of the Type. Test Agency. The test conditions shall comply with the requirements set out in clause 6. of Chapter 3 of this Part.

The test engines shall respect the following requirements

 - (a) They shall have no emission control system defects;
 - (b) Any malfunctioning or excessively worn emission-related original part shall be repaired or replaced;
 - (c) They shall be tuned properly and set to the manufacturer's specification prior to emission testing.
- 3.4.6 For the purposes of points (b) and (c) of clause 3.4.4. of this Chapter the sample shall be clearly and indelibly marked with the applicant's trade name or mark and its commercial designation.
- 3.4.7 For the purposes of point (c) of clause 3.4.4. of this Chapter, the sample shall be a qualified deteriorated component.

4.0 APPROVAL

- 4.1** In order to receive a type-approval of an engine system or engine family as a separate technical unit, or type-approval of a vehicle with an approved engine system with regard to emissions, or a type-approval of a vehicle with regard to emissions, the manufacturer shall, in accordance

with the provisions of this Part demonstrate that the vehicles or engine systems are subject to the tests and comply with the requirements set out in the gazette notification G.S.R 889 (E) dated 16.09.2016 published by Ministry of Road Transport and Highways (MoRTH). The Test Agency shall also ensure compliance with the specifications of reference fuels set out in Chapter 4 of this Part.

In order to receive type-approval of a vehicle with an approved engine system with regard to emissions or a type-approval of a vehicle with regard to emissions the manufacturer shall ensure compliance with the installation requirements set out in clause 6 of this Chapter.

4.2 In order to receive an extension of the type-approval of a vehicle with regard to emissions type approved under this Part with a reference mass exceeding 2,380 kg but not exceeding 2,610 kg the manufacturer shall meet the requirements set out in Appendix 1 of Chapter 11 of this Part.

4.3 In order to receive a type-approval of a dual-fuel engine or engine family as a separate technical unit, or type-approval of a dual-fuel vehicle with an approved dual-fuel engine with regard to emissions, or a type-approval of a dual-fuel vehicle with regard to emissions, the manufacturer shall, in addition to the requirements of clause 4.1. of this Chapter demonstrate that the dual-fuel vehicles or engine are subject to the tests and comply with the requirements set out in Chapter 14 of this Part.

4.4 **Reserved**

4.5 In order to receive a type-approval of an engine system or engine family as a separate technical unit or a type-approval of a vehicle with regard to emissions, the manufacturer shall ensure compliance with the requirements on fuel range for a universal fuel approval or in case of a positive ignition engine fuelled with natural gas and LPG a restricted fuel range approval as specified in clause 4.6 and 4.7 of this Chapter respectively.

4.5.1 Tables summarizing the requirements for approval of NG-Fuelled engines, LPG-Fuelled engines and dual-fuelled engines are provided in Appendix 2 of this Chapter.

4.6 **Requirements On Universal Fuel Range Type-Approval**

A universal fuel range approval shall be granted subject to the requirements specified in clauses 4.6.1 to 4.6.6.1.

4.6.1 The parent engine shall meet the requirements of this Part on the appropriate reference fuels specified in Chapter 4 of this Part. Specific requirements shall apply to natural gas fuelled engines, as laid down in clause 4.6.3.

- 4.6.2 If the manufacturer permits to operate the engine family to run on market fuels not included in Chapter 4 of this Part, the manufacturer shall, in addition to the requirements in clause 4.6.1:
- (a) Declare the fuels the engine family is capable to run on in Chapter 2 of this Part.
 - (b) Demonstrate the capability of the parent engine to meet the requirements of this Part on the fuels declared;
 - (c) Be liable to meet the requirements of in-service conformity specified in clause 9 of this Chapter on the fuels declared, including any blend between the declared fuels and the relevant market fuels and standards
- 4.6.3 In the case of a natural gas /biomethane fuelled engines, including dual fuel engines, the manufacturer shall demonstrate the parent engines capability to adapt to any natural gas/biomethane composition that may occur across the market. This demonstration shall be carried out according to this clause and, in case of dual-fuel engines, also according to the additional provisions regarding the fuel adaptation procedure set out in clause 6.4. of Chapter 14 of this Part.
- 4.6.3.1 In the case of compressed natural gas/biomethane there are generally two types of fuel, high calorific fuel (H-gas) and low calorific fuel (L-gas), but with a significant spread within both ranges; they differ significantly in their energy content expressed by the Wobbe Index and in their λ -shift factor ($S\lambda$). Natural gases with a λ -shift factor between 0.89 and 1.08 ($0.89 \leq S\lambda \leq 1.08$) are considered to belong to H-range, while natural gases with a λ -shift factor between 1.08 and 1.19 ($1.08 \leq S\lambda \leq 1.19$) are considered to belong to L-range. The composition of the reference fuels reflects the extreme variations of $S\lambda$.
- The parent engine shall meet the requirements of this Part on the reference fuels G_R (fuel 1) and G_{25} (fuel 2), as specified in Chapter 4 of this Part, without any readjustment to the fuelling system between the two tests (Self adaptation is required). One adaptation run over one WHTC hot cycle without measurement is permitted after the change of the fuel. After the adaptation run the engine shall be cooled down in accordance with clause 7.6.1 of Chapter 3 of this Part.
- 4.6.3.1.1 At the manufacturer's request, the engine may be tested on third fuel (fuel 3) in the λ -shift factor ($S\lambda$) lies between 0.89 (that is the lower range of G_R) and 1.19 (that is the upper range of G_{25}), for example when fuel 3 is a market fuel. The results of this test may be used as a basis for the evaluation of the conformity of the production
- 4.6.3.2 In the case of liquefied natural gas/liquefied biomethane (LNG) the parent engine shall meet the requirements of this Part on the reference fuels G_R (Fuel 1) and G_{20} (Fuel 2), as specified in Chapter 4 of this Part, without any manual readjustment to the engine fuelling system between the two tests (self-adaptation is required). One adaptation run over one WHTC hot cycle without measurement is permitted after the change of the fuel. After the adaptation run, the engine shall be cooled down in accordance with clause 7.6.1. of Chapter 3 of this Part.

- 4.6.4 In the case of an engine fuelled with compressed natural gas/biomethane (CNG) which is self-adaptive for the range of H-gases on the one hand and the range of L-gases on the other hand, and which switches between the H-range and the L-range by means of a switch, the parent engine shall be tested on the relevant reference fuel as specified in Chapter 4 of this Part for each range, at each position of the switch. The fuels are G_R (fuel 1) and G_{23} (fuel 3) for the H-range of gases and G_{25} (fuel 2) and G_{23} (fuel 3) for the L-range of gases. The parent engine shall meet the requirements of this Part at both positions of the switch without any readjustment to the fuelling between the two tests at each position of the switch. One adaptation run over one WHTC hot cycle without measurement is permitted after the change of the fuel. After the adaptation run the engine shall be cooled down in accordance with Clause 7.6.1 of Chapter 3 of this Part.
- 4.6.4.1. At the manufacturer's request the engine may be tested on a third fuel instead of G_{23} (fuel 3) if the λ -shift factor (S_λ) lies between 0.89 (that is the lower range of G_R) and 1.19 (that is the upper range of G_{25}), for example when fuel 3 is a market fuel. The results of this test may be used as a basis for the evaluation of the conformity of the production
- 4.6.5 In the case of natural gas/bio-methane engines, the ratio of the emission results 'r' shall be determined for each pollutant as follows:

$$r = \frac{\text{emission result on reference fuel 2}}{\text{emission result on reference fuel 1}}$$

Or

$$r_a = \frac{\text{emission result on reference fuel 2}}{\text{emission result on reference fuel 3}}$$

and

$$r_b = \frac{\text{emission result on reference fuel 1}}{\text{emission result on reference fuel 3}}$$

- 4.6.6 In the case of LPG, the manufacturer shall demonstrate the parent engines capability to adapt to any fuel composition that may occur across the market

In the case of LPG there are variations in C_3/C_4 composition. These variations are reflected in the reference fuels. The parent engine shall meet the emission requirements on the reference fuels A and B as specified in Chapter 4 without any readjustment to the fuelling between the two tests. One adaptation run over one WHTC hot cycle without measurement is permitted after the change of the fuel. After the adaptation run the engine shall be cooled down in accordance with Clause 7.6.1 of Chapter 3 of this Part.

- 4.6.6.1 The ratio of emission results 'r' shall be determined for each pollutant as follows

$$r = \frac{\text{emission result on reference fuel B}}{\text{emission result on reference fuel A}}$$

4.7 Requirements on restricted fuel range type-approval in case of positive-ignition engines fuelled with natural gas/biomethane or LPG including dual-fuel engines.

Restricted Fuel range type approval shall be granted subject to the requirements specified in clauses 4.7.1 to 4.7.2.3 below.

4.7.1 Exhaust emissions type-approval of an engine running on CNG and laid out for operation on either the range of H-gases or on the range of L-gases

4.7.1.1 The parent engine shall be tested on the relevant reference fuel, as specified in Chapter 4 of this Part, for the relevant range. The fuels are G_R (fuel 1) and G_{23} (fuel 3) for the H-range of gases and G_{25} (fuel 2) and G_{23} (fuel 3) for the L-range of gases. The parent engine shall meet the requirements of this Part without any readjustment to the fuelling between the two tests. One adaptation run over one WHTC hot cycle without measurement is permitted after the change of the fuel. After the adaptation run the engine shall be cooled down in accordance with Clause 7.6.1 of Chapter 3 of this Part.

4.7.1.2 At the manufacturer's request the engine may be tested on a third fuel instead of G_{23} (fuel 3) if the λ -shift factor (S_λ) lies between 0.89 (that is the lower range of G_R) and 1.19 (that is the upper range of G_{25}), for example when fuel 3 is a market fuel. The results of this test may be used as a basis for the evaluation of the conformity of the production

4.7.1.3 In the case of natural gas/bio-methane engines, the ratio of the emission results 'r' shall be determined for each pollutant as follows:

$$r = \frac{\text{emission result on reference fuel 2}}{\text{emission result on reference fuel 1}}$$

Or

$$r_a = \frac{\text{emission result on reference fuel 2}}{\text{emission result on reference fuel 3}}$$

and

$$r_b = \frac{\text{emission result on reference fuel 1}}{\text{emission result on reference fuel 3}}$$

4.7.1.4 On delivery to the customer the engine should bear a label as specified in clause 4.12.1 of this Chapter stating for which range of gases the engine is approved.

4.7.2 Exhaust emission type-approval of an engine running on natural gas or LPG and designed for operation on one specific fuel composition.

4.7.2.1 The parent engine shall meet the emission requirements on the reference fuels G_R and G_{25} in the case of CNG, on the reference fuels G_R and G_{20} in the case of LNG, or on the reference fuels A and B in the case of LPG, as specified in Chapter 4 of this Part. Fine tuning of the fuelling system is allowed between the tests. This fine tuning will consist of a recalibration of the fuelling database, without any alteration to either the basic control strategy or the basic structure of the database. If necessary, the exchange of parts that are directly related to the amount of fuel flow such as injector nozzles is allowed.

4.7.2.2 In the case of CNG, at the manufacturer's request the engine may be tested on the reference fuels G_R and G_{23} , or on the reference fuels G_{25} and G_{23} , in which case the type-approval is only valid for the H-range or the L-range of gases respectively.

4.7.2.3 On delivery to the customer the engine shall bear a label as specified in clause 4.12.1 of this Chapter stating for which fuel range composition the engine has been calibrated.

4.8 Requirements on Fuel-specific Type-approval in the case of Engines Fuelled with Liquefied Natural Gas/Liquefied Biomethane (LNG).

In case of liquefied natural gas/liquefied biomethane, a fuel specific type-approval may be granted subject to the requirements specified in clauses 4.8.1 to 4.8.2.

4.8.1 Conditions for Applying for a Fuel-specific Type-approval in the Case of Engines Fuelled with Liquefied Natural Gas/Liquefied Biomethane (LNG).

4.8.1.1 The manufacturer can only apply for a fuel specific type-approval in the case of the engine being calibrated for a specific LNG gas composition resulting in a λ -shift factor not differing by more than 3% from the λ -shift factor of the G20 fuel specified in Chapter 4 of this Part, and the ethane content of which does not exceed 1.5%.

4.8.1.2 In all other cases the manufacturer shall apply for a universal fuel type approval according to the specifications of clause 4.6.3.2. of this Chapter.

4.8.2 Specific Test Requirements in the Case of a Fuel-specific Type-approval (LNG).

4.8.2.1 In the case of a dual-fuel engine family where the engines are calibrated for a specific LNG gas composition (1) resulting in a λ -shift factor not differing by more than 3% from the λ -shift factor of the G20 fuel specified in Chapter 4 of this Part, and the ethane content of which does not exceed 1.5%, the parent engine shall only be tested on the G20 reference gas fuel, as specified in Chapter 4 of this Part.

4.9 Exhaust Emissions Type-Approval of A Member of a Family

4.9.1 With the exception of the case mentioned in clause 4.8.2 of this Chapter, the type-approval of a parent engine shall be extended to all family members, without further testing, for any fuel composition within the range for which the parent engine has been approved (in the case of engines described in clause 4.7.2 of this Chapter) or the same range of fuels (in the case of engines described in either clause 4.6 and 4.7 of this Chapter) for which the parent engine has been type-approved

4.9.2 If the Test Agency determines that, with regard to the selected parent engine the submitted application does not fully represent the engine family specified in technical specifications submitted by manufacturer as per Chapter 2 of this Part, an alternative and if necessary an additional reference test engine may be selected by the Test Agency and tested.

4.10 Requirements for approval regarding the on-board diagnostic systems.

- 4.10.1 Manufacturers shall ensure that all engine systems and vehicles are equipped with an OBD system.
- 4.10.2 The OBD system shall be designed, constructed and installed on a vehicle in accordance with Chapter 8A of this Part, so as to enable it to identify, record, and communicate the types of deterioration or malfunction specified in that Chapter over the entire life of the vehicle.
- 4.10.3 The manufacturer shall ensure that the OBD system complies with the requirements set out in Chapter 8A of this Part, including the OBD in-use performance requirements, under all normal and reasonably foreseeable driving conditions, including the conditions of normal use specified in Chapter 8B of this Part.
- 4.10.4 When tested with a qualified deteriorated component, the OBD system malfunction indicator shall be activated in accordance with Chapter 8B of this Part. The OBD system malfunction indicator may also be activated at levels of emissions below the OBD thresholds limits specified in Chapter 8A of this Part.
- 4.10.5 The manufacturer shall ensure that the provisions for in-use performance of an OBD engine family laid down in Chapter 8A of this Part are followed.
- 4.10.6 The OBD in-use performance related data shall be stored and made available without any encryption through the standard OBD communication protocol by the OBD system in accordance with the provisions of Chapter 8A of this Part.
- 4.10.7 If the manufacturer chooses, until the date of implementation of BS-VI OBD II for new type approvals, as specified in the MoRTH Gazette Notification G.S.R 889 (E) dated 16.09.2016, OBD systems may comply with alternative provisions as specified in Chapter 8A of this Part and referring to this clause.
- 4.10.8 If the manufacturer chooses, until the date of implementation of BS-VI OBD-II for new type approvals as specified in the MoRTH Gazette Notification G.S.R 889 (E) dated 16.09.2016, he may use alternative provisions for the monitoring of the Diesel Particulate Filter (DPF) as set out in clause 2.3.2.2. of Chapter 8A of this Part.

4.11 Requirements for approval regarding replacement pollution control devices.

- 4.11.1 The manufacturer shall ensure that replacement pollution control devices intended to be fitted to type-approved engine systems or vehicles covered by this Part are type-approved, as separate technical units in accordance with the requirements of clauses 4.11.2. to 4.11.5.

Catalytic converters, deNO_x devices and particulate filters shall be considered to be pollution control devices for the purposes of this Part.

- 4.11.2 Original replacement pollution control devices, which fall within the type covered by the technical specifications submitted as per Chapter 2 of this Part and are intended for fitment to a vehicle to which the relevant type approval document refers, do not need to comply with all provisions of Chapter 12 of this Part provided that they fulfil the requirements of clauses 2.1., 2.2. and 2.3. of that Chapter.
- 4.11.3 The manufacturer shall ensure that the original pollution control device carries identification markings.
- 4.11.4 The identification markings referred to in clause 4.11.3. shall comprise the following:
 - (a) The vehicle or engine manufacturer's name or trade mark;
 - (b) The make and identifying part number of the original pollution control device as specified in technical specifications submitted as per Chapter 2 of this Part.
- 4.11.5 Replacement pollution control devices shall only be type approved according to this Part once the specific testing requirements are introduced in Chapter 12 of this Part.

4.12 Approval marks and labeling for engine systems and vehicles

4.12.1 Labels for natural gas/biomethane and LPG fuelled engines

In the case of natural gas and LPG fuelled engines with a restricted fuel range type-approval, the following labels are applicable:

4.12.1.1 Content:

The following information shall be given:

In the case of clause 4.7.1.4. of this Chapter, the label shall state "ONLY FOR USE WITH NATURAL GAS RANGE H". If applicable, "H" is replaced by "L".

In the case of clause 4.7.2.3. of this Chapter, the label shall state "ONLY FOR USE WITH NATURAL GAS SPECIFICATION ..." or "ONLY FOR USE WITH LIQUEFIED PETROLEUM GAS SPECIFICATION ...", as applicable. All the information in the relevant table(s) in Chapter 4 of this Part shall be given with the individual constituents and limits specified by the engine manufacturer.

The letters and figures shall be at least 4 mm in height.

Note: If lack of space prevents such labelling, a simplified code may be used. In this event, explanatory notes containing all the above information shall be easily accessible to any person filling the fuel tank or performing maintenance or repair on the engine and its accessories, as well as to the Test Agencies concerned. The site and content of these explanatory notes will be determined by agreement between the manufacturer and the Test Agency.

4.12.1.2 Properties

Labels shall be durable for the useful life of the engine. Labels shall be clearly legible and their letters and figures shall be indelible. Additionally, labels shall be attached in such a manner that their fixing is durable for the useful life of the engine, and the labels cannot be removed without destroying or defacing them

4.12.1.3 Placing

Labels shall be secured to an engine part necessary for normal engine operation and not normally requiring replacement during engine life. Additionally, these labels shall be located so as to be readily visible after the engine has been completed with all the auxiliaries necessary for engine operation.

4.12.2 In case of an application for approval for a vehicle type in respect of its engine, the marking specified in clause 4.12.1 shall also be placed close to fuel filling aperture.

4.12.3 In case of an application for approval for a vehicle type with an approved engine, the marking specified in clause 4.12.1 shall also be placed close to the fuel filling aperture.

5.0 REQUIREMENTS AND TESTS

5.1 General

5.1.1 Manufacturers shall equip vehicles and engines so that the components likely to affect emissions are designed, constructed and assembled so as to enable the vehicle or engine, in normal use, to comply with this Part and its implementing measures.

5.1.2 The manufacturer shall take technical measures so as to ensure that the tailpipe emissions are effectively limited, in accordance with this Part, throughout the normal life of the vehicle and under normal conditions of use.

5.1.2.1 Those measures referred to in clause 5.1.2. shall include ensuring that the security of hoses, joints and connections, used within the emission control systems, are constructed so as to conform to the original design intent.

5.1.2.2 The manufacturer shall ensure that the emissions test results comply with the applicable limit value under the test conditions specified in this Part.

5.1.2.3 Any engine system and any element of design liable to affect the emission of gaseous and particulate pollutants shall be designed, constructed, assembled and installed so as to enable the engine, in normal use, to comply with the provisions of this Part. The manufacturer shall also ensure compliance with off-cycle requirements set out in clause 5.1.3. of this Chapter and Chapter 9 of this Part.

- 5.1.2.4 The use of defeat strategies that reduce the effectiveness of emission control equipment shall be prohibited.
- 5.1.2.5 In order to receive a type approval in the case of a petrol or E85 fuelled engine, the manufacturer shall ensure that the specific requirements for inlets to fuel tanks for petrol and E85 fuelled vehicles laid down in clause 6.3. of this Chapter are fulfilled.
- 5.1.3 **Requirements to limit off-cycle emissions**
 - 5.1.3.1 When meeting the requirements of clause 5.1.2. of this Chapter, the technical measures undertaken shall take the following into account:
 - (a) The general requirements, including the performance requirements and the prohibition of defeat strategies, as specified in Chapter 9 of this Part.
 - (b) The requirements to effectively limit the tailpipe emissions under the range of ambient conditions under which the vehicle may be expected to operate, and under the range of operating conditions that may be encountered;
 - (c) The requirements with respect to off-cycle laboratory testing at type approval;
 - (d) The requirements with respect to the PEMS demonstration test at type approval and any additional requirements with respect to off-cycle in use vehicle testing, as provided for in this Part. The in-service conformity factors shall be applicable from the dates specified in Gazette Notification GSR-889(E) dated 16th September 2016 published by MoRTH or as amended from time to time;
 - (e) The requirement for the manufacturer to provide a statement of compliance with the requirements limiting off-cycle emissions.
 - 5.1.3.2 The manufacturer shall fulfil the specific requirements, together with the associated test procedures, set out in Chapter 9 of this Part.
- 5.1.4 **Documentation Requirements**
 - 5.1.4.1 The documentation package required by clause 3 of this Chapter. enabling the Test Agency to evaluate the emission control strategies and the systems on-board the vehicle and engine to ensure the correct operation of NOx control measures, as well as the documentation packages required in Chapter 9 (off-cycle emissions), Chapters 8A and 8B (OBD) and Chapter 14 of this Part (dual-fuel engines), shall be made available in the two following parts:
 - (a) The "formal documentation package"
 - (b) The "extended documentation package" that shall remain strictly confidential.

- 5.1.4.2 The formal documentation package may be brief, provided that it exhibits evidence that all outputs permitted by a matrix obtained from the range of control of the individual unit inputs have been identified. The documentation shall describe the functional operation of the inducement system required by Chapter 10 of this Part, including the parameters necessary for retrieving the information associated with that system. This material shall be retained by the Test Agency.
- 5.1.4.3 The extended documentation package shall include:
- (a) Information on the operation of all AES and BES, including a description of the parameters that are modified by any AES and the boundary conditions under which the AES operate, and indication of which AES and BES are likely to be active under the conditions of the test procedures set out in Chapter 9 of this Part.
 - (b) The extended documentation package shall include a description of the fuel system control logic, timing strategies and switch points during all modes of operation.
 - (c) It shall also include a full description of the inducement system required in Chapter 10 of this Part including the associated monitoring strategies.
 - (d) The description of the anti- tampering measures considered in clause 3.1.4 (b) and 3.2.4 (a) of this Chapter.
- 5.1.4.4 The extended documentation package shall remain strictly confidential. It may be kept by the Test Agency, or, at the discretion of the Test Agency, may be retained by the manufacturer. In the case the manufacturer retains the documentation package, that package shall be identified and dated by the Test Agency once reviewed and approved. It shall be made open for inspection by the Test Agency at the time of approval or at any time during the validity of the approval.
- 5.1.5 **Provisions for electronic system security**
- 5.1.5.1 The general requirements, including the specific requirements for electronic system security, shall be those set out in clause 4 of Chapter 8B of this Part and those described in clause 2 of Chapter 8A of this Part.
- 5.2 Specifications Concerning the Emission of Gaseous and Particulate Pollutants**
- 5.2.1 In undertaking the tests set out in Chapter 3 of this Part the gaseous and particulate matter emissions shall not exceed the limits shown in clause 5.3 of this Chapter.
- 5.2.2 For positive ignition engines subject to the test set out in Chapter 5 of this Part, the maximum permissible carbon monoxide content in the exhaust gases at normal engine idling speed shall be that stated by the vehicle manufacturer. However, the maximum carbon monoxide content shall not exceed the value specified in Gazette Notification, as amended from time to time.

At high idle speed, the carbon monoxide content by volume of the exhaust gases shall not exceed 0.2 per cent vol., with the engine speed being at least 2,000 min⁻¹ and Lambda being 1 ± 0.03 or in accordance with the specifications of the manufacturer.

5.2.3 In the case of a closed crankcase, manufacturers shall ensure that for the tests set out in clauses 6.10. and 6.11. of Chapter 3 of this Part, the engine's ventilation system does not permit the emission of any crankcase gases into the atmosphere. If the crankcase is of an open type, the emissions shall be measured and added to the tailpipe emissions, following the provisions set out in clause 6.10 of Chapter 3 of this Part.

5.2.4 For the dilute testing of positive ignition engines by using an exhaust dilution system, it is permitted to use analyser systems that meet the general requirements and calibration procedures of AIS-137 (Part 3). In this case, the provisions of clause 9 and Appendix 2 of Chapter 3 of this Part shall not apply.

However, the test procedures in clause 7. of Chapter 3 of this Part and the emission calculations provided in clause 8. of Chapter 3 of this Part shall apply.

5.3 EMISSION LIMITS

Table 3 below provides the mass emission limits for BS-VI as specified in the Gazette Notification GSR-889 (E) dated 16th September 2016 published by MoRTH

Table 3 Mass Emission Limits								
	Limit values							
	CO (mg/ kW)	THC (mg/ kWh)	NMHC (mg/ kWh)	CH ₄ (mg/ kWh)	NO _x (mg/ kWh)	NH ₃ (ppm)	PM mass (mg/ kWh)	PM number (#/kWh)
WHSC (CI)	1500	130			400	10	10	8.0 x 10 ¹¹
WHTC (CI)	4000	160			460	10	10	6.0 x 10 ¹¹
WHTC (PI)	4000		160	500	460	10	10	6.0 x 10 ¹¹
Notes: PI Positive Ignition CI Compression Ignition								

5.4 Durability and Deterioration Factors

The manufacturer shall determine deterioration factors that will be used to demonstrate that the gaseous and particulate emissions of an engine family or engine- after-treatment system family remain in conformity with the emission limits set out in clause 5.3 above. Over the normal useful life periods set out below.

The procedures for demonstrating the compliance of an engine system or engine-after-treatment system family over the normal useful life are set out in Chapter 6 of this Part

The mileage and period of time by reference to which the tests for durability of pollution control devices undertaken for type approval and testing of conformity of in-service vehicles or engines are to be carried out shall be the following:

- (a) 160,000 km or five years, whichever is the sooner, in the case of engines fitted to vehicles of category M1, N1 and M2;
- (b) 300,000 km or six years, whichever is the sooner, in the case of engines fitted to vehicles of category N2, N3 with a maximum technically permissible mass not exceeding 16 t and M3 vehicles of Type-I and Type-II (as defined in AIS-052) with a maximum technically permissible mass not exceeding 7.5 t;
- (c) 700,000 km or seven years, whichever is the sooner, in the case of engines fitted to vehicles of category N3 with a maximum technically permissible mass exceeding 16 t and M3 vehicles of Type-II and Type-III (as defined in AIS-052) with a maximum technically permissible mass exceeding 7.5 t.

Alternate to the mileage and period mentioned above, the durability tests can be performed for the minimum service accumulation periods mentioned in the Gazette Notification 889 (E) dated 16th September 2016 and the results to be extrapolated to the mileage mentioned above using the procedure given in Chapter 6 of this Part. Alternate to this procedure, manufacturer may opt for fixed deterioration factors specified in Gazette Notification GSR-889 (E) dated 16th September 2016 published by MoRTH.

5.5 Requirements to Ensure Correct Operation of NOx Control Measures

- 5.5.1 When applying for type approval, manufacturers shall present to Test Agency information showing that the NOx system retains its emission control function during all conditions regularly pertaining in India.

In addition, manufacturers shall provide the Test Agency with information on the operating strategy of any exhaust gas recirculation system (EGR), including it's functioning at low ambient temperatures.

Information on the tests and procedures for fulfilling these requirements is provided in Chapter 10 of this Part.

6.0 INSTALLATION ON THE VEHICLE

6.1. The engine installation on the vehicle shall be performed in such a way as to ensure that the type-approval requirements are met. The following characteristics in respect to the type-approval of the engine shall be taken into consideration:

- 6.1.1. Intake depression shall not exceed that declared for the engine type-approval in Chapter 2 of this Part
- 6.1.2. Exhaust back pressure shall not exceed that declared for the engine type-approval in Chapter 2 of this Part
- 6.1.3. Power absorbed by the auxiliaries needed for operating the engine shall not exceed that declared for the engine type-approval in Chapter 2 of this Part;
- 6.1.4. The characteristics of the exhaust after-treatment system shall be in accordance with those declared for the engine type-approval in Chapter 2 of this Part.

6.2 Installation of A Type-Approved Engine On A Vehicle

6.2.1 The installation of an engine type-approved as a separate technical unit on a vehicle shall, in addition, comply with the following requirements:

- (a) As regard to the compliance of the OBD system, the installation shall, according to Appendix 1 of Chapter 8B of this Part, meet the manufacturer's installation requirements as specified in Chapter 2 of this Part;
- (b) As regard to the compliance of the system ensuring the correct operation of NO_x control measures, the installation shall, according to Appendix 4 of Chapter 10 of this Part, meet the manufacturer's installation requirements as specified in Chapter 2 of this Part.
- (c) The installation of a dual-fuel engine type-approved as a separate technical unit on a vehicle shall, in addition, meet the specific installation requirements and the manufacturer's installation requirements set out in Chapter 14 of this Part.

6.3 Inlet to Fuel Tanks in The Case of a Petrol or E85 Fuelled Engine

6.3.1. The inlet orifice of the petrol or E85 tank shall be designed so it prevents the tank from being filled from a fuel pump delivery nozzle that has an external diameter of 23.6 mm or greater.

6.3.2. Clause 6.3.1 shall not apply to a vehicle for which both of the following conditions are satisfied:

- (a) The vehicle is designed and constructed so that no device designed to control the emission of gaseous pollutants is adversely affected by leaded petrol;

- (b) The vehicle is conspicuously, legibly and indelibly marked with the symbol for unleaded petrol specified in AIS-071 (Part 1) in a position immediately visible to a person filling the fuel tank. Additional markings are permitted.
- 6.3.3. Provision shall be made to prevent excess evaporative emissions and fuel spillage caused by a missing fuel filler cap. This may be achieved by using one of the following:
- (a) An automatically opening and closing, non-removable fuel filler cap;
 - (b) Design features which avoid excess evaporative emissions in the case of a missing fuel filler cap;
 - (c) Or in case of M1 or N1 vehicles, any other provision which has the same affect. Examples may include, but are not limited to, a tethered filler cap, a chained filler cap or one utilizing the same locking key for the filler cap as for the vehicle's ignition. In this case the key shall be removable from the filler cap only in the locked condition.

7.0 ENGINE FAMILY

7.1. Parameters defining the engine family

The engine family, as determined by the engine manufacturer, shall comply with clause 5.2 of Chapter 3 of this Part.

In case of a dual-fuel engine, the engine family shall also comply with the additional requirements of clause 3.1.1 of Chapter 14 of this Part.

7.2 Choice of the parent engine

The parent engine of the family shall be selected in accordance with the requirements set out in clause 5.2.4 of Chapter 3 of this Part .

In case of a dual-fuel engine, the parent engine family shall also comply with the additional requirements of clause 3.1.2. of Chapter 14 of this Part.

7.3 Extension to include a new engine system into an engine-family

7.3.1 At the request of the manufacturer and upon approval of the Test Agency, a new engine system may be included as a member of a certified engine family if the criteria specified in clause 7.1 of this Chapter are met.

7.3.2 If the elements of design of the parent engine system are representative of those of the new engine system according to clause 7.2. of this Chapter or, in the case of dual-fuel engines, to clause 3.1.2 of Chapter 14 of this Part, then the parent engine system shall remain unchanged and the manufacturer shall modify the application document specified in Chapter 2 of this Part.

- 7.3.2 If the new engine system contains elements of design that are not represented by the parent engine system according to clause 7.2. of this Chapter or, in the case of dual-fuel engines, to clause 3.1.2 of Chapter 14 of this Part, but itself would represent the whole family according to these clauses, then the new engine system shall become the new parent engine. In this case the new elements of design shall be demonstrated to comply with the provisions of this Part and the information document specified in Chapter 2 of this Part shall be modified.

7.4 Parameters for defining an OBD -Engine family

The OBD-engine family shall be determined by basic design parameters that shall be common to engine systems within the family, in accordance with clause 6.1. of Chapter 8B of this Part.

8.0 CONFORMITY OF PRODUCTION

- 8.1 Measures to ensure production conformity must be taken in accordance with the provisions as per AIS-137 (Part 6). However, when the period between commencement of production of a new model and beginning of next rationalized COP period is less than two months, the same would be merged with the rationalized COP period.

- 8.1.1. Conformity of production shall be checked on the basis of the description in the type approval certificate. For verifying the conformity of production the following procedure as per Option 1 as given in clause 8.3 of this Chapter shall be adopted.

To verify the conformity of production for low volume vehicle model and its variants with production volume less than 250 no. in any consecutive period of six months in a year, manufacture can choose from option 1 (clause 8.3 of this Chapter) or option 2 (clause 8.4 of this Chapter) as listed below.

8.2. General Requirements

- 8.2.1 In applying Option 1, clause 8.3 of this Chapter, the measured emission of the gaseous and particulate pollutants from engines subject to checking for conformity of production shall be adjusted by application of the appropriate deterioration factors (DF's) for that engine as recorded in the type approval certificate or test report granted in accordance with this Part.

8.2.2 Reserved

- 8.2.3 Three engine samples subject to tests shall be randomly taken from the series production.

8.3 Option 1

8.3.1 Emission of Pollutants

If emissions of pollutants are to be measured and an engine type approval has had one or more extensions, the tests shall be carried out on the engines described in the application document relating to the relevant extension.

8.3.2 Conformity of the engine subjected to a pollutant test:

After submission of the engine to the Test Agencies, the manufacturer may not carry out any adjustment to the engines selected.

8.3.2.1 Three engines shall be taken from the series production of the engines under consideration. Engines shall be subjected to testing on the WHTC and on the WHSC, if applicable, for the checking of the production conformity. The limit values shall be those set out in clause 5.3. of this Chapter.

8.3.2.2 The tests shall be carried out according to Appendix 1 of this Chapter

8.3.2.3 On the basis of test of the engine by sampling as set out in clause 8.3.2.1. of this Chapter, the series production of the engines under consideration is regarded as conforming where a pass decision is reached for all the pollutants and as non-conforming where a fail decision is reached for one pollutant, in accordance with the test criteria applied in the Appendix 1 of this Chapter.

When the pass decision has been reached for one pollutant, this decision may not be changed as a consequence of a result from any additional tests made in order to reach a decision for the other pollutants.

If a pass decision is not reached for all the pollutants and if no fail decision is reached for any pollutant, a test is carried out on another engine (see Figure 1 below).

If no decision is reached, the manufacturer may at any time decide to stop testing. In that case a fail decision is recorded

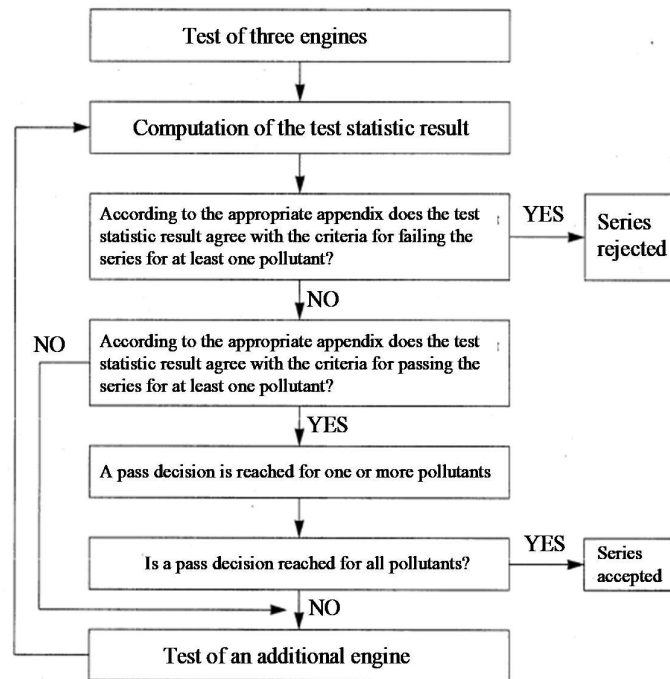


Figure 1

Option 1 : COP Test Procedure

8.4 Option 2

8.4.1 Conformity of the engine subjected to a pollutant test

After submission of the engine to the Test Agencies, the manufacturer shall not carry out any adjustment to the engines selected

Three engines shall be taken from the series production. With agreement of Test Agency, only one engine is subject to testing on the WHTC and on the WHSC, if applicable, for the checking of the production conformity. The limit values shall be those set out in clause 5.3. of this Chapter.

The tests shall be carried out according to Appendix 1 of this Chapter

On the basis of a test of the engine, the production of a series is regarded as conforming where a pass decision is reached for all the pollutants and nonconforming where a no pass decision is reached for one pollutant, in accordance with the limit values are given in Table 3 in clause 5.3 of this Chapter. When no pass decision has been reached for one pollutant sample 2 and 3 are subjected to test mentioned in 8.4.1 of this Chapter

If no pass decision is reached for all the pollutants and if no fail decision is reached for one pollutant, a test is carried out on another engine (see Figure 2 below).

If no decision is reached, the manufacturer may at any time decide to stop testing. In that case a fail decision is recorded.

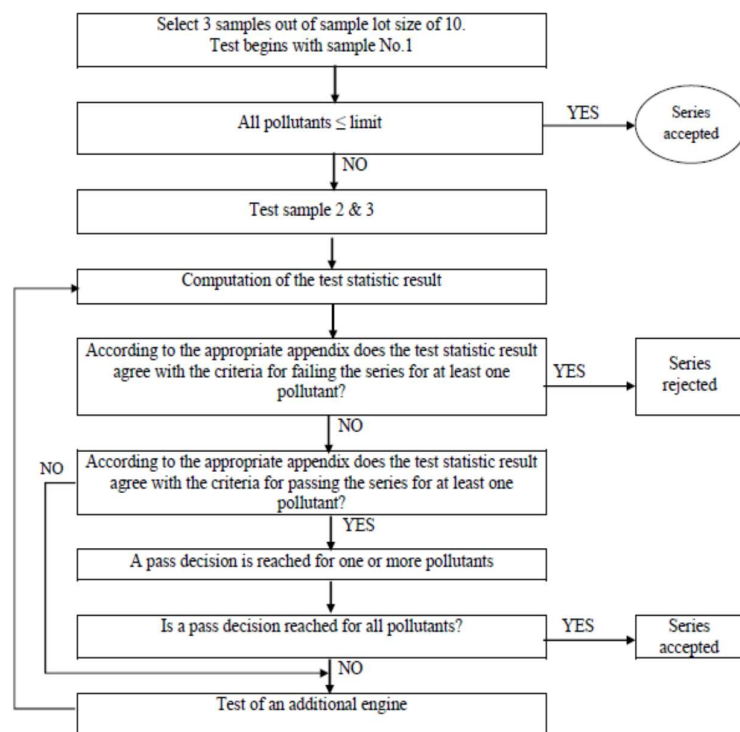


Figure 2

Option 2 : Schematic of Production Conformity Testing

8.5 Common Requirements for Option 1 & Option 2

8.5.1 The tests shall be carried out on newly manufactured engines.

8.5.1.1 At the request of the manufacturer, the tests may be carried out on engines which have been run-in, up to a maximum of 125 hours. In this case, the running-in procedure shall be conducted by the manufacturer who shall undertake not to make any adjustments to those engines.

8.5.1.2 When the manufacturer requests to conduct a running-in procedure in accordance with clause 8.5.1.1., it may be carried out on either of the following:

- (a) All the engines that are tested; or
- (b) The first engine tested, with the determination of an evolution coefficient as follows:
 - (i) The pollutant emissions shall be measured both on the newly manufactured engine and before the maximum of 125 hours set in p clause 8.5.1.1 on the first engine tested;
 - (ii) The evolution coefficient of the emissions between the two tests shall be calculated for each pollutant:

$$\frac{\text{Emissions at second test}}{\text{Emissions at first test}}$$

The evolution coefficient may have a value less than one.

The subsequent test engines shall not be subjected to the running-in procedure, but their emissions when newly manufactured shall be modified by the evolution coefficient.

In this case, the values to be taken shall be the following:

- (a) For the first engine, the values from the second test;
- (b) For the other engines, the values when newly manufactured multiplied by the evolution coefficient.

8.5.1.3 For diesel, ethanol (ED95), petrol, E85, LNG and LPG fuelled including dual-fuel engines, all these tests may be conducted with the applicable market fuels. However, at the manufacturer's request, the reference fuels described in Chapter 4 of this Part may be used. This implies tests, as described in clause 4 of this Chapter.

8.5.1.4 For natural gas fuelled engines including dual fuel engines, all these tests may be conducted with market fuel in the following way:

- (a) For H marked engines with a market fuel within the H-range ($0.89 \leq S\lambda \leq 1.00$);
- (b) For L marked engines with a market fuel within the L-range ($1.00 \leq S\lambda \leq 1.19$);
- (c) For HL marked engines with a market fuel within the extreme range of the λ -shift factor ($0.89 \leq S\lambda \leq 1.19$).

However, at the manufacturer's request, the reference fuels described in Chapter 4 of this Part may be used. This implies tests, as described in clause 4 of this Chapter.

8.5.1.5 Non-compliance of Gas and Dual-fuel engines:

In the case of dispute caused by the non-compliance of gas fuelled engines including dual fuel engines, when using a market fuel, the tests shall be performed with a reference fuel on which the parent engine has been tested, and at the request of the manufacturer, with the possible additional third fuel, as referred to in clauses 4.6.4.1 and 4.7.1.2 of this Chapter, on which the parent engine may have been tested.

When applicable, the result shall be converted by a calculation, applying the relevant factors “r”, “ra” or “rb” as described in clauses 4.6.5., 4.6.6.1. and 4.7.1.3 of this Chapter. If r, ra or rb are less than 1, no correction shall take place.

The measured results and when applicable, the calculated results shall demonstrate that the engine meets the limit values with all relevant fuels (for example fuels 1, 2 and, if applicable, third fuel in the case of natural gas engines, and fuels A and B in the case of LPG engines).

8.5.1.6 Tests for conformity of production of a gas fuelled engine laid out for operation on one specific fuel composition shall be performed on the fuel for which the engine has been calibrated.

8.6 On-Board Diagnostics (OBD)

8.6.1 When the Test Agency determines that the quality of production seems unsatisfactory, it may request a verification of the conformity of production of the OBD system. Such verification shall be carried out in accordance with the following:

An engine shall be randomly taken from series production and subjected to the tests described in Chapter 8 B of this Part and in case of dual fuel engines to the additional tests required by clause 7 of Chapter 14 of this Part. The tests may be carried out on an engine that has been run-in up to a maximum of 125 hours.

8.6.2 The production is deemed to conform if this engine meets the requirements of the tests described in Chapter 8B of this Part and in case of dual fuel engines to the additional tests required by clause 7 of Chapter 14 of this Part.

8.6.3 If the engine taken from the series production does not satisfy the requirements of clause 8.6.1. above, a further random sample of four engines shall be taken from the series production and subjected to the tests described in Chapter 8B of this Part and in the case of dual fuel engines to the additional tests required by clause 7 of Chapter 14 of this Part. The tests may be carried out on engines that have been run-in, up to a maximum of 125 hours.

8.6.4 The production is deemed to conform if at least three engines out of the further random sample of four engines meet the requirements of the tests described in Chapter 8B of this Part.

8.7 Electronic control unit (ECU) information required for in-service testing

- 8.7.1. The availability of the data stream information requested in clause 9.4.2.1. of this Chapter according to the requirements of clause 9.4.2.2 of this Chapter. shall be demonstrated by using an external OBD scan-tool as described in Chapter 8B of this Part.
- 8.7.2 In the case where this information cannot be retrieved in a proper manner while the scan-tool is working properly according to Chapter 8B, the engine shall be considered as non-compliant.
- 8.7.3 The conformity of the ECU torque signal with the requirements of clauses 9.4.2.2. and 9.4.2.3 of this Chapter. Shall be demonstrated by performing the WHSC test according to Chapter 3 of this Part.
- 8.7.4 In the case where the test equipment does not match the requirements specified in standard AIS-137 (Part 5) concerning auxiliaries, the measured torque shall be corrected in accordance to the correction method set out in Chapter 3 of this Part.
- 8.7.5 The conformity of the ECU torque signal shall be considered sufficient if the calculated torque remains within the tolerances specified in clause 9.4.2.5 of this Chapter.
- 8.7.6 The availability and conformity checks of the ECU information required for In-service testing shall be performed by the manufacturer on a regular basis on each produced engine-type within each produced engine-family.
- 8.7.7 The results of the manufacturer's survey shall be made available to the Test Agency at its request.
- 8.7.8 At the request of the Test Agency, the manufacturer shall demonstrate the availability or the conformity of the ECU information in serial production by performing the appropriate testing referred to in clauses 8.7.1 to 8.7.4 on a sample of engines selected from the same engine type. The sampling rules including sampling size and statistical pass fail criteria shall be those specified in clauses 8.1. to 8.3. of this Chapter for checking the conformity of emissions.

9.0 CONFORMITY OF IN-SERVICE VEHICLES/ENGINES

- 9.1** This clause sets out the in-service conformity requirements for vehicles/engines type-approved to this Part.

9.2. In-service conformity

- 9.2.1. Measures to ensure in-service conformity of vehicles or engine systems type approved under this Part as per the applicable CMVR Gazette Notification for which the vehicle is subjected to test, and complying with the requirements of Chapter 7 of this Part as applicable.
- 9.2.2. The technical measures taken by the manufacturer shall be such as to ensure that the tailpipe emissions are effectively limited, throughout the normal life of the vehicles under normal conditions of use. The conformity with the provisions of this Part shall be checked over the normal useful life of an engine system installed in a vehicle under normal conditions of use as specified in Chapter 7 of this Part as applicable.
- 9.2.3. The manufacturer shall carry out in-service testing in consultation with Test Agency which granted the original type approval in accordance with the initial plan submitted at type approval. Any deviation from the initial plan shall be justified to the satisfaction of the Test Agency.
- 9.2.4. If the Test Agency which granted the original type approval is not satisfied with the test result in accordance with clause 10 of Chapter 7 of this Part or has reported evidence of unsatisfactory in service conformity, Test Agency may order the manufacturer to run a test for confirmatory purposes. The Test Agency shall examine the confirmatory test report supplied by the manufacturer.
- 9.2.5. Where the Test Agency which granted the original type approval is not satisfied with the results of in-service tests or confirmatory tests in accordance with the criteria set out in Chapter 7 of this Part, it shall require the manufacturer to submit a plan of remedial measures to remedy the non-conformity in accordance with clause 9.3. of this Chapter and clause 9. of Chapter 7 of this Part.

9.3. Remedial Measures

- 9.3.1. On request of the Test Agency and following in-service testing in accordance with clause 9.2. of this Chapter, the manufacturer shall submit the plan of remedial measures to the Test Agency no later than 60 working days after receipt of the notification from the Test Agency. Where the manufacturer can demonstrate to the satisfaction of the Test Agency that further time is required to investigate the reason for the non-compliance in order to submit a plan of remedial measures, an extension may be granted.
- 9.3.2. The remedial measures shall apply to all engines in service belonging to the same engine families or OBD engine families and be extended also to engine families or OBD engine families which are likely to be affected with the same defects. The need to amend the type approval documents shall be assessed by the manufacturer and the result reported to the Test Agency.

- 9.3.3. The Test Agency shall consult the manufacturer in order to secure agreement on a plan of remedial measures and on executing the plan. If the Test Agency which granted the original type approval establishes that no agreement can be reached, it shall take the necessary measures, including, where necessary, the withdrawal of type approval, to ensure that production vehicles, systems, components or separate technical units, as the case may be, are brought into conformity with the approved type. If the type approval is withdrawn, the Test Agency shall inform the Ministry within 20 working days of the withdrawal and of the reasons therefor.
- 9.3.4. The Test Agency shall within 30 working days from the date on which it has received the plan of remedial measures from the manufacturer, approve or reject the plan of remedial measures. The Test Agency shall within the same time also notify the manufacturer of its decision to approve or reject the plan of remedial measures.
- 9.3.5. The manufacturer shall be responsible for the execution of the approved plan of remedial measures.
- 9.3.6. The manufacturer shall keep a record of every engine system or vehicle recalled and repaired or modified and of the workshop which performed the repair. The Test Agency shall have access to that record on request during the execution and for a period of 5 years after the completion of the execution of the plan.
- 9.3.7. Any repair or modification referred to in clause 9.3.6. shall be recorded in a certificate supplied by the manufacturer to the owner of the engine or vehicle.

9.4 Requirements and Tests for In-Service Testing

9.4.1. Introduction

This clause (clause 9.4.) sets out the specifications and tests of the ECU data at type approval for the purpose of in-service testing.

9.4.2. General Requirements

- 9.4.2.1. For the purpose of in-service testing, the calculated load (engine torque as a percentage of maximum torque and the maximum torque available at the current engine speed), the engine speed, the engine coolant temperature, the instantaneous fuel consumption, and the reference maximum engine torque as a function of engine speed shall be made available by the OBD system in real time and at a frequency of at least 1 Hz, as mandatory data stream information.
- 9.4.2.2. The output torque may be estimated by the ECU using built-in algorithms to calculate the produced internal torque and the friction torque.

- 9.4.2.3. The engine torque in Nm resulting from the above data stream information shall permit a direct comparison with the values measured when determining the engine power. In particular, any eventual corrections as regards auxiliaries shall be included in the above data stream information.
- 9.4.2.4. Access to the information required in clause 9.4.2.1. of this Chapter shall be provided in accordance with the requirements set out in Chapter 8 of this Part and with the standards referred to in Appendix 6 of Chapter 8B of this Part.
- 9.4.2.5. The average load at each operating condition in Nm calculated from the information requested in clause 9.4.2.1. of this Chapter shall not differ from the average measured load at that operating condition by more than:
 - (a) 7 per cent (i.e., $\pm 7\%$) when determining the engine power according to AIS-137 (Part 5);
 - (b) 10 per cent (i.e., $\pm 10\%$) when performing the World Harmonized Steady State Cycle (here in after "WHSC") test according to Chapter 3, clause 7.7.
- 9.4.2.6. External access to the information required in clause 9.4.2.1. of this Chapter shall not influence the vehicle emissions or performance.
- 9.4.3. **Verification of the availability and conformity of the ECU information required for in- service testing**
- 9.4.3.1. The availability of the data stream information required in clause 9.4.2.1., according to the requirements set out in clause 9.4.2.2. of this Chapter, shall be demonstrated by using an external OBD scan-tool as described in Chapter 8B of this Part.
- 9.4.3.2. In the case where this information cannot be retrieved in a proper manner, using a scan-tool that is working properly, the engine is considered as non-compliant.
- 9.4.3.3. The conformity of the ECU torque signal to the requirements of clauses 9.4.2.2. and 9.4.2.3. of this Chapter shall be demonstrated with the parent engine of an engine family when determining the engine power according to the procedure laid down in the standard AIS-137 (Part 5) and when performing the WHSC test according to Chapter 3, clause 7.7. and off-cycle laboratory testing at type approval according to clause 7. of Chapter 9 of this Part.
- 9.4.3.3.1 The conformity of the ECU torque signal to the requirements of clause 9.4.2.2 and 9.4.2.3 of this Chapter shall be demonstrated for each engine family member when determining the engine power according to the procedure laid down in the standard AIS-137 (Part 5) For this purpose additional measurements shall be performed at several part load and engine speed operating points (for example at the modes of the WHSC and some additional random points).

9.4.3.4. In the case where the engine under test does not match the requirements set out in the standard AIS-137 (Part 5), concerning auxiliaries, the measured torque shall be corrected in accordance to the correction method for power as set out in clause 6.3.5 of Chapter 3 of this Part.

9.4.3.5. The conformity of the ECU torque signal is considered to be demonstrated if the torque signal remains within the tolerances set out in clause 9.4.2.5. of this Chapter.

10.0 PENALTIES FOR NON CONFORMITY OF PRODUCTION

10.1 The approval granted in respect of an engine or vehicle type pursuant to this Part may be withdrawn if the requirements laid down in clause 8.1 are not complied with or if the engine(s) or vehicle (s) taken fail to the pass test prescribed in clause 8.3 of this Chapter.

10.2 If the vehicle/engine fails to meet the requirements of COP, the Test Agency shall send the copies of the test report to the Nodal Agency and the manufacturer.

11.0 MODIFICATION AND EXTENSION OF APPROVAL OF THE APPROVED TYPE

11.1. Every modification of the approved type shall be notified to the Test Agency which approved the type. The Test Agency may then either:

11.1.1. Consider that the modifications made are unlikely to have an appreciable adverse effect and that in any case the modified type still complies with the requirement; or

11.1.2. Require a further test report.

11.2. Confirmation or refusal of approval, specifying the alterations, shall be communicated to the manufacturer.

12.0 PRODUCTION DEFINITELY DISCONTINUED

If the holder of the approval completely ceases to manufacture the type approved engines or vehicles in accordance with this Part, he shall so inform the Test Agency which granted the approval. Upon receiving the relevant communication that Test Agency shall inform thereof Ministry.

13.0 TRANSITIONAL PROVISIONS

13.1. General provisions

13.1.1. As from the official date of entry into force of this Part, no Test Agency shall refuse to grant approval under this Part as amended.

13.1.2. As from the date of implementation of BS-VI emission norms, Test Agencies shall grant approvals only if the engine meets the requirements of this Part as amended.

13.2. New Type Approvals

- 13.2.1. Test Agencies shall, from the date of entry into force of BS-VI OBD-I norms specified in MoRTH Gazette Notification GSR 889(E) dated 16.09.2016, grant an approval to an engine system or vehicle only if it complies with:
- (a) The requirements of clause 4.1. of this Chapter;
 - (b) The performance monitoring requirements of clause 2.3.2.2. of Chapter 8A of this Part in case of compression ignition and dual fuel engines and vehicles.
 - (c) The NOx OTL monitoring requirements as set out in the Table 1 of Chapter 8A of this Part;
 - (d) The reagent quality and consumption requirements as set out in clause 7.1.1.1 of Chapter 10 of this Part.
- 13.2.1.1 In accordance with the requirements of clause 6.4.4. of Chapter 8A of this Part manufacturers are exempted from providing a statement of OBD in-use performance compliance.
- 13.2.2 Reserved
- 13.2.3 Test Agencies shall, from the date of implementation of BS-VI OBD-II norms, grant an approval to an engine system or vehicle only if it complies with:
- (a) The requirements of clause 4.1 of this Chapter;
 - (b) The PM Mass OTL monitoring requirements as set out in Table 2 of Chapter 8A of this Part;
 - (c) The NOx OTL monitoring requirements as set out in Table 2 of Chapter 8A of this Part;
 - (d) The reagent quality and consumption requirements as set out in clauses 7.1.1. and 8.4.1. of Chapter 10 of this Part;
 - (e) The requirements regarding the plan and implementation of the monitoring techniques according to clauses 2.3.1.2. and 2.3.1.2.1 of Chapter 8A of this Part;
 - (f) The requirements of clause 6.4.1. of Chapter 8A of this Part for providing a statement of OBD in-use Performance compliance.

CHAPTER 1 - APPENDIX 1

PROCEDURE FOR PRODUCTION CONFORMITY TESTING

1. This Appendix describes the procedure to be used to verify production conformity for the emissions of pollutants.
2. With a minimum sample size of three engines the sampling procedure is set so that the probability of a lot passing a test with 40 % of the engines defective is 0.95 (producer's risk = 5 %) while the probability of a lot being accepted with 65 % of the engines defective is 0.10 (consumer's risk = 10 %).
3. The values of the pollutants given in clause 5.3 of this Chapter, after having applied the relevant DF, are considered to be log normally distributed and should be transformed by taking their natural logarithms. Let m_0 and m denote the minimum and maximum sample size respectively ($m_0 = 3$ and $m = 32$) and let n denote the current sample number.
4. If the natural logarithms of the measured values (after having applied the relevant DF) in the series are x_1, x_2, \dots, x_i and L is the natural logarithm of the limit value for the pollutant, then, define:

$$d_i = x_i - L \text{ and,}$$

$$\bar{d}_n = \frac{1}{n} \sum_{i=1}^n d_i$$

$$v_n^2 = \frac{1}{n} \sum_{i=1}^n (d_i - \bar{d}_n)^2$$

5. Table 1 of this Appendix shows values of the pass (A_n) and fail (B_n) decision numbers against current sample number. The test statistic result is the ratio: \bar{d}_n / v_n and shall be used to determine whether the series has passed or failed as follows:

for $m_0 \leq n < m$:

— pass the series if $\bar{d}_n / v_n \leq A_n$,

— fail the series if $\bar{d}_n / v_n \geq B_n$,

— take another measurement if $A_n < \bar{d}_n / v_n < B_n$.

6. Remarks:

The following recursive formulae are useful for calculating successive values of the test statistic:

$$\bar{d}_n = \left(1 - \frac{1}{n}\right)\bar{d}_{n-1} + \frac{1}{n}d_n$$

$$V_n^2 = \left(1 - \frac{1}{n}\right)V_{n-1}^2 + \frac{(\bar{d}_n - d_n)^2}{n-1} \quad (n = 2, 3, \dots; \bar{d}_1 = d_1; V_1 = 0)$$

Table 1

**Pass and Fail Decision Numbers of Appendix 1 Sampling Plan
Minimum Sample Size: 3**

Cumulative Number of Engine Tested (sample size)	Pass Decision Number An	Fail Decision Number Bn
3	-0.80381	16.64743
4	-0.76339	7.68627
5	-0.72982	4.67136
6	-0.69962	3.25573
7	-0.67129	2.45431
8	-0.64406	1.94369
9	-0.61750	1.59105
10	-0.59135	1.33295
11	-0.56542	1.13566
12	-0.53960	0.97970
13	-0.51379	0.85307
14	-0.48791	0.74801
15	-0.46191	0.65928
16	-0.43573	0.58321
17	-0.40933	0.51178
18	-0.38266	0.45922
19	-0.35570	0.40788
20	-0.32840	0.36203
21	-0.30072	0.32078
22	-0.27263	0.28243
23	-0.24410	0.24943
24	-0.21509	0.21831
25	-0.18557	0.18970
26	-0.15550	0.16328
27	-0.12483	0.13880
28	-0.09354	0.11603
29	-0.06159	0.09480
30	-0.02892	0.07493
31	-0.00449	0.05629
32	0.03876	0.03876

CHAPTER 1-APPENDIX 2

**SUMMARY OF APPROVAL PROCESS FOR ENGINES FUELLED WITH
NATURAL GAS, ENGINES FUELLED WITH LPG AND DUAL FUEL
ENGINES FUELLED WITH NATURAL GAS /BIOMETHANE OR LPG**

Approval for LPG Engines

	Clause 4.6 requirements on universal fuel range type approval	Numbers of test runs	Calculation of “r”	Clause 4.7 requirements on restricted fuel range type approval in case of positive ignition engines fuelled with natural gas or LPG	Numbers of test runs	Calculation of “r”
Refer to clause 4.6.6 LPG engine adaptable to any fuel composition	Fuel A and Fuel B	2	$r = \frac{\text{fuel B}}{\text{fuel A}}$			
Refer to clause 4.7.2 LPG engine laid out for operation on one specific fuel composition				Fuel A and Fuel B fine-tuning between the tests allowed	2	

Approval for Natural Gas Engines

	Clause 4.6 requirements on universal fuel range type approval	Numbers of test runs	Calculation of “r”	Clause 4.7 requirements on restricted fuel range type approval in case of positive ignition engine fuelled with natural gas or LPG	Numbers of test runs	Calculation of “r”
Refer to clause 4.6.3 NG engine adaptable to any fuel composition	G _R (1) and G ₂₅ (2) at manufacturer's request engine may be tested on an additional market fuel (3), if S _λ =0.89-1.19	2 (max 3)	$r = \frac{\text{fuel 2}(G_{25})}{\text{fuel 1}(G_R)}$ <p>and if tested with an additional fuel,</p> $r_a = \frac{\text{fuel 2}(G_{25})}{\text{fuel 3}(\text{market fuel})}$ <p>and</p> $r_b = \frac{\text{fuel 1}(G_R)}{\text{fuel 3}(G_{23} \text{ or market fuel})}$			
Refer to clause 4.6.4 NG engine which is self-adaptive by a switch	G _R (1) and G ₂₃ (3) for H and G ₂₅ (2) G ₂₃ (3) for L at manufacturer's request engine may be tested on market fuel (3), instead of G ₂₃ , if S _λ =0.89-1.19	2 for H range and 2 for the L range at respective position of switch 4	$r_b = \frac{\text{fuel 1}(G_R)}{\text{fuel 3}(G_{23} \text{ or market fuel})}$ $r_a = \frac{\text{fuel 2}(G_{25})}{\text{fuel 3}(G_{23} \text{ or market fuel})}$			
Refer to clause 4.7.1 NG engine laid out for operation on either H-range gas or L-range gas				G _R (1) and G ₂₃ (3) for H or G ₂₅ (2) G ₂₃ (3) for L At manufacturer request engine may be tested on market fuel (3), instead of G ₂₃ , if S _λ =0.89-1.19	2 for H range or 2 for the L-range 2	$r_b = \frac{\text{fuel 1}(G_R)}{\text{fuel 3}(G_{23} \text{ or market fuel})}$ <p>for the H range or</p> $r_b = \frac{\text{fuel 2}(G_{25})}{\text{fuel 3}(G_{23} \text{ or market fuel})}$ <p>for the L range</p>
Refer to clause 4.7.2. NG-engine laid out for operation on one specific fuel composition				G _R (1) and G ₂₅ (2), Fine-tuning between the tests allowed; At manufacturer's request engine may be tested on: G _R (1) and G ₂₃ (3) for H or G ₂₅ (2) and G ₂₃ (3) for L		

APPROVAL FOR DUEL FUELLED WITH NATURAL GAS / BIOMEHNE OR LPG					
Duel fuel type ⁽¹⁾	Diesel mode	Dual fuel mode			
		CNG	LNG	LNG20	LPG
1A		Universal or Restricted (2 test)	Universal (2 tests)	Fuel specific (1test)	Universal or Restricted (2 test)
1B	Universal (1 test)	Universal or Restricted (2 test)	Universal (2 tests)	Fuel specific (1test)	Universal or Restricted (2 test)
2A		Universal or Restricted (2 test)	Universal (2 tests)	Fuel specific (1test)	Universal or Restricted (2 test)
2B	Universal (1 test)l	Universal or Restricted (2 test)	Universal (2 tests)	Fuel specific (1test)	Universal or Restricted (2 test)
3B	Universal (1 test)	Universal or Restricted (2 test)	Universal (2 tests)	Fuel specific (1test)	Universal or Restricted (2 test)
⁽¹⁾ According to the definitions of Chapter 14 of this Part					

CHAPTER 2

ESSENTIAL CHARACTERISTICS OF THE VEHICLE AND ENGINE AND INFORMATION CONCERNING THE CONDUCT OF TESTS

- 1.0 Vehicle manufacturer shall provide information on essential characteristics of the vehicle and engine and information concerning the conduct of tests as per AIS-007, as amended time to time.

CHAPTER 3

TEST PROCEDURE

1.0 INTRODUCTION

- 1.1 This Chapter describes the methods of determining gaseous emissions, particulate emissions from the engines to be tested. Two test cycles are described that shall be applied:

World-wide Harmonized Steady State Cycle (WHSC)

World-wide Harmonized Transient Cycle (WHTC) (Cold and Hot)

- 1.2 The test shall be carried out with the engine mounted on a test bench and connected to a dynamometer.

- 1.3 This Chapter is based on the world-wide harmonized heavy duty certification (WHDC) procedure given in Global Technical Regulation (GTR) - 4

2.0 RESERVED

3.0 DEFINITIONS, SYMBOLS & ABBREVIATIONS

3.1 Definitions

- 3.1.1 **"Declared maximum power (P_{max})"** means the maximum power in kW (net power) as declared by the manufacturer in his application for approval.
- 3.1.2 **"Delay time"** means the difference in time between the change of the component to be measured at the reference point and a system response of 10 per cent of the final reading (t_{10}) with the sampling probe being defined as the reference point. For the gaseous components, this is the transport time of the measured component from the sampling probe to the detector.
- 3.1.3 **"Drift"** means the difference between the zero or span responses of the measurement instrument after and before an emissions test.
- 3.1.4 **"Full flow dilution method"** means the process of mixing the total exhaust flow with diluent prior to separating a fraction of the diluted exhaust stream for analysis.
- 3.1.5 **"High speed (n_{hi})"** means the highest engine speed where 70 per cent of the declared maximum power occurs.
- 3.1.6 **"Low speed (n_{lo})"** means the lowest engine speed where 55 per cent of the declared maximum power occurs.

- 3.1.7 **"Maximum power (P_{max})"** means the maximum power in kW as specified by the manufacturer.
- 3.1.8 **"Maximum torque speed"** means the engine speed at which the maximum torque is obtained from the engine, as specified by the manufacturer.
- 3.1.9 **"Normalized torque"** means engine torque in per cent normalized to the maximum available torque at an engine speed.
- 3.1.10 **"Operator demand"** means an engine operator's input to control engine output. The operator may be a person (i.e., manual), or a governor (i.e., automatic) that mechanically or electronically signals an input that demands engine output. Input may be from an accelerator pedal or signal, a throttle-control lever or signal, a fuel lever or signal, a speed lever or signal, or a governor set point or signal.
- 3.1.11 **"Partial flow dilution method"** means the process of separating a part from the total exhaust flow, then mixing it with an appropriate amount of diluent prior to the particulate sampling filter.
- 3.1.12 **"Ramped steady state test cycle"** means a test cycle with a sequence of steady state engine test modes with defined speed and torque criteria at each mode and defined ramps between these modes (WHSC).
- 3.1.13 **"Rated speed"** means the maximum full load speed allowed by the governor as specified by the manufacturer in his sales and service literature, or, if such a governor is not present, the speed at which the maximum power is obtained from the engine, as specified by the manufacturer. in his sales and service literature.
- 3.1.14 **"Response time"** means the difference in time between the change of the component to be measured at the reference point and a system response of 90 per cent of the final reading (t_{90}) with the sampling probe being defined as the reference point, whereby the change of the measured component is at least 60 per cent full scale (FS) and takes place in less than 0.1 second. The system response time consists of the delay time to the system and of the rise time of the system.
- 3.1.15 **"Rise time"** means the difference in time between the 10 per cent and 90 per cent response of the final reading ($t_{90} - t_{10}$).
- 3.1.16 **"Span response"** means the mean response to a span gas during a 30 s time interval.
- 3.1.17 **"Specific emissions"** means the mass emissions expressed in g/kWh.
- 3.1.18 **"Test cycle"** means a sequence of test points each with a defined speed and torque to be followed by the engine under steady state (WHSC) or transient operating conditions (WHTC).

- 3.1.19 **"Transformation time"** means the difference in time between the change of the component to be measured at the reference point and a system response of 50 per cent of the final reading (t_{50}) with the sampling probe being defined as the reference point. The transformation time is used for the signal alignment of different measurement instruments.
- 3.1.20 **"Transient test cycle"** means a test cycle with a sequence of normalized speed and torque values that vary relatively quickly with time (WHTC).
- 3.1.21 **"Zero response"** means the mean response to a zero gas during a 30 s time interval.

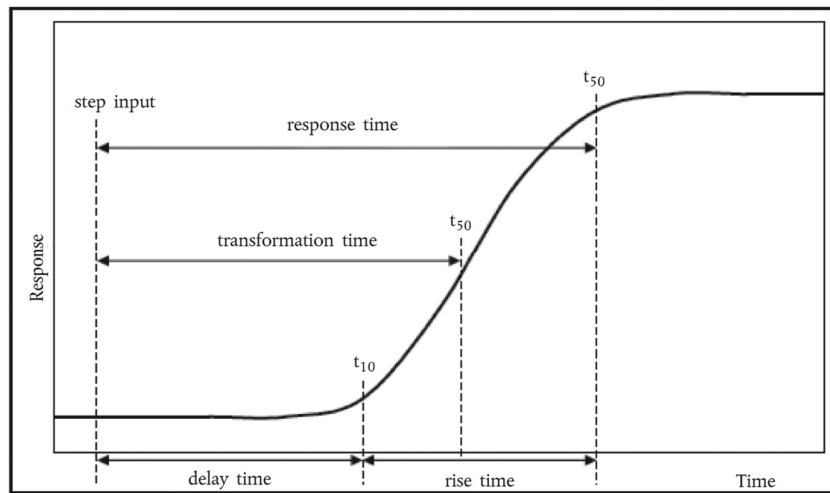


Figure 1
Definition of System Response

3.2 General Symbols

Symbol	Unit	Term
a_1	-	Slope of the regression
a_0	-	y intercept of the regression
A/F_{st}	-	Stoichiometric air to fuel ratio
c	ppm/Vol per cent	Concentration
c_d	ppm/Vol per cent	Concentration on dry basis
c_w	ppm/Vol per cent	Concentration on wet basis
c_b	ppm/Vol per cent	Background concentration
C_d	-	Discharge coefficient of SSV
c_{gas}	ppm/Vol per cent	Concentration on the gaseous components
\bar{c}_s	ppm/Vol per cent	Average concentration of particles from the diluted exhaust gas corrected to standard conditions (273.2 K and 101.33 kPa) particles per cubic centimeter
$c_{s,i}$	Particles per cubic centimeter	A discrete measurement of particle concentration in the diluted gas exhaust from the particle counter, corrected for coincidence and to standard conditions (273.2 K and 101.33 kPa)
d	M	Diameter
d_i		Particle electrical mobility diameter (30, 50 or 100 nm)
d_v	m	Throat diameter of venturi
D_0	m ³ /s	PDP calibration intercept
D	-	Dilution factor
Δt	S	Time interval
e		The number of particles emitted per kWh
e_{gas}	g/kWh	Specific emission of gaseous components

e_{PM}	g/kWh	Specific emission of particulates
e_r	g/kWh	Specific emission during regeneration
e_w	g/kWh	Weighted specific emission
E_{CO_2}	Per cent	CO_2 quench of NO_x analyzer
E_E	Per cent	Ethane efficiency
E_{H_2O}	Per cent	Water quench of NO_x analyzer
E_m	percent	Methane efficiency
E_{NO_x}	Per cent	Efficiency of NO_x converter
f	Hz	Data sampling rate
f_a	-	Laboratory atmospheric factor
F_S	-	Stoichiometric factor
\bar{f}_r	-	Mean particle concentration reduction factor of the volatile particle remover specific to the dilution settings used for the test
H_a	g/kg	Absolute humidity of the intake air
H_d	g/kg	Absolute humidity of the diluent
i	-	Subscript denoting an instantaneous measurement (e.g. 1 Hz)
k	-	Calibration factor to correct the particle number counter measurements to the level of the reference instrument where this is not applied internally within the particle number counter. Where the calibration factor is applied internally within the particle number counter, a value of 1 shall be used for k in the above equation
k_c	-	Carbon specific factor
$k_{f,d}$	m ³ /kg fuel	Combustion additional volume of dry exhaust

$k_{f,w}$	m ³ /kg fuel	Combustion additional volume of wet exhaust
$k_{h,D}$	-	Humidity correction factor for NO x for CI engines
$k_{h,G}$	-	Humidity correction factor for NO x for PI engines
k_r		The regeneration adjustment, according to clause 6.6.2 of this Chapter, or in the case of engines without periodically regenerating after- treatment $k_r = 1$
$k_{r,d}$	-	Downward regeneration adjustment factor
$k_{r,u}$	-	Upward regeneration adjustment factor
$k_{w,a}$	-	Dry to wet correction factor for the intake air
$k_{w,d}$	-	Dry to wet correction factor for the diluent
$k_{w,e}$	-	Dry to wet correction factor for the diluted exhaust gas
$k_{w,r}$	-	Dry to wet correction factor for the raw exhaust gas
K_V	-	CFV calibration function
λ	-	Excess air ratio
m_b	mg	Particulate sample mass of the diluent collected
m_d	kg	Mass of the diluent sample passed through the particulate sampling filters
m_{ed}	kg	Total diluted exhaust mass over the cycle
m_{edf}	kg	Mass of equivalent diluted exhaust gas over the test cycle
m_{ew}	kg	Total exhaust mass over the cycle

m_{ex}	kg	Total mass of diluted exhaust gas extracted from the dilution tunnel for particle number sampling
m_f	mg	Particulate sampling filter mass
m_{gas}	g	Mass of gaseous emissions over the test cycle
m_P	mg	Particulate sample mass collected
m_{PM}	g	Mass of particulate emissions over the test cycle
$m_{PM,corr}$	g/test	Mass of particulates corrected for extraction of particle number sample flow
m_{se}	kg	Exhaust sample mass over the test cycle
m_{sed}	kg	Mass of diluted exhaust gas passing the dilution tunnel
m_{sep}	kg	Mass of diluted exhaust gas passing the particulate collection filters
m_{ssd}	kg	Mass of secondary diluent
M	Nm	Torque
M_a	g/mol	Molar mass of the intake air
M_d	g/mol	Molar mass of the diluent
M_e	g/mol	Molar mass of the exhaust
M_f	Nm	Torque absorbed by auxiliaries/equipment to be fitted
M_{gas}	g/mol	Molar mass of gaseous components
M_r	Nm	Torque absorbed by auxiliaries/equipment to be removed
N	-	Number of particles emitted over the test cycle
n	-	Number of measurements
n_r	-	Number of measurements with regeneration

n	min^{-1}	Engine rotational speed
n_{hi}	min^{-1}	High engine speed
n_{lo}	min^{-1}	Low engine speed
n_{pref}	min^{-1}	Preferred engine speed
n_p	r/s	PDP pump speed
N_{cold}	-	The total number of particles emitted over the WHTC cold test cycle
N_{hot}	-	The total number of particles emitted over the WHTC hot test cycle
N_{in}	-	Upstream particle number concentration
N_{out}	-	Downstream particle number concentration
p_a	kPa	Saturation vapour pressure of engine intake air
p_b	kPa	Total atmospheric pressure
p_d	kPa	Saturation vapour pressure of the diluent
p_p	kPa	Absolute pressure
p_r	kPa	Water vapour pressure after cooling bath
p_s	kPa	Dry atmospheric pressure
P	kW	Power
P_f	kW	Power absorbed by auxiliaries/ equipment to be fitted
P_r	kW	Power absorbed by auxiliaries/ equipment to be removed
q_{ex}	kg/s	Particle number sample mass flow rate
q_{mad}		Intake air mass flow rate on dry basis

q_{maw}	kg/s	Intake air mass flow rate on wet basis
q_{mCe}	kg/s	Carbon mass flow rate in the raw exhaust gas
q_{mCf}	kg/s	Carbon mass flow rate into the engine
q_{mCp}	kg/s	Carbon mass flow rate in the partial flow dilution system
q_{mdew}	kg/s	Diluted exhaust gas mass flow rate on wet basis
q_{mdw}	kg/s	Diluent mass flow rate on wet basis
q_{medf}	kg/s	Equivalent diluted exhaust gas mass flow rate on wet basis
q_{mew}	kg/s	Exhaust gas mass flow rate on wet basis
q_{mex}	kg/s	Sample mass flow rate extracted from dilution tunnel
q_{mf}	kg/s	Fuel mass flow rate
q_{mp}	kg/s	Sample flow of exhaust gas into partial flow dilution system
q_{sw}	kg/s	Mass flow rate fed back into dilution tunnel to compensate for particle number sample extraction
q_{vCVS}	m ³ /s	CVS volume rate
q_{vs}	dm ³ /min	System flow rate of exhaust analyzer system
q_{vt}	cm ³ /min	Tracer gas flow rate
r^2	-	Coefficient of determination
r_d	-	Dilution ratio
r_D	-	Diameter ratio of SSV
r_h	-	Hydrocarbon response factor of the FID
r_m	-	Methanol response factor of the FID

r_p	-	Pressure ratio of SSV
r_s	-	Average sample ratio
s		Standard deviation
ρ	kg/m ³	Density
ρ_e	kg/m ³	Exhaust gas density
σ	-	Standard deviation
T	K	Absolute temperature
T_a	K	Absolute temperature of the intake air
t	S	Time
t_{10}	S	Time between step input and 10 per cent of final reading
t_{50}	S	Time between step input and 50 per cent of final reading
t_{90}	S	Time between step input and 90 per cent of final reading
u	-	Ratio between the densities (or molar masses) of the gas components and the exhaust gas divided by 1,000
V_0	m ³ /r	PDP gas volume pumped per revolution
V_s	dm ³	System volume of exhaust analyzer bench
W_{act}	kWh	Actual cycle work of the test cycle
$W_{act,cold}$	kWh	The actual cycle work over the WHTC cold test cycle according to clause 7.8.6. of this Chapter.
$W_{act,hot}$	kWh	The actual cycle work over the WHTC hot test cycle according to clause 7.8.6. of this Chapter
W_{ref}	kWh	Reference cycle work of the test cycle
X_0	m ³ /r	PDP calibration function

3.3 Symbols and Abbreviations for The Fuel Composition

w_{ALF} Hydrogen content of fuel, per cent mass

w_{BET} Carbon content of fuel, per cent mass

w_{GAM} Sulphur content of fuel, per cent mass

w_{DEL} Nitrogen content of fuel, per cent mass

w_{EPS} Oxygen content of fuel, per cent mass

α Molar hydrogen ratio (H/C)

γ Molar sulphur ratio (S/C)

δ Molar nitrogen ratio (N/C)

ε Molar oxygen ratio (O/C)

referring to a fuel $CH_\alpha O_\varepsilon N_\delta S_\gamma$

3.4 Symbols and abbreviations for the chemical components

C1 Carbon 1 equivalent hydrocarbon

CH₄ Methane

C₂H₆ Ethane

C₃H₈ Propane

CO Carbon monoxide

CO₂ Carbon dioxide

DOP Di-octylphtalate

HC Hydrocarbons

H₂O Water

NMHC Non-methane hydrocarbons

NO_x Oxides of nitrogen

NO Nitric oxide

NO₂ Nitrogen dioxide

PM Particulate matter

Abbreviations

CFV	Critical flow venturi
CLD	Chemiluminescent detector
CVS	Constant volume sampling
deNO _x	NO _x after-treatment system
EGR	Exhaust gas recirculation
ET	Evaporation tube
FID	Flame ionization detector
FTIR	Fourier transform infrared analyser
GC	Gas chromatograph
HCLD	Heated chemiluminescent detector
HFID	Heated flame ionization detector
LDS	Laser diode spectrometer
LPG	Liquefied petroleum gas
NDIR	Non-dispersive infrared (analyzer)
NG	Natural gas
NMC	Non-methane cutter
OT	Outlet tube
PDP	Positive displacement pump
Per cent FS	Per cent of full scale
PCF	Particle pre-classifier
PFS	Partial flow system
PNC	Particle number counter
PND	Particle number diluter
PTS	Particle transfer system
PTT	Particle transfer tube
SSV	Subsonic venturi
VGT	Variable geometry turbine
VPR	Volatile particle remover
WHSC	World Harmonised Steady State Cycle
WHTC	World Harmonised Transient Cycle

4.0 GENREAL REQUIREMENTS

- 4.1** The engine system shall be so designed, constructed and assembled as to enable the engine in normal use to comply with the provisions of this Chapter during its useful life, as defined in this Part, including when installed in the vehicle.

5.0 PERFORMANCE REQUIREMENT

5.1 The Emissions of Gaseous and Particulate Pollutants

The emissions of gaseous and particulate pollutants by the engine shall be determined on the WHTC and WHSC test cycles, as described in clause 7. of this Chapter. The measurement systems shall meet the linearity requirements in clause 9.2 and the specifications in clause 9.3 (gaseous emissions measurement), clause 9.4 (particulate measurement) and in Appendix 2 of this Chapter.

Other systems or analyzers may be approved by the Test Agency, if it is found that they yield equivalent results in accordance with clause 5.1.1. of this Chapter.

5.1.1 Equivalency

The determination of system equivalency shall be based on a seven-sample pair (or larger) correlation study between the system under consideration and one of the systems of this Chapter. "Results" refer to the specific cycle weighted emissions value. The correlation testing is to be performed at the same laboratory, test cell, and on the same engine, and is preferred to be run concurrently. The equivalency of the sample pair averages shall be determined by F-test and t-test statistics as described in Appendix 3 of this Chapter, clause A.3.3, obtained under the laboratory test cell and the engine conditions described above. Outliers shall be determined in accordance with ISO 5725 and excluded from the database. The systems to be used for correlation testing shall be subject to the approval by the Test Agency.

5.2 Engine Family

5.2.1 General:

An engine family is characterized by design parameters. These shall be common to all engines within the family. The engine manufacturer may decide which engines belong to an engine family, as long as the membership criteria listed in clause 5.2.3 are respected. The engine family shall be approved by the Test Agency. The manufacturer shall provide to the Test Agency the appropriate information relating to the emission levels of the members of the engine family.

5.2.2 Special Cases

In some cases, there may be interaction between parameters. This shall be taken into consideration to ensure that only engines with similar exhaust emission characteristics are included within the same engine family. These cases shall be identified by the manufacturer and notified

to the Test Agency. It shall then be taken into account as a criterion for creating a new engine family.

In case of devices or features, which are not listed in clause 5.2.3 and which have a strong influence on the level of emissions, this equipment shall be identified by the manufacturer on the basis of good engineering

practice, and shall be notified to the Test Agency. It shall then be taken into account as a criterion for creating a new engine family.

In addition to the parameters listed in clause 5.2.3 of this Chapter, the manufacturer may introduce additional criteria allowing the definition of families of more restricted size. These parameters are not necessarily parameters that have an influence on the level of emissions

5.2.3 Parameters Defining the Engine Family

5.2.3.1 Combustion cycle

- a) 2-stroke cycle;
- b) 4-stroke cycle;
- c) Rotary engine;
- d) Others.

5.2.3.2 Configuration of the cylinders

5.2.3.2.1 Position of the cylinders in the block

- a) V;
- b) In line;
- c) Radial;
- d) Others (F, W, etc.).

5.2.3.2.2 Relative position of the cylinders

Engines with the same block may belong to the same family as long as their bore center-to-center dimensions are the same

5.2.3.3 Main cooling medium:

- a) Air;
- b) Water;
- c) Oil.

5.2.3.4 Individual cylinder displacement

5.2.3.4.1 Engine with a unit cylinder displacement $\geq 0.75 \text{ dm}^3$

In order for engines with a unit cylinder displacement of $\geq 0.75 \text{ dm}^3$ to be considered to belong to the same engine family, the spread of their individual cylinder displacements shall not exceed 15 per cent of the largest individual cylinder displacement within the family.

5.2.3.4.2 Engine with a unit cylinder displacement $< 0.75 \text{ dm}^3$

In order for engines with a unit cylinder displacement of $< 0.75 \text{ dm}^3$ to be considered to belong to the same engine family, the spread of their individual cylinder displacements shall not exceed 30 per cent of the largest individual cylinder displacement within the family.

5.2.3.4.3 Engine with other unit cylinder displacement limits

Engines with an individual cylinder displacement that exceeds the limits defined in clauses 5.2.3.4.1 and 5.2.3.4.2 may be considered to belong to the same family with the approval of the Test Agency. The approval shall be based on technical elements (calculations, simulations, experimental results etc.) showing that exceeding the limits does not have a significant influence on the exhaust emissions.

5.2.3.5 Method of air aspiration

- a) Naturally aspirated;
- b) Pressure charged;
- c) Pressure charged with charge cooler.

5.2.3.6 Fuel type

- a) Diesel;
- b) Natural gas (NG);
- c) Liquefied petroleum gas (LPG);
- d) Ethanol.

5.2.3.7 Combustion chamber type

- a) Open chamber;
- b) Divided chamber;
- c) Other types

5.2.3.8 Ignition Type

- a) Positive ignition;
- b) Compression ignition.

5.2.3.9 Valves and porting

- a) Configuration;
- b) Number of valves per cylinder.

5.2.3.10 Fuel supply type

- a) Liquid fuel supply type:
 - i) Pump and (high pressure) line and injector;
 - ii) In-line or distributor pump;
 - iii) Unit pump or unit injector;
 - iv) Common rail;
 - v) Carburetor(s);
 - vi) others

b) Gas fuel supply type

- i) Gaseous;
- ii) Liquid;
- iii) Mixing units;
- iv) Others

c) other types

5.2.3.11 **Miscellaneous devices**

- a) Exhaust gas recirculation (EGR);
- b) Water injection;
- c) Air injection;
- d) Others.

5.2.3.12 **Electronic control strategy**

The presence or absence of an electronic control unit (ECU) on the engine is regarded as a basic parameter of the family.

In the case of electronically controlled engines, the manufacturer shall present the technical elements explaining the grouping of these engines in the same family, i.e. the reasons why these engines can be expected to satisfy the same emission requirements.

These elements can be calculations, simulations, estimations, description of injection parameters, experimental results, etc.

Examples of controlled features are

- a) Timing;
- b) Injection pressure;
- c) Multiple injections;
- d) Boost pressure;
- e) VGT
- f) EGR

5.2.3.13 **Exhaust after-treatment systems**

The function and combination of the following devices are regarded as membership criteria for an engine family:

- a) Oxidation catalyst;
- b) Three-way catalyst;
- c) de NO_x system with selective reduction of NO_x (addition of reducing agent);
- d) Other de NO_x systems;
- e) Particulate trap with passive regeneration;

- f) Particulate trap with active regeneration;
- g) Other particulate traps;
- h) Other devices.

When an engine has been certified without an after-treatment system, whether as parent engine or as member of the family, then this engine, when equipped with an oxidation catalyst, may be included in the same engine family, if it does not require different fuel characteristics.

If it requires specific fuel characteristics (e.g. particulate traps requiring special additives in the fuel to ensure the regeneration process), the decision to include it in the same family shall be based on technical elements provided by the manufacturer. These elements shall indicate that the expected emission level of the equipped engine complies with the same limit value as the non-equipped engine.

When an engine has been certified with an after-treatment system, whether as parent engine or as member of a family, whose parent engine is equipped with the same after-treatment system, then this engine, when equipped without after-treatment system, shall not be added to the same engine family

5.2.4 **Choice of the Parent Engine**

5.2.4.1 **Compression ignition engines**

Once the engine family has been agreed by the Test Agency, the parent engine of the family shall be selected using the primary criterion of the highest fuel delivery per stroke at the declared maximum torque speed. In the event that two or more engines share this primary criterion, the parent engine shall be selected using the secondary criterion of highest fuel delivery per stroke at rated speed.

5.2.4.2 **Positive ignition engines**

Once the engine family has been agreed by the Test Agency, the parent engine of the family shall be selected using the primary criterion of the largest displacement. In the event that two or more engines share this primary criterion, the parent engine shall be selected using the secondary criterion in the following order of priority:

- a) The highest fuel delivery per stroke at the speed of declared rated power;
- b) The most advanced spark timing;
- c) The lowest EGR rate.

5.2.4.3 Remarks on the choice of the Parent Engine

The Test Agency may conclude that the worst-case emission of the family can best be characterized by testing additional engines. In this case, the engine manufacturer shall submit the appropriate information to determine the engines within the family likely to have the highest emissions level.

If engines within the family incorporate other features which may be considered to affect exhaust emissions, these features shall also be identified and taken into account in the selection of the parent engine.

If engines within the family meet the same emission values over different useful life periods, this shall be taken into account in the selection of the parent engine

6.0 TEST CONDITIONS

6.1 Laboratory Test Conditions

The absolute temperature (T_a) of the engine intake air expressed in Kelvin, and the dry atmospheric pressure (p_s), expressed in kPa shall be measured and the parameter f_a shall be determined according to the following provisions. In multi-cylinder engines having distinct groups of intake manifolds, such as in a "Vee" engine configuration, the average temperature of the distinct groups shall be taken. The parameter f_a shall be reported with the test results. For better repeatability and reproducibility of the test results, it is recommended that the parameter f_a be such that: $0.93 \leq f_a \leq 1.07$.

a) Compression-ignition engines:

Naturally aspirated and mechanically supercharged engines:

$$f_a = \left(\frac{99}{p_s}\right) \times \left(\frac{T_a}{298}\right)^{0.7} \quad (1)$$

Turbocharged engines with or without cooling of the intake air:

$$f_a = \left(\frac{99}{p_s}\right)^{0.7} \times \left(\frac{T_a}{298}\right)^{1.5} \quad (2)$$

b) Positive ignition engines

$$f_a = \left(\frac{99}{p_s}\right)^{1.2} \times \left(\frac{T_a}{298}\right)^{0.6} \quad (3)$$

6.2 Engines with charge air-cooling

The charge air temperature shall be recorded and shall be, at the rated speed and full load, within ± 5 K of the maximum charge air temperature specified by the manufacturer. The temperature of the cooling medium shall be at least 293 K (20 °C).

If a test laboratory system or external blower is used, the coolant flow rate shall be set to achieve a charge air temperature within ± 5 K of the maximum charge air temperature specified by the manufacturer at the

rated speed and full load. Coolant temperature and coolant flow rate of the charge air cooler at the above set point shall not be changed for the whole test cycle, unless this results in unrepresentative overcooling of the charge air. The charge air cooler volume shall be based upon good engineering practice and shall be representative of the production engine's in-use installation. The laboratory system shall be designed to minimize accumulation of condensate. Any accumulated condensate shall be drained and all drains shall be completely closed before emission testing.

If the engine manufacturer specifies pressure-drop limits across the charge-air cooling system, it shall be ensured that the pressure drop across the charge-air cooling system at engine conditions specified by the manufacturer is within the manufacturer's specified limit(s). The pressure drop shall be measured at the manufacturer's specified locations.

6.3 Engine Power

The basis of specific emissions measurement is engine power and cycle work as determined in accordance with clauses 6.3.1 to 6.3.5. of this Chapter.

6.3.1 General engine installation

The engine shall be tested with the auxiliaries/equipment listed in Appendix 6 of this Chapter.

If auxiliaries/equipment are not installed as required, their power shall be taken into account in accordance with clauses 6.3.2 to 6.3.5. of this Chapter.

6.3.2 Auxiliaries/Equipment to Be Fitted for the Emissions Test

If it is inappropriate to install the auxiliaries/equipment required according to Appendix 6 of this Chapter on the test bench, the power absorbed by them shall be determined and subtracted from the measured engine power (reference and actual) over the whole engine speed range of the WHTC and over the test speeds of the WHSC.

6.3.3 Auxiliaries/Equipment to Be Removed for the Test

Where the auxiliaries/equipment not required according to Appendix 6 of this Chapter cannot be removed, the power absorbed by them may be determined and added to the measured engine power (reference and actual) over the whole engine speed range of the WHTC and over the test speeds of the WHSC. If this value is greater than 3 per cent of the maximum power at the test speed it shall be demonstrated to the Test Agency.

6.3.4 Determination of Auxiliary Power

The power absorbed by the auxiliaries/equipment needs only be determined, if:

- (a) Auxiliaries/equipment required according to Appendix 6 of this Chapter, are not fitted to the engine; and/or
- (b) Auxiliaries/equipment not required according to Appendix 6 of this Chapter, are fitted to the engine.

The values of auxiliary power and the measurement/calculation method for determining auxiliary power shall be submitted by the engine manufacturer for the whole operating area of the test cycles, and approved by the Test Agency.

6.3.5 Engine Cycle Work

The calculation of reference and actual cycle work (see clauses 7.4.8 and 7.8.6 of this Chapter) shall be based upon engine power according to clause 6.3.1. In this case, P_f and P_r of equation 4 are zero, and P equals P_m .

If auxiliaries/equipment are installed according to clauses 6.3.2 and/or 6.3.3., the power absorbed by them shall be used to correct each instantaneous cycle power value $P_{m,i}$, as follows:

$$P_i = P_{m,i} - P_{f,i} + P_{r,i} \quad (4)$$

Where:

$P_{m,i}$ is the measured engine power, kW

$P_{f,i}$ is the power absorbed by auxiliaries/equipment to be fitted, kW

$P_{r,i}$ is the power absorbed by auxiliaries/equipment to be removed, kW.

6.4 Engine Air Intake System

An engine air intake system or a test laboratory system shall be used presenting an air intake restriction within ± 300 Pa of the maximum value specified by the manufacturer for a clean air cleaner at the rated speed and full load. The static differential pressure of the restriction shall be measured at the location specified by the manufacturer.

6.5 Engine Exhaust System

An engine exhaust system or a test laboratory system shall be used presenting an exhaust backpressure within 80 to 100 per cent of the maximum value specified by the manufacturer at the rated speed and full load. If the maximum restriction is 5 kPa or less, the set point shall be no less than 1.0 kPa from the maximum. The exhaust system shall conform to the requirements for exhaust gas sampling, as set out in clauses 9.3.10 and 9.3.11 of this Chapter.

6.6 Engine with exhaust after-treatment system

If the engine is equipped with an exhaust after-treatment system, the exhaust pipe shall have the same diameter as found in-use, or as specified by the manufacturer, for at least four pipe diameters upstream of the expansion section containing the after-treatment device. The distance from the exhaust manifold flange or turbocharger outlet to the exhaust after-treatment system shall be the same as in the vehicle configuration or within the distance specifications of the manufacturer. The exhaust backpressure or restriction shall follow the same criteria as above, and may be set with a valve. For variable-restriction after-treatment devices, the maximum exhaust restriction is defined at the after-treatment condition (degreening/ageing and regeneration/loading level) specified by the manufacturer. If the maximum restriction is 5 kPa or less, the set point shall be no less than 1.0 kPa from the maximum. The after-treatment container may be removed during dummy tests and during engine mapping, and replaced with an equivalent container having an inactive catalyst support.

The emissions measured on the test cycle shall be representative of the emissions in the field. In the case of an engine equipped with an exhaust after-treatment system that requires the consumption of a reagent, the reagent used for all tests shall be declared by the manufacturer.

Engines equipped with exhaust after-treatment systems with continuous regeneration do not require a special test procedure, but the regeneration process needs to be demonstrated according to clause 6.6.1. of this Chapter.

For engines equipped with exhaust after-treatment systems that are regenerated on a periodic basis, as described in clauses 6.6.2 of this Chapter, emission results shall be adjusted to account for regeneration events. In this case, the average emission depends on the frequency of the regeneration event in terms of fraction of tests during which the regeneration occurs.

6.6.1 Continuous Regeneration

The emissions shall be measured on an after-treatment system that has been stabilized so as to result in repeatable emissions behavior. The regeneration process shall occur at least once during the WHTC hot start test and the manufacturer shall declare the normal conditions under which regeneration occurs (soot load, temperature, exhaust back-pressure, etc.).

In order to demonstrate that the regeneration process is continuous, at least three WHTC hot start tests shall be conducted. For the purpose of this demonstration, the engine shall be warmed up in accordance with clause 7.4.1 of this Chapter, the engine be soaked according to clause 7.6.3 of this Chapter and the first WHTC hot start test be run. The subsequent hot start tests shall be started after soaking according to clause 7.6.3 of this Chapter. During the tests, exhaust temperatures and

pressures shall be recorded (temperature before and after the after-treatment system, exhaust back pressure, etc.).

If the conditions declared by the manufacturer occur during the tests and the results of the three (or more) WHTC hot start tests do not scatter by more than ± 25 per cent or 0.005 g/kWh, whichever is greater, the after-treatment system is considered to be of the continuous regeneration type, and the general test provisions of clause 7.6 (WHTC) and clause 7.7 (WHSC) of this Chapter apply.

If the exhaust after-treatment system has a security mode that shifts to a periodic regeneration mode, it shall be checked according to clause 6.6.2. For that specific case, the applicable emission limits may be exceeded and would not be weighted.

6.6.2 Periodic Regeneration

For an exhaust after-treatment based on a periodic regeneration process, the emissions shall be measured on at least three WHTC hot start tests, one with and two without a regeneration event on a stabilized after-treatment system, and the results be weighted in accordance with equation 5.

The regeneration process shall occur at least once during the WHTC hot start test. The engine may be equipped with a switch capable of preventing or permitting the regeneration process provided this operation has no effect on the original engine calibration.

The manufacturer shall declare the normal parameter conditions under which the regeneration process occurs (soot load, temperature, exhaust back-pressure, etc.) and its duration. The manufacturer shall also provide the frequency of the regeneration event in terms of number of tests during which the regeneration occurs compared to number of tests without regeneration. The exact procedure to determine this frequency shall be based upon in-use data using good engineering judgment, and shall be agreed by the Test Agency.

The manufacturer shall provide an after-treatment system that has been loaded in order to achieve regeneration during a WHTC test. For the purpose of this testing, the engine shall be warmed up in accordance with clause 7.4.1 of this Chapter, the engine be soaked according to clause 7.6.3 of this Chapter and the WHTC hot start test be started. Regeneration shall not occur during the engine warm-up.

Average specific emissions between regeneration phases shall be determined from the arithmetic mean of several approximately equidistant WHTC hot start test results (g/kWh). As a minimum, at least one WHTC hot start test as close as possible prior to a regeneration test and one WHTC hot start test immediately after a regeneration test shall be conducted. As an alternative, the manufacturer may provide data to show that the emissions remain constant (± 25 per cent or 0.005 g/kWh, whichever is greater) between regeneration phases. In this case, the emissions of only one WHTC hot start test may be used.

During the regeneration test, all the data needed to detect regeneration shall be recorded (CO or NO_x emissions, temperature before and after the after-treatment system, exhaust back pressure, etc.).

During the regeneration test, the applicable emission limits may be exceeded.

The test procedure is schematically shown in Figure 2.

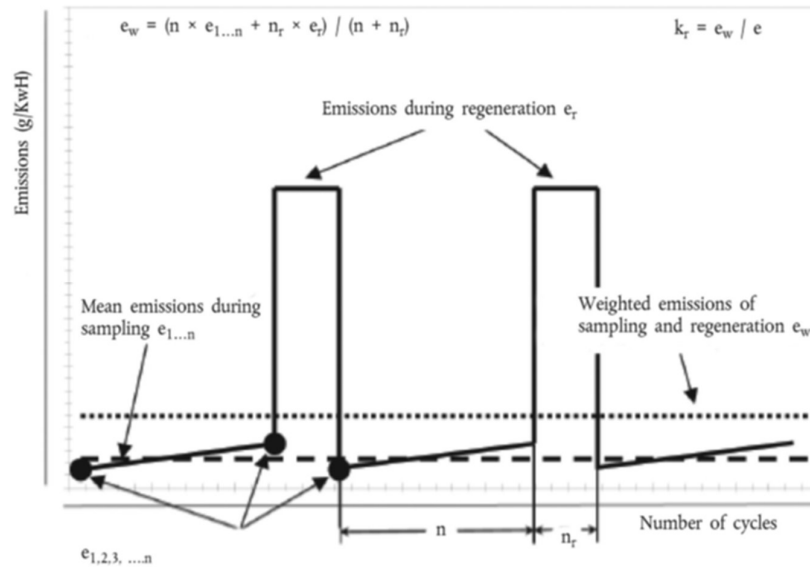


Figure 2
Scheme of Periodic Regeneration

The WHTC hot start emissions shall be weighted as follows:

$$e_w = \frac{n \times \bar{e} + n_r \times \bar{e}_r}{n + n_r} \quad (5)$$

Where:

n	is the number of WHTC hot start tests without regeneration
n_r	is the number of WHTC hot start tests with regeneration (minimum one test)
\bar{e}	is the average specific emission without regeneration, g/kWh
\bar{e}_r	is the average specific emission with regeneration, g/kWh

For the determination of \bar{e}_r , the following provisions apply:

- If regeneration takes more than one hot start WHTC, consecutive full hot start WHTC tests shall be conducted and emissions continued to be measured without soaking and without shutting the engine off, until regeneration is completed, and the average of the hot start WHTC tests be calculated;

- (b) If regeneration is completed during any hot start WHTC, the test shall be continued over its entire length.

In agreement with the Test Agency, the regeneration adjustment factors may be applied either multiplicative (c) or additive (d) based upon good engineering analysis.

- (c) The multiplicative adjustment factors shall be calculated as follows:

$$k_{r,u} = \frac{e_w}{e} \text{ (upward)} \quad (6)$$

$$k_{r,d} = \frac{e_w}{e_r} \text{ (downward)} \quad (6a)$$

- (d) The additive adjustment factors shall be calculated as follows:

$$k_{r,u} = e_w - e \text{ (upward)} \quad (7)$$

$$k_{r,d} = e_w - e_r \text{ (downward)} \quad (8)$$

With reference to the specific emission calculations in clause 8.6.3 of this Chapter, the regeneration adjustment factors shall be applied, as follows:

- (e) For a test without regeneration, $k_{r,u}$ shall be multiplied with or be added to, respectively, the specific emission e in equations 69 or 70 of clause 8.6.3 of this Chapter;
- (f) For a test with regeneration, $k_{r,d}$ shall be multiplied with or be added to, respectively, the specific emission e in equations 69 or 70 of clause 8.6.3. of this Chapter

At the request of the manufacturer, the regeneration adjustment factors

- (g) May be extended to other members of the same engine family;
- (h) May be extended to other engine families using the same after-treatment system with the prior approval of the Test Agency based on technical evidence to be supplied by the manufacturer, that the emissions are similar.

6.7 Cooling System

An engine cooling system with sufficient capacity to maintain the engine at normal operating temperatures prescribed by the manufacturer shall be used.

6.8 Lubricating System

The lubricating oil shall be specified by the manufacturer and be representative of lubricating oil available on the market; the specifications of the lubricating oil used for the test shall be recorded and presented with the results of the test.

6.9 Specification of the reference fuel

The reference fuels are specified in Chapter 4 of this Part.

The fuel temperature shall be in accordance with the manufacturer's recommendations.

6.10 Crankcase Emissions

No crankcase emissions shall be discharged directly into the ambient atmosphere, with the following exception: engines equipped with turbochargers, pumps, blowers, or superchargers for air induction may discharge crankcase emissions to the ambient atmosphere if the emissions are added to the exhaust emissions (either physically or mathematically) during all emission testing. Manufacturers taking advantage of this exception shall install the engines so that all crankcase emission can be routed into the emissions sampling system.

For the purpose of this paragraph, crankcase emissions that are routed into the exhaust upstream of exhaust after-treatment during all operation are not considered to be discharged directly into the ambient atmosphere.

Open crankcase emissions shall be routed into the exhaust system for emission measurement, as follows:

- (a) The tubing materials shall be smooth-walled, electrically conductive, and not reactive with crankcase emissions. Tube lengths shall be minimized as far as possible;
- (b) The number of bends in the laboratory crankcase tubing shall be minimized, and the radius of any unavoidable bend shall be maximized;
- (c) The laboratory crankcase exhaust tubing shall be heated, thin-walled or insulated and shall meet the engine manufacturer's specifications for crankcase back pressure;
- (d) The crankcase exhaust tubing shall connect into the raw exhaust downstream of any after-treatment system, downstream of any installed exhaust restriction, and sufficiently upstream of any sample probes to ensure complete mixing with the engine's exhaust before sampling. The crankcase exhaust tube shall extend into the free stream of exhaust to avoid boundary-layer effects and to promote mixing. The crankcase exhaust tube's outlet may orient in any direction relative to the raw exhaust flow.

6.11 Clause 6.11.1 and 6.11.2 shall apply to positive-ignition engines fuelled with petrol or E85.

- 6.11.1 The pressure in the crankcase shall be measured over the emissions test cycles at an appropriate location. It shall be measured at the dip-stick hole with an inclined-tube manometer.

- 6.11.1.1 The pressure in the intake manifold shall be measured to within ± 1 kPa.
- 6.11.1.2 The pressure measured in the crankcase shall be measured to within ± 0.01 kPa.
- 6.11.2 Compliance with clause 6.10 of this Chapter shall be deemed satisfactory if, in every condition of measurement set out in clause 6.11.1, the pressure measured in the crankcase does not exceed the atmospheric pressure prevailing at the time of measurement.

7.0 TEST PROCEDURES

7.1 Principles of Emissions Measurement

To measure the specific emissions, the engine shall be operated over the test cycles defined in clauses 7.2.1 and 7.2.2. The measurement of specific emissions requires the determination of the mass of components in the exhaust and the corresponding engine cycle work. The components are determined by the sampling methods described in clauses 7.1.1 and 7.1.2.

7.1.1 Continuous Sampling

In continuous sampling, the component's concentration is measured continuously from raw or dilute exhaust. This concentration is multiplied by the continuous (raw or dilute) exhaust flow rate at the emission sampling location to determine the component's mass flow rate. The component's emission is continuously summed over the test cycle. This sum is the total mass of the emitted component.

7.1.2 Batch Sampling

In batch sampling, a sample of raw or dilute exhaust is continuously extracted and stored for later measurement. The extracted sample shall be proportional to the raw or dilute exhaust flow rate. Examples of batch sampling are collecting diluted gaseous components in a bag and collecting particulate matter (PM) on a filter. The batch sampled concentrations are multiplied by the total exhaust mass or mass flow (raw or dilute) from which it was extracted during the test cycle. This product is the total mass or mass flow of the emitted component. To calculate the PM concentration, the PM deposited onto a filter from proportionally extracted exhaust shall be divided by the amount of filtered exhaust.

7.1.3 Measurement Procedures

This Chapter applies two measurement procedures that are functionally equivalent. Both procedures may be used for both the WHTC and the WHSC test cycle:

- (a) The gaseous components are sampled continuously in the raw exhaust gas, and the particulates are determined using a partial flow dilution system;

- (b) The gaseous components and the particulates are determined using a full flow dilution system (CVS system).

Any combination of the two principles (e.g. raw gaseous measurement and full flow particulate measurement) is permitted.

7.2 Test Cycles

7.2.1 The Transient Test Cycle WHTC

The transient test cycle WHTC is listed in Appendix 1 of this Chapter as a second-by-second sequence of normalized speed and torque values. In order to perform the test on an engine test cell, the normalized values shall be converted to the actual values for the individual engine under test based on the engine-mapping curve. The conversion is referred to as denormalization, and the test cycle so developed as the reference cycle of the engine to be tested. With those references speed and torque values, the cycle shall be run on the test cell, and the actual speed, torque and power values shall be recorded. In order to validate the test, run, a regression analysis between reference and actual speed, torque and power values shall be conducted upon completion of the test.

For calculation of the brake specific emissions, the actual cycle work shall be calculated by integrating actual engine power over the cycle. For cycle validation, the actual cycle work shall be within prescribed limits of the reference cycle work.

For the gaseous pollutants, continuous sampling (raw or dilute exhaust gas) or batch sampling (dilute exhaust gas) may be used. The particulate sample shall be diluted with a conditioned diluent (such as ambient air), and collected on a single suitable filter. The WHTC is shown schematically in Figure 3 below.

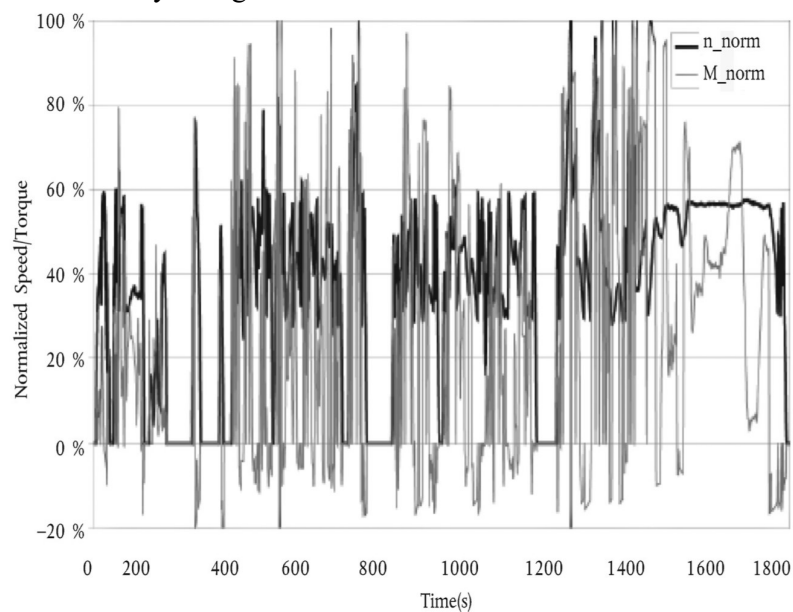


Figure 3
WHTC Test Cycle

7.2.2 Ramped steady state test cycle WHSC

The ramped steady state test cycle WHSC consists of a number of normalized speed and load modes which shall be converted to the reference values for the individual engine under test based on the engine-mapping curve. The engine shall be operated for the prescribed time in each mode, whereby engine speed and load shall be changed linearly within 20 ± 1 seconds. In order to validate the test run, a regression analysis between reference and actual speed, torque and power values shall be conducted upon completion of the test.

The concentration of each gaseous pollutant, exhaust flow and power output shall be determined over the test cycle. The gaseous pollutants may be recorded continuously or sampled into a sampling bag. The particulate sample shall be diluted with a conditioned diluent (such as ambient air). One sample over the complete test procedure shall be taken, and collected on a single suit filter.

For calculation of the brake specific emissions, the actual cycle work shall be calculated by integrating actual engine power over the cycle.

The WHSC is shown in Table 1 below. Except for mode 1, the start of each mode is defined as the beginning of the ramp from the previous mode.

Table 1
WHSC Test Cycle

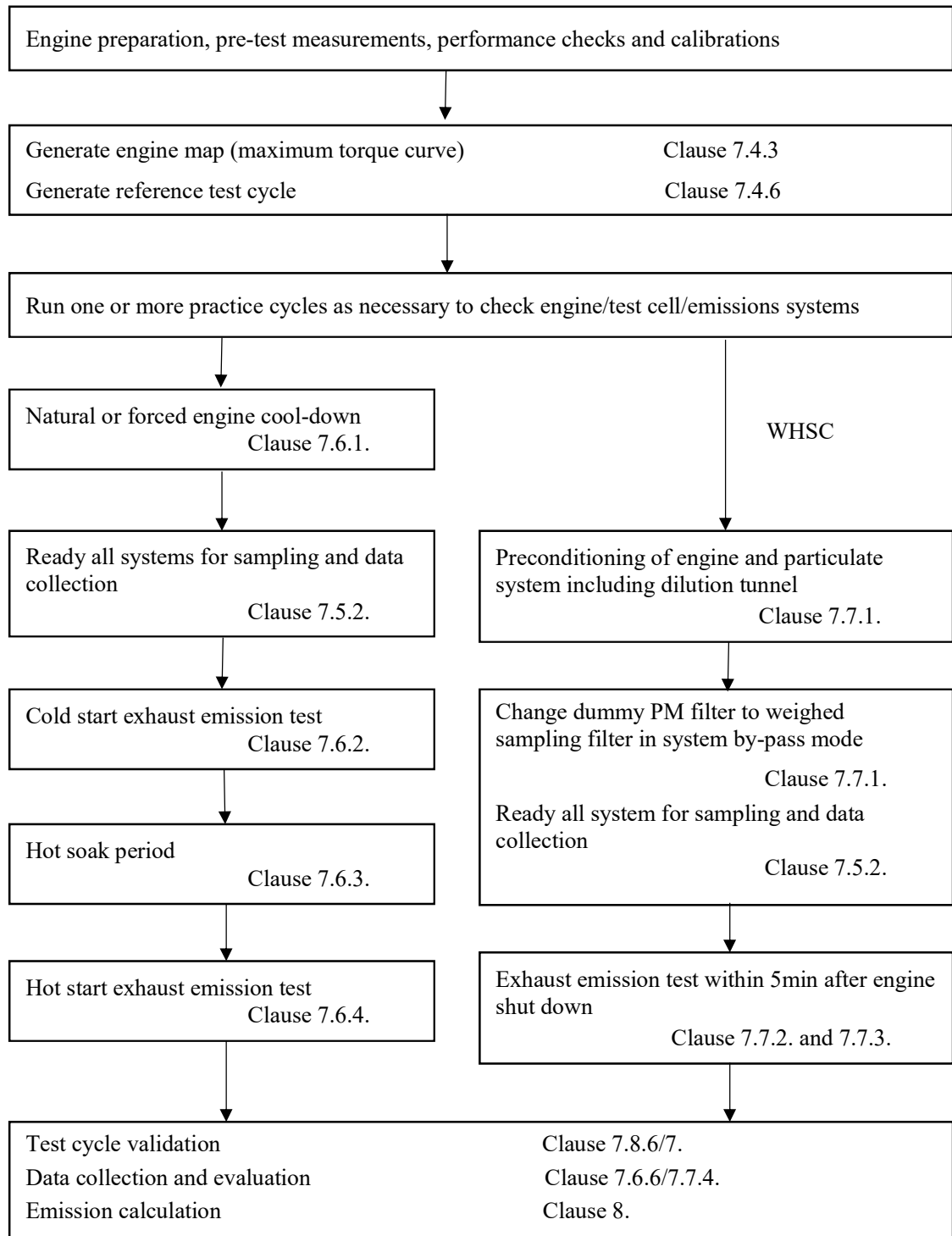
Mode	Normalized speed (per cent)	Normalized torque (per cent)	Mode length(s) incl. 20s ramp
1	0	0	210
2	55	100	50
3	55	25	250
4	55	70	75
5	35	100	50
6	25	25	200
7	45	70	75
8	45	25	150
9	55	50	125
10	75	100	50
11	35	50	200
12	35	25	250
13	0	0	210
sum			1895

7.3 General Test Sequence

The following flow chart outlines the general guidance that should be followed during testing. The details of each step are described in the relevant clauses. Deviations from the guidance are permitted where appropriate, but the specific requirements of the relevant clauses are mandatory.

For the WHTC, the test procedure consists of a cold start test following either natural or forced cool-down of the engine, a hot soak period and a hot start test.

For the WHSC, the test procedure consists of a hot start test following engine preconditioning at WHSC mode 9



7.4 Engine mapping and Reference Cycle

Pre-test engine measurements, pre-test engine performance checks and pre-test system calibrations shall be made prior to the engine mapping procedure in line with the general test sequence shown in clause 7.3. of this Chapter.

As basis for WHTC and WHSC reference cycle generation, the engine shall be mapped under full load operation for determining the speed vs. maximum torque and speed vs. maximum power curves. The mapping curve shall be used for denormalizing engine speed (clause 7.4.6) and engine torque (clause 7.4.7).

7.4.1 Engine warm-up

The engine shall be warmed up between 75 per cent and 100 per cent of its maximum power or according to the recommendation of the manufacturer and good engineering judgment. Towards the end of the warm up it shall be operated in order to stabilize the engine coolant and lube oil temperatures to within ± 2 per cent of its mean values for at least 2 minutes or until the engine thermostat controls engine temperature.

7.4.2 Determination of the mapping speed range

The minimum and maximum mapping speeds are defined as follows:

Minimum mapping speed = idle speed

Maximum mapping speed = $n_{hi} \times 1.02$ or speed where full load torque drops off to zero, whichever is smaller.

7.4.3 Engine mapping curve

When the engine is stabilized according to clause 7.4.1, the engine mapping shall be performed according to the following procedure.

- (a) The engine shall be unloaded and operated at idle speed;
- (b) The engine shall be operated with maximum operator demand at minimum mapping speed;
- (c) The engine speed shall be increased at an average rate of $8 \pm 1 \text{ min}^{-1}/\text{s}$ from minimum to maximum mapping speed, or at a constant rate such that it takes 4 to 6 minutes to sweep from minimum to maximum mapping speed. Engine speed and torque points shall be recorded at a sample rate of at least one point per second.

When selecting option (b) in clause 7.4.7 for determining negative reference torque, the mapping curve may directly continue with minimum operator demand from maximum to minimum mapping speed.

7.4.4 Alternate Mapping

If a manufacturer believes that the above mapping techniques are unsafe or unrepresentative for any given engine, alternate mapping techniques may be used. These alternate techniques shall satisfy the intent of the specified mapping procedures to determine the maximum available torque at all engine speeds achieved during the test cycles. Deviations from the mapping techniques specified in this clause for reasons of safety or representativeness shall be approved by the Test Agency along with the justification for their use. In no case, however, the torque curve shall be run by descending engine speeds for governed or turbocharged engines.

7.4.5 Replicate Tests

An engine need not be mapped before each and every test cycle. An engine shall be remapped prior to a test cycle if:

- An unreasonable amount of time has transpired since the last map, as determined by engineering judgment; or
- Physical changes or recalibrations have been made to the engine which potentially affect engine performance.

7.4.6 Denormalization of Engine Speed

For generating the reference cycles, the normalized speeds of Appendix 1 (WHTC) and Table 1 (WHSC) shall be denormalized using the following equation:

$$n_{ref} = n_{norm} \times (0.45 \times n_{lo} + 0.45 \times n_{pref} + 0.1 \times n_{hi} - n_{idle}) \times 2.0327 + n_{idle} \quad (9)$$

For determination of n_{pref} , the integral of the maximum torque shall be calculated from n_{idle} to n_{95h} from the engine mapping curve, as determined in accordance with clause 7.4.3.

The engine speeds in Figures 4 and 5 of this Chapter are defined, as follows:

n_{norm}	is the normalized speed in Appendix 1 and Table 1 of this Chapter divided by 100
n_{lo}	is the lowest speed where the power is 55 per cent of maximum power
n_{pref}	is the engine speed where the integral of max. Mapped torque is 51 per cent of the whole integral between n_{idle} and n_{95h}
n_{hi}	is the highest speed where the power is 70 per cent of maximum power
n_{idle}	is the idle speed
n_{95h}	is the highest speed where the power is 95 per cent of maximum power

For engines (mainly positive ignition engines) with a steep governor droop curve, where fuel cut off does not permit to operate the engine up to n_{hi} or n_{95h} , the following provisions apply:

n_{hi} in equation 9 is replaced with $n_{P_{max}} \times 1.02$

n_{95h} is replaced with $n_{P_{max}} \times 1.02$

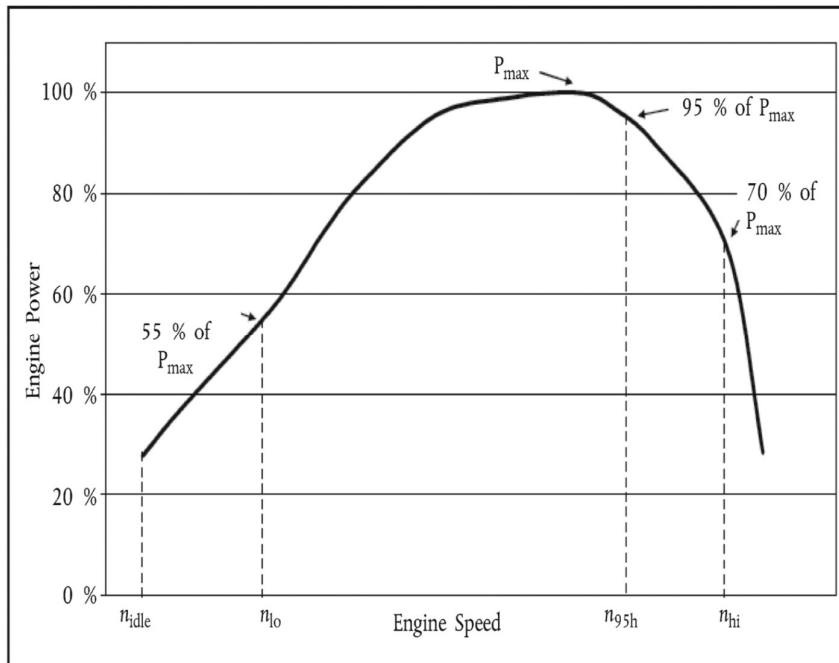


Figure 4
Definition of Test Speeds

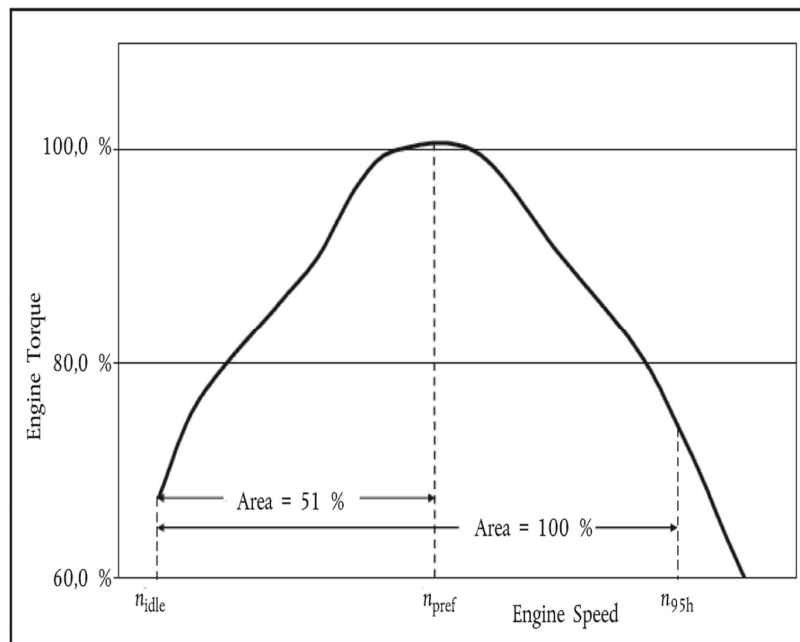


Figure 5
Definition of n_{Pref}

7.4.7

Denormalization of Engine Torque

The torque values in the engine dynamometer schedule of Appendix 1 of this Chapter (WHTC) and in Table 1 (WHSC) are normalized to the maximum torque at the respective speed. For generating the reference cycles, the torque values for each individual reference speed value as determined in clause 7.4.6 shall be denormalized, using the mapping curve determined according to clause 7.4.3, as follows:

$$M_{ref,i} = \frac{M_{norm,i}}{100} \times M_{max,i} + M_{f,i} - M_{r,i} \quad (10)$$

$M_{norm,i}$	is the normalized torque, per cent
$M_{max,i}$	is the maximum torque from the mapping curve, Nm
$M_{f,i}$	is the torque absorbed by auxiliaries/equipment to be fitted, Nm
$M_{r,i}$	is the torque absorbed by auxiliaries/equipment to be removed, Nm

If auxiliaries/equipment are fitted in accordance with clause 6.3.1 and Appendix 6 of this Chapter, M_f and M_r are zero.

The negative torque values of the motoring points (m in Appendix 1 of this Chapter) shall take on, for purposes of reference cycle generation, reference values determined in either of the following ways:

- Negative 40 per cent of the positive torque available at the associated speed point;
- Mapping of the negative torque required to motor the engine from maximum to minimum mapping speed;
- Determination of the negative torque required to motor the engine at idle and at n_{hi} and linear interpolation between these two points.

7.4.8

Calculation of Reference Cycle Work

Reference cycle work shall be determined over the test cycle by synchronously calculating instantaneous values for engine power from reference speed and reference torque, as determined in clause 7.4.6 and 7.4.7. Instantaneous engine power values shall be integrated over the test cycle to calculate the reference cycle work W_{ref} (kWh). If auxiliaries are not fitted in accordance with clause 6.3.1 of this Chapter, the instantaneous power values shall be corrected using equation 4 in clause 6.3.5 of this Chapter.

The same methodology shall be used for integrating both reference and actual engine power. If values are to be determined between adjacent reference or adjacent measured values, linear interpolation shall be used. In integrating the actual cycle work, any negative torque values shall be set equal to zero and included. If integration is performed at a frequency of less than 5 Hz, and if, during a given time

segment, the torque value changes from positive to negative or negative to positive, the negative portion shall be computed and set equal to zero. The positive portion shall be included in the integrated value.

7.5 Pre-test procedures

7.5.1 Installation of the measurement equipment

The instrumentation and sample probes shall be installed as required. The tailpipe shall be connected to the full flow dilution system, if used.

7.5.2 Preparation of measurement equipment for sampling

The following steps shall be taken before emission sampling begins:

- a) Leak checks shall be performed within 8 hours prior to emission sampling according to clause 9.3.4 of this Chapter;
- b) For batch sampling, clean storage media shall be connected, such as evacuated bags;
- c) All measurement instruments shall be started according to the instrument manufacturer's instructions and good engineering judgment;
- d) Dilution systems, sample pumps, cooling fans, and the data-collection system shall be started;
- e) The sample flow rates shall be adjusted to desired levels, using bypass flow, if desired;
- f) Heat exchangers in the sampling system shall be pre-heated or pre-cooled to within their operating temperature ranges for a test;
- g) Heated or cooled components such as sample lines, filters, coolers, and pumps shall be allowed to stabilize at their operating temperatures;
- h) Exhaust dilution system flow shall be switched on at least 10 minutes before a test sequence;
- i) Any electronic integrating devices shall be zeroed or re-zeroed, before the start of any test interval.

7.5.3 Checking the gas analyzers

Gas analyzer ranges shall be selected. Emission analyzers with automatic or manual range switching are permitted. During the test cycle, the range of the emission analyzers shall not be switched. At the same time the gains of an analyzer's analogue operational amplifier(s) may not be switched during the test cycle.

Zero and span response shall be determined for all analyzers using internationally-traceable gases that meet the specifications of clause 9.3.3 of this Chapter. FID analyzers shall be spanned on a carbon number basis of one (C1).

7.5.4 Preparation of the particulate sampling filter

At least one hour before the test, the filter shall be placed in a petri dish, which is protected against dust contamination and allows air exchange, and placed in a weighing chamber for stabilization. At the end of the stabilization period, the filter shall be weighed and the tare weight shall be recorded. The filter shall then be stored in a closed petri dish or sealed filter holder until needed for testing. The filter shall be used within eight hours of its removal from the weighing chamber.

7.5.5 Adjustment of the dilution system

The total diluted exhaust gas flow of a full flow dilution system or the diluted exhaust gas flow through a partial flow dilution system shall be set to eliminate water condensation in the system, and to obtain a filter face temperature between 315 K (42 °C) and 325 K (52 °C).

7.5.6 Starting the particulate sampling system

The particulate sampling system shall be started and operated on bypass. The particulate background level of the diluent may be determined by sampling the diluent prior to the entrance of the exhaust gas into the dilution tunnel. The measurement may be done prior to or after the test. If the measurement is done both at the beginning and at the end of the cycle, the values may be averaged. If a different sampling system is used for background measurement, the measurement shall be done in parallel to the test run

7.6 WHTC Cycle Run**7.6.1 Engine cool-down**

A natural or forced cool-down procedure may be applied. For forced cool-down, good engineering judgment shall be used to set up systems to send cooling air across the engine, to send cool oil through the engine lubrication system, to remove heat from the coolant through the engine cooling system, and to remove heat from an exhaust after-treatment system. In the case of a forced after-treatment system cool down, cooling air shall not be applied until the after-treatment system has cooled below its catalytic activation temperature. Any cooling procedure that results in unrepresentative emissions is not permitted

7.6.2 Cold Start Test

The cold-start test shall be started when the temperatures of the engine's lubricant, coolant, and after-treatment systems are all between 293 and 303 K (20 and 30 °C). The engine shall be started using one of the following methods:

- (a) The engine shall be started as recommended in the owner's manual using a production starter motor and adequately charged battery or a suitable power supply; or

- (b) The engine shall be started by using the dynamometer. The engine shall be motored within ± 25 per cent of its typical in-use cranking speed. Cranking shall be stopped within 1 second after the engine is running. If the engine does not start after 15 seconds of cranking, cranking shall be stopped and the reason for the failure to start determined, unless the owner's manual or the service-repair manual describes the longer cranking time as normal.

7.6.3 Hot Soak Period

Immediately upon completion of the cold start test, the engine shall be conditioned for the hot start test using a 10 ± 1 minute hot soak period.

7.6.4 Hot Start Test

The engine shall be started at the end of the hot soak period as defined in clause 7.6.3 using the starting methods given in clause 7.6.2 of this Chapter.

7.6.5 Test Sequence

The test sequence of both cold start and hot start test shall commence at the start of the engine. After the engine is running, cycle control shall be initiated so that engine operation matches the first set point of the cycle.

The WHTC shall be performed according to the reference cycle as set out in clause 7.4. Engine speed and torque command set points shall be issued at 5 Hz (10 Hz recommended) or greater. The set points shall be calculated by linear interpolation between the 1 Hz set points of the reference cycle. Actual engine speed and torque shall be recorded at least once every second during the test cycle (1 Hz), and the signals may be electronically filtered.

7.6.6 Collection of emission relevant data

At the start of the test sequence, the measuring equipment shall be started, simultaneously:

- (a) Start collecting or analyzing diluent, if a full flow dilution system is used;
- (b) Start collecting or analyzing raw or diluted exhaust gas, depending on the method used;
- (c) Start measuring the amount of diluted exhaust gas and the required temperatures and pressures;
- (d) Start recording the exhaust gas mass flow rate, if raw exhaust gas analysis is used
- (e) Start recording the feedback data of speed and torque of the dynamometer.

If raw exhaust measurement is used, the emission concentrations ((NM)HC, CO and NO_x) and the exhaust gas mass flow rate shall be measured continuously and stored with at least 2 Hz on a computer system. All other data may be recorded with a sample rate of at least 1 Hz. For analogue analyzers the response shall be recorded, and the calibration data may be applied online or offline during the data evaluation.

If a full flow dilution system is used, HC and NO_x shall be measured continuously in the dilution tunnel with a frequency of at least 2 Hz. The average concentrations shall be determined by integrating the analyzer signals over the test cycle. The system response time shall be no greater than 20 seconds, and shall be coordinated with CVS flow fluctuations and sampling time/test cycle offsets, if necessary. CO, CO₂, and NMHC may be determined by integration of continuous measurement signals or by analyzing the concentrations in the sample bag, collected over the cycle. The concentrations of the gaseous pollutants in the diluent shall be determined prior to the point where the exhaust enters into the dilution tunnel by integration or by collecting into the background bag. All other parameters that need to be measured shall be recorded with a minimum of one measurement per second (1 Hz).

7.6.7

Particulate Sampling

At the start of the test sequence, the particulate sampling system shall be switched from by-pass to collecting particulates.

If a partial flow dilution system is used, the sample pump(s) shall be controlled, so that the flow rate through the particulate sample probe or transfer tube is maintained proportional to the exhaust mass flow rate as determined in accordance with clause 9.4.6.1 of this Chapter.

If a full flow dilution system is used, the sample pump(s) shall be adjusted so that the flow rate through the particulate sample probe or transfer tube is maintained at a value within ± 2.5 per cent of the set flow rate. If flow compensation (i.e., proportional control of sample flow) is used, it shall be demonstrated that the ratio of main tunnel flow to particulate sample flow does not change by more than ± 2.5 per cent of its set value (except for the first 10 seconds of sampling). The average temperature and pressure at the gas meter(s) or flow instrumentation inlet shall be recorded. If the set flow rate cannot be maintained over the complete cycle within ± 2.5 per cent because of high particulate loading on the filter, the test shall be voided. The test shall be rerun using a lower sample flow rate

Engine Stalling and Equipment Malfunction

If the engine stalls anywhere during the cold start test, the test shall be voided. The engine shall be preconditioned and restarted according to the requirements of clause 7.6.2 of this Chapter, and the test repeated.

If the engine stalls anywhere during the hot start test, the hot start test shall be voided. The engine shall be soaked according to clause 7.6.3 of this Chapter, and the hot start test repeated. In this case, the cold start test need not be repeated.

If a malfunction occurs in any of the required test equipment during the test cycle, the test shall be voided and repeated in line with the above provisions

7.7 WHSC cycle run

7.7.1 Preconditioning the dilution system and the engine

The dilution system and the engine shall be started and warmed up in accordance with clause 7.4.1 of this Chapter. After warm-up, the engine and sampling system shall be preconditioned by operating the engine at mode 9 (see clause 7.2.2, Table 1 of this Chapter) for a minimum of 10 minutes while simultaneously operating the dilution system. Dummy particulate emissions samples may be collected. Those sample filters need not be stabilized or weighed, and may be discarded. Flow rates shall be set at the approximate flow rates selected for testing. The engine shall be shut off after preconditioning.

7.7.2 Engine starting

5 ± 1 minutes after completion of preconditioning at mode 9 as described in clause 7.7.1, the engine shall be started according to the manufacturer's recommended starting procedure in the owner's manual, using either a production starter motor or the dynamometer in accordance with clause 7.6.2. of this Chapter.

7.7.3 Test Sequence

The test sequence shall commence after the engine is running and within one minute after engine operation is controlled to match the first mode of the cycle (idle).

The WHSC shall be performed according to the order of test modes listed in Table 1 of clause 7.2.2 of this Chapter.

7.7.4 Collection of emission relevant data

At the start of the test sequence, the measuring equipment shall be started, simultaneously:

- (a) Start collecting or analyzing diluent, if a full flow dilution system is used;
- (b) Start collecting or analyzing raw or diluted exhaust gas, depending on the method used;
- (c) Start measuring the amount of diluted exhaust gas and the required temperatures and pressures;
- (d) Start recording the exhaust gas mass flow rate, if raw exhaust gas analysis is used;
- (e) Start recording the feedback data of speed and torque of the dynamometer.

If raw exhaust measurement is used, the emission concentrations ((NM)HC, CO and NO_x) and the exhaust gas mass flow rate shall be measured continuously and stored with at least 2 Hz on a computer system. All other data may be recorded with a sample rate of at least 1 Hz. For analogue analyzers the response shall be recorded, and the calibration data may be applied online or offline during the data evaluation.

If a full flow dilution system is used, HC and NO_x shall be measured continuously in the dilution tunnel with a frequency of at least 2 Hz. The average concentrations shall be determined by integrating the analyzer signals over the test cycle. The system response time shall be no greater than 20 seconds, and shall be coordinated with CVS flow fluctuations and sampling time/test cycle offsets, if necessary. CO, CO₂, and NMHC may be determined by integration of continuous measurement signals or by analyzing the concentrations in the sample bag, collected over the cycle. The concentrations of the gaseous pollutants in the diluent shall be determined prior to the point where the exhaust enters into the dilution tunnel by integration or by collecting into the background bag. All other parameters that need to be measured shall be recorded with a minimum of one measurement per second (1 Hz).

7.7.5

Particulate Sampling

At the start of the test sequence, the particulate sampling system shall be switched from by-pass to collecting particulates. If a partial flow dilution system is used, the sample pump(s) shall be controlled, so that the flow rate through the particulate sample probe or transfer tube is maintained proportional to the exhaust mass flow rate as determined in accordance with clause 9.4.6.1. of this Chapter.

If a full flow dilution system is used, the sample pump(s) shall be adjusted so that the flow rate through the particulate sample probe or transfer tube is maintained at a value within ± 2.5 per cent of the set flow rate. If flow compensation (i.e., proportional control of sample flow) is used, it shall be demonstrated that the ratio of main tunnel flow to particulate sample flow does not change by more than ± 2.5 per cent of its set value (except for the first 10 seconds of sampling). The average temperature and pressure at the gas meter(s) or flow instrumentation inlet shall be recorded. If the set flow rate cannot be maintained over the complete cycle within ± 2.5 per cent because of high particulate loading on the filter, the test shall be voided. The test shall be rerun using a lower sample flow rate.

7.7.6

Engine stalling and Equipment Malfunction

If the engine stalls anywhere during the cycle, the test shall be voided. The engine shall be preconditioned according to clause 7.7.1 and restarted according to clause 7.7.2, and the test repeated.

If a malfunction occurs in any of the required test equipment during the test cycle, the test shall be voided and repeated in line with the above provisions.

7.8 Post Test Procedures

7.8.1 Operations after test

At the completion of the test, the measurement of the exhaust gas mass flow rate, the diluted exhaust gas volume, the gas flow into the collecting bags and the particulate sample pump shall be stopped. For an integrating analyzer system, sampling shall continue until system response times have elapsed.

7.8.2 Verification of proportional Sampling

For any proportional batch sample, such as a bag sample or PM sample, it shall be verified that proportional sampling was maintained according to clauses 7.6.7 and 7.7.5. of this Chapter. Any sample that does not fulfil the requirements shall be voided.

7.8.3 PM Conditioning and Weighing

The particulate filter shall be placed into covered or sealed containers or the filter holders shall be closed, in order to protect the sample filters against ambient contamination. Thus protected, the filter shall be returned to the weighing chamber. The filter shall be conditioned for at least one hour, and then weighed according to clause 9.4.5. of this Chapter. The gross weight of the filter shall be recorded.

7.8.4 Drift Verification

As soon as practical but no later than 30 minutes after the test cycle is complete or during the soak period, the zero and span responses of the gaseous analyzer ranges used shall be determined. For the purpose of this clause, test cycle is defined as follows:

- (a) For the WHTC: the complete sequence cold – soak – hot;
- (b) For the WHTC hot start test (clause 6.6): the sequence soak – hot;
- (c) For the multiple regeneration WHTC hot start test (clause 6.6): the total number of hot start tests;
- (d) For the WHSC: the test cycle

The following provisions apply for analyzer drift:

- (a) The pre-test zero and span and post-test zero and span responses may be directly inserted into equation 66 of clause 8.6.1 of this Chapter without determining the drift;
- (b) If the drift between the pre-test and post-test results is less than 1 per cent of full scale, the measured concentrations may be used uncorrected or may be corrected for drift according to clause 8.6.1 of this Chapter;
- (c) If the drift difference between the pre-test and post-test results is equal to or greater than 1 per cent of full scale, the test shall be voided or the measured concentrations shall be corrected for drift according to clause 8.6.1. of this Chapter.

7.8.5 Analysis of gaseous bag sampling

As soon as practical, the following shall be performed:

Gaseous bag samples shall be analyzed no later than 30 minutes after the hot start test is complete or during the soak period for the cold start test;

Background samples shall be analyzed no later than 60 minutes after the hot start test is complete.

7.8.6 Validation of Cycle Work

Before calculating actual cycle work, any points recorded during engine starting shall be omitted. Actual cycle work shall be determined over the test cycle by synchronously using actual speed and actual torque values to calculate instantaneous values for engine power. Instantaneous engine power values shall be integrated over the test cycle to calculate the actual cycle work W_{act} (kWh). If auxiliaries/equipment are not fitted in accordance with clause 6.3.1, the instantaneous power values shall be corrected using equation 4 in clause 6.3.5. of this Chapter.

The same methodology as described in clause 7.4.8 of this Chapter shall be used for integrating actual engine power.

The actual cycle work W_{act} is used for comparison to the reference cycle work W_{ref} and for calculating the brake specific emissions (see clause 8.6.3 of this Chapter).

W_{act} shall be between 85 per cent and 105 per cent of W_{ref}

7.8.7 Validation statistics of the test cycle

Linear regressions of the actual values (n_{act} , M_{act} , P_{act}) on the reference values (n_{ref} , M_{ref} , P_{ref}) shall be performed for both the WHTC and the WHSC.

To minimize the biasing effect of the time lag between the actual and reference cycle values, the entire engine speed and torque actual signal sequence may be advanced or delayed in time with respect to the reference speed and torque sequence. If the actual signals are shifted, both speed and torque shall be shifted by the same amount in the same direction.

The method of least squares shall be used, with the best-fit equation having the form:

$$y = a_1x + a_0 \quad (11)$$

Y	y is the actual value of speed (min^{-1}), torque (Nm), or power (kW)
a_1	a_1 is the slope of the regression line
X	x is the reference value of speed (min^{-1}), torque (Nm), or power (kW)
a_0	a_0 is the y intercept of the regression line

The standard error of estimate (SEE) of y on x and the coefficient of determination (r^2) shall be calculated for each regression line.

It is recommended that this analysis be performed at 1 Hz. For a test to be considered valid, the criteria of Table 2 (WHTC) or Table 3 (WHSC) below shall be met.

Table 2 Regression Line Tolerances for the WHTC			
	Speed	Torque	Power
Standard error of estimate (SEE) of y on x	maximum 5 per cent of maximum test speed	maximum 10 per cent of maximum engine torque	maximum 10 per cent of maximum engine power
Slope of the regression line, a_1	0.95 to 1.03	0.83 - 1.03	0.89 - 1.03
Coefficient of determination, r^2	minimum 0.970	minimum 0.850	minimum 0.910
y intercept of the regression line, a_0	maximum 10 per cent of idle speed	± 20 Nm or ± 2 per cent of maximum torque whichever is greater	± 4 kW or ± 2 per cent of maximum power whichever is greater

Table 3 Regression Line Tolerances for the WHSC			
	Speed	Torque	Power
Standard error of estimate (SEE) of y on x	maximum 1 per cent of maximum test speed	maximum 2 per cent of maximum engine torque	maximum 2 per cent of maximum engine power
Slope of the regression line, a_1	0.99 to 1.01	0.98 - 1.02	0.98 - 1.02
Coefficient of determination, r^2	minimum 0.990	minimum 0.950	minimum 0.950
y intercept of the regression line, a_0	maximum 1 per cent of maximum test speed	± 20 Nm or ± 2 per cent of maximum torque whichever is greater	± 4 kW or ± 2 per cent of maximum power whichever is greater

For regression purposes only, point omissions are permitted where noted in Table 4 below before doing the regression calculation. However, those points shall not be omitted for the calculation of cycle work and emissions. Point omission may be applied to the whole or to any part of the cycle.

Table 4

Permitted Point Omissions from Regression Analysis		
Event	Conditions	Permitted point omissions
Minimum operator demand (idle point)	$n_{ref} = 0$ per cent and $M_{ref} = 0$ per cent and $M_{act} > (M_{ref} - 0.02 M_{Max \text{ mapped torque}})$ and $M_{act} < (M_{ref} + 0.02 M_{Max \text{ mapped torque}})$	speed and power
Minimum operator demand (motoring point)	$M_{ref} < 0$ per cent	power and torque
Minimum operator demand	$n_{act} \leq 1.02 n_{ref}$ and $M_{act} > M_{ref}$ or $n_{act} > n_{ref}$ and $M_{act} \leq M_{ref}$ or $n_{act} > 1.02 n_{ref}$ and $M_{ref} < M_{act} \leq (M_{ref} + 0.02 M_{Max \text{ mapped torque}})$	power and either torque or speed
Maximum operator demand	$n_{act} < n_{ref}$ and $M_{act} \geq M_{ref}$ or $n_{act} \geq 0.98 n_{ref}$ and $M_{act} < M_{ref}$ OR $n_{act} \geq 0.98 n_{ref}$ and $M_{ref} > M_{act} \geq (M_{ref} - 0.02 M_{Max \text{ mapped torque}})$	power and either torque or speed

8.0 EMISSION CALCULATION

The final test result shall be rounded in one step to the number of places to the right of the decimal point indicated by the applicable emission standard plus one additional significant figure, in accordance with ASTM E 29-06B. No rounding of intermediate values leading to the final break-specific emission result is permitted.

Calculation of hydrocarbons and/or non-methane hydrocarbons is based on the following molar carbon/hydrogen/oxygen ratios (C/H/O) of the fuel:

$\text{CH}_{1.86}\text{O}_{0.006}$	for diesel (B7),
$\text{CH}_{2.92}\text{O}_{0.46}$	for ethanol for dedicated C.I. engines(ED95),
$\text{CH}_{1.93}\text{O}_{0.032}$	for gasoline (E10),
$\text{CH}_{2.74}\text{O}_{0.385}$	for ethanol (E85),
$\text{CH}_{2.525}$	for LPG (Liquefied Petroleum Gas),
CH_4	for NG (Natural Gas) and biomethane,
$\text{C}_1\text{H}_{1.89}\text{O}_{0.016}$	for gasoline (E5)

Examples of the calculation procedures are given in Appendix 5 of this Chapter.

Emissions calculation on a molar basis, in accordance with Annex 7 of UN GTR No 11 concerning the exhaust emission test protocol for Non-Road Mobile Machinery (NRMM), is permitted with the prior agreement of the Test Agency.

8.1 Dry/Wet Correction

If the emissions are measured on a dry basis, the measured concentration shall be converted to a wet basis according to the following equation:

$$c_w = k_w \times c_d \quad (12)$$

Where

c_d is the dry concentration in ppm or per cent volume

k_w is the dry/wet correction factor ($k_{w,a}$, $k_{w,e}$, or $k_{w,d}$ depending on respective equation used)

8.1.1 Raw Exhaust Gas

$$k_{w,r} = \left(1 - \frac{1.2442 \times H_a + 111.19 \times w_{ALF} \times \frac{q_{mf,i}}{q_{mad,i}}}{773.4 + 1.2442 \times H_a + \frac{q_{mf,i}}{q_{mad,i}} \times k_{f,w} \times 1000} \right) \times 1.008 \quad (13)$$

Or

$$k_{w,r} = \left(1 - \frac{1.2442 \times H_a + 111.19 \times w_{ALF} \times \frac{q_{mf,i}}{q_{mad,i}}}{773.4 + 1.2442 \times H_a + \frac{q_{mf,i}}{q_{mad,i}} \times k_{f,w} \times 1000} \right) / (1 - p_r/p_b) \quad (14)$$

$$k_{w,r} = \left(\frac{1}{1 + a \times 0.005 \times (c_{CO_2} + c_{CO})} - k_{wl} \right) \times 1.008 \quad (15)$$

$$k_{f,w} = 0.055594 \times w_{ALF} + 0.0080021 \times w_{DEL} + 0.0070046 \times w_{EPS} \quad (16)$$

$$k_{w1} = \frac{1.608 \times H_a}{1000 + (1.608 \times H_a)} \quad (17)$$

Where

- H_a is the intake air humidity, g water per kg dry air
- w_{ALF} is the hydrogen content of the fuel, per cent mass
- $q_{mf,i}$ Is the instantaneous fuel mass flow rate, kg/s
- $q_{mad,i}$ is the instantaneous dry intake air mass flow rate, kg/s
- p_r is the water vapour pressure after cooling bath, kPa
- p_b is the total atmospheric pressure, kPa
- w_{DEL} is the nitrogen content of the fuel, per cent mass
- w_{EPS} is the oxygen content of the fuel, per cent mass
- α is the molar hydrogen ratio of the fuel
- c_{CO_2} is the dry CO₂ concentration, per cent
- c_{CO} is the dry CO concentration, per cent

Equations 13 and 14 are principally identical with the factor 1.008 in equations 13 and 15 being an approximation for the more accurate denominator in equation 14.

8.1.2

Diluted Exhaust Gas

$$K_{w,e} = \left[\left(\frac{1 - \alpha \times c_{CO_2w}}{200} \right) - K_{w2} \right] \times 1.008 \quad (18)$$

OR

$$K_{w,e} = \left[\frac{1 - K_{w2}}{1 + \left(\frac{\alpha \times c_{CO_2d}}{200} \right)} \right] \times 1.008 \quad (19)$$

$$K_{w2} = 1.608 \times \frac{\left[H_d \times \left(1 - \frac{1}{D} \right) + H_a \times \left(\frac{1}{D} \right) \right]}{1000 + \left\{ 1.608 \times \left[H_d \times \left(1 - \frac{1}{D} \right) + H_a \times \left(\frac{1}{D} \right) \right] \right\}} \quad (20)$$

- α is the molar hydrogen ratio of the fuel
- c_{CO_2w} is the wet CO₂ concentration, per cent
- c_{CO_2d} is the dry CO₂ concentration, per cent
- H_d is the diluent humidity, g water per kg dry air
- H_a is the intake air humidity, g water per kg dry air
- D is the dilution factor (see clause 8.5.2.3.2)

8.1.3 **Diluent**

$$K_{wd} = (1 - K_{w3}) \times 1.008 \quad (21)$$

$$\text{With} \quad K_{w2} = \frac{1.608 \times H_d}{1000 + (1.608 \times H_d)} \quad (22)$$

H_d is the diluent humidity, g water per kg dry air

8.2 **NO_x correction for humidity**

As the NO_x emission depends on ambient air conditions, the NO_x concentration shall be corrected for humidity with the factors given in clause 8.2.1 or 8.2.2. The intake air humidity H_a may be derived from relative humidity measurement, dew point measurement, vapour pressure measurement or dry/wet bulb measurement using generally accepted equations.

8.2.1 **Compression-ignition engines**

$$k_{h,D} = \frac{15.698 \times H_a}{1000} + 0.832 \quad (23)$$

Where:

H_a is the intake air humidity, g water per kg dry air

8.2.2 **Positive ignition engines**

$$k_{h,G} = 0.6272 + 44.030 \times 10^{-3} \times H_a - 0.862 \times 10^{-3} \times H_a^2 \quad (24)$$

Where: H_a is the intake air humidity, g water per kg dry air

8.3 **Particulate Filter Buoyancy Correction**

The sampling filter mass shall be corrected for its buoyancy in air. The buoyancy correction depends on sampling filter density, air density and the density of the balance calibration weight, and does not account for the buoyancy of the PM itself. The buoyancy correction shall be applied to both tare filter mass and gross filter mass.

If the density of the filter material is not known, the following densities shall be used:

- (a) Teflon coated glass fiber filter: 2 300 kg/m³ ;
- (b) Teflon membrane filter: 2 144 kg/m³ ;
- (c) Teflon membrane filter with polymethylpentene support ring: 920 kg/m³

For stainless steel calibration weights, a density of 8000 kg/m³ shall be used

The following equation shall be used:

$$m_f = m_{uncor} \times \left[\frac{1 - \frac{\rho_a}{\rho_w}}{1 - \frac{\rho_a}{\rho_f}} \right] \quad (25)$$

With

$$p_a = \frac{p_b \times 28.836}{8.3144 \times T_a} \quad (26)$$

m_{uncor} is the uncorrected particulate filter mass, mg

ρ_a is the density of the air, kg/m³

ρ_w is the density of balance calibration weight, kg/m³

ρ_f is the density of the particulate sampling filter, kg/m³

p_b is the total atmospheric pressure, kPa

T_a is the air temperature in the balance environment, K

28.836 is the molar mass of the air at reference humidity (282.5 K), g/mol

8.3144 is the molar gas constant

The particulate sample mass m_p used in clauses 8.4.3 and 8.5.3 shall be calculated as follows:

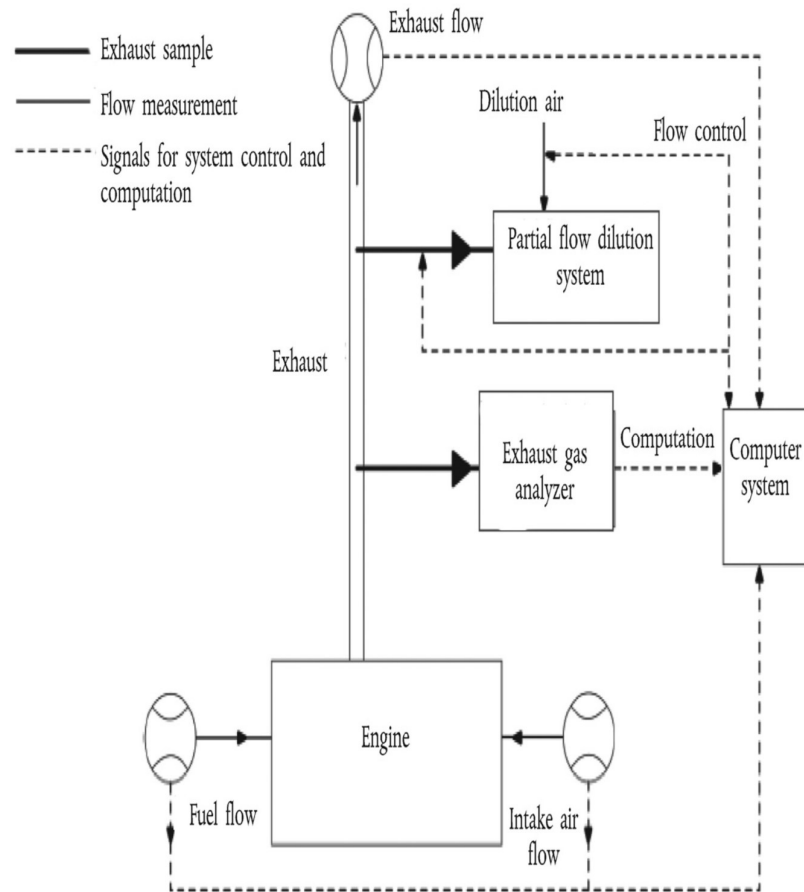
$$m_p = m_{f,G} - m_{f,T} \quad (27)$$

$m_{f,G}$ is the buoyancy corrected gross particulate filter mass, mg

$m_{f,T}$ is the buoyancy corrected tare particulate filter mass, mg

8.4 Partial flow dilution (PFS) and raw gaseous measurement

The instantaneous concentration signals of the gaseous components are used for the calculation of the mass emissions by multiplication with the instantaneous exhaust mass flow rate. The exhaust mass flow rate may be measured directly, or calculated using the methods of intake air and fuel flow measurement, tracer method or intake air and air/fuel ratio measurement. Special attention shall be paid to the response times of the different instruments. These differences shall be accounted for by time aligning the signals. For particulates, the exhaust mass flow rate signals are used for controlling the partial flow dilution system to take a sample proportional to the exhaust mass flow rate. The quality of proportionality shall be checked by applying a regression analysis between sample and exhaust flow in accordance with clause 9.4.6.1. of this Chapter. The complete test set up is schematically shown in Figure 6 below.

**Figure 6****Scheme of Raw /Partial Flow Measurement System****8.4.1 Determination of exhaust gas mass flow****8.4.1.1 Introduction**

For calculation of the emissions in the raw exhaust gas and for controlling of a partial flow dilution system, it is necessary to know the exhaust gas mass flow rate. For the determination of the exhaust mass flow rate, one of the methods described in clauses 8.4.1.3 to 8.4.1.7 may be used.

8.4.1.2 Response Time

For the purpose of emissions calculation, the response time of any of the methods described in clauses 8.4.1.3 to 8.4.1.7 shall be equal to or less than the analyzer response time of ≤ 10 seconds, as required in clause 9.3.5. of this Chapter.

For the purpose of controlling of a partial flow dilution system, a faster response is required. For partial flow dilution systems with online control, the response time shall be ≤ 0.3 second. For partial flow dilution systems with look ahead control based on a pre-recorded test run, the response time of the exhaust flow measurement

system shall be ≤ 5 seconds with a rise time of ≤ 1 second. The system response time shall be specified by the instrument manufacturer. The combined response time requirements for the exhaust gas flow and partial flow dilution system are indicated in clause 9.4.6.1. of this Chapter.

8.4.1.3 Direct Measurement Method

Direct measurement of the instantaneous exhaust flow shall be done by systems, such as:

- a) Pressure differential devices, like flow nozzle, (details see ISO 5167);
- b) Ultrasonic flowmeter;
- c) Vortex flowmeter.

Precautions shall be taken to avoid measurement errors which will impact emission value errors. Such precautions include the careful installation of the device in the engine exhaust system according to the instrument manufacturers' recommendations and to good engineering practice. Especially, engine performance and emissions shall not be affected by the installation of the device.

The flowmeters shall meet the linearity requirements of clause 9.2. of this Chapter.

8.4.1.4 Air and fuel measurement method

This involves measurement of the airflow and the fuel flow with suitable flowmeters. The calculation of the instantaneous exhaust gas flow shall be as follows:

$$q_{mew,i} = q_{maw,i} + q_{mf,i} \quad (28)$$

Where

$q_{mew,i}$ is the instantaneous exhaust mass flow rate, kg/s

$q_{maw,i}$ is the instantaneous intake air mass flow rate, kg/s

$q_{mf,i}$ is the instantaneous fuel mass flow rate, kg/s

The flowmeters shall meet the linearity requirements of clause 9.2 of this Chapter, but shall be accurate enough to also meet the linearity requirements for the exhaust gas flow.

8.4.1.5 Tracer measurement method

This involves measurement of the concentration of a tracer gas in the exhaust.

A known amount of an inert gas (e.g. pure helium) shall be injected into the exhaust gas flow as a tracer. The gas is mixed and diluted by the exhaust gas, but shall not react in the exhaust pipe. The concentration of the gas shall then be measured in the exhaust gas sample.

In order to ensure complete mixing of the tracer gas, the exhaust gas sampling probe shall be located at least 1 m or 30 times the diameter of the exhaust pipe, whichever is larger, downstream of the tracer gas

injection point. The sampling probe may be located closer to the injection point if complete mixing is verified by comparing the tracer gas concentration with the reference concentration when the tracer gas is injected upstream of the engine

The tracer gas flow rate shall be set so that the tracer gas concentration at engine idle speed after mixing becomes lower than the full scale of the trace gas analyzer.

The calculation of the exhaust gas flow shall be as follows:

$$q_{mew,i} = \frac{q_{vt} \times \rho_e}{60 \times (c_{mix,i} - c_b)} \quad (29)$$

Where,

- $q_{mew,i}$ is the instantaneous exhaust mass flow rate, kg/s
- q_{vt} is tracer gas flow rate, cm³/min
- $c_{mix,i}$ is the instantaneous concentration of the tracer gas after mixing, ppm
- ρ_e is the density of the exhaust gas, kg/m³ (see Table 5 of this Chapter)
- c_b is the background concentration of the tracer gas in the intake air, ppm

The background concentration of the tracer gas (c_b) may be determined by averaging the background concentration measured immediately before the test run and after the test run.

When the background concentration is less than 1 per cent of the concentration of the tracer gas after mixing ($c_{mix,i}$) at maximum exhaust flow, the background concentration may be neglected.

The total system shall meet the linearity requirements for the exhaust gas flow of clause 9.2. of this Chapter.

8.4.1.6 Airflow and air to fuel ratio measurement method

This involves exhaust mass calculation from the air flow and the air to fuel ratio. The calculation of the instantaneous exhaust gas mass flow is as follows.

$$q_{mew,i} = q_{maw,i} \times \left(1 + \frac{1}{A/F_{st} \times \lambda_i} \right) \quad (30)$$

$$\frac{A}{F_{st}} = \frac{138.0 \times \left(1 + \frac{\alpha}{4} - \frac{\epsilon}{2} + \gamma \right)}{12.011 \times \beta + 1.00794 \times \alpha + 15.9994 \times \epsilon + 14.0067 \times \delta + 32.065 \times \gamma} \quad (31)$$

$$\lambda_i = \frac{\left(100 - \frac{c_{COd} \times 10^{-4}}{2} - c_{HCW} \times 10^{-4} \right) + \left(\frac{\alpha}{4} \times \frac{1 - \frac{2 \times c_{COd} \times 10^{-4}}{3.5 \times c_{CO_2d}}}{1 + \frac{c_{CO} \times 10^{-4}}{3.5 \times c_{CO_2d}}} - \frac{\epsilon}{2} - \frac{\delta}{2} \right) (c_{CO_2d} + c_{COd} \times 10^{-4})}{4.764 \times \left(1 + \frac{\alpha}{4} - \frac{\epsilon}{2} + \gamma \right) \times (c_{CO_2d} + c_{COd} \times 10^{-4} + c_{CH_4} \times 10^{-4})} \quad (32)$$

Where

$q_{maw,i}$	is the instantaneous intake air mass flow rate, kg/s
A/F_{st}	is the stoichiometric air to fuel ratio, kg/kg
λ_i	is the instantaneous excess air ratio
c_{CO_2}	is the dry CO ₂ concentration, per cent
c_{CO}	is the dry CO concentration, ppm
c_{HC_w}	is the wet HC concentration, ppm

Air flow meter and analyzers shall meet the linearity requirements of clause 9.2 of this Chapter, and the total system shall meet the linearity requirements for the exhaust gas flow of clause 9.2 of this Chapter.

If an air to fuel ratio measurement equipment such as a zirconia type sensor is used for the measurement of the excess air ratio, it shall meet the specifications of clause 9.3.2.7. of this Chapter.

8.4.1.7 Carbon Balance Method

This involves exhaust mass calculation from the fuel flow and the gaseous exhaust components that include carbon. The calculation of the instantaneous exhaust gas mass flow is as follows:

$$q_{mew,i} = q_{mf,i} \times \left[\frac{w_{BET}^2 \times 1.4}{(1.0828 \times w_{BET} + k_{fd} \times k_c) \times k_c} \left(1 + \frac{H_a}{1000} \right) + 1 \right] \quad (33)$$

With

$$k_c = (c_{CO_2d} - c_{CO_2d,a}) \times 0.5441 + \frac{c_{COd}}{18.552} + \frac{c_{CH_w}}{17.355} \quad (34)$$

And

$$k_{fd} = -0.055594 \times w_{ALF} + 0.0080021 \times w_{DEL} + 0.0070046 \times w_{EPS} \quad (35)$$

$q_{mf,i}$	is the instantaneous fuel mass flow rate, kg/s
H_a	is the intake air humidity, g water per kg dry air
w_{BET}	is the carbon content of the fuel, per cent mass
w_{ALF}	is the hydrogen content of the fuel, per cent mass
w_{DEL}	is the nitrogen content of the fuel, per cent mass
w_{EPS}	is the oxygen content of the fuel, per cent mass
c_{CO_2d}	is the dry CO ₂ concentration, per cent
$c_{CO_2d,a}$	is the dry CO ₂ concentration of the intake air, per cent
c_{COd}	is the dry CO concentration, ppm
c_{CH_w}	is the wet HC concentration, ppm

8.4.2 Determination of the gaseous components

8.4.2.1 Introduction

The gaseous components in the raw exhaust gas emitted by the engine submitted for testing shall be measured with the measurement and sampling systems described in clause 9.3. and Appendix 2 of this Chapter. The data evaluation is described in clause 8.4.2.2.

Two calculation procedures are described in clause 8.4.2.3 and 8.4.2.4, which are equivalent for the reference fuel specified in Chapter 4 of this Part. The procedure in clause 8.4.2.3 is more straightforward, since it uses tabulated u values for the ratio between component and exhaust gas density. The procedure in clause 8.4.2.4 is more accurate for fuel qualities that deviate from the specifications in specified in Chapter 4 of this Part, but requires elementary analysis of the fuel composition.

8.4.2.2 Data Evaluation

The emission relevant data shall be recorded and stored in accordance with clause 7.6.6. of this Chapter.

For calculation of the mass emission of the gaseous components, the traces of the recorded concentrations and the trace of the exhaust gas mass flow rate shall be time aligned by the transformation time as defined in clause 3.1. of this Chapter. Therefore, the response time of the exhaust gas mass flow system and each gaseous emissions analyzer shall be determined according to clauses 8.4.1.2 and 9.3.5 of this Chapter respectively, and recorded.

8.4.2.3 Calculation of Mass Emission based on tabulated values

The mass of the pollutants (g/test) shall be determined by calculating the instantaneous mass emissions from the raw concentrations of the pollutants and the exhaust gas mass flow, aligned for the transformation time as determined in accordance with clause 8.4.2.2, integrating the instantaneous values over the cycle, and multiplying the integrated values with the u values from Table 5 of this Chapter. If measured on a dry basis, the dry/wet correction according to clause 8.1 of this Chapter shall be applied to the instantaneous concentration values before any further calculation is done.

For the calculation of NO_x , the mass emission shall be multiplied, where applicable, with the humidity correction factor $k_{h,D}$, or, $k_{h,G}$ as determined according to clause 8.2. of this Chapter.

The following equation shall be applied:

$$m_{gas} = u_{gas} \times \sum_{i=1}^n c_{gas,i} \times q_{mew,i} \times \frac{1}{f} \text{ (in g/test)} \quad (36)$$

Where

u_{gas} is the respective value of the exhaust component from Table 5 of this Chapter

$c_{gas,i}$ is the instantaneous concentration of the component in the exhaust gas, ppm

$q_{mew,i}$ is the instantaneous exhaust mass flow, kg/s

f is the data sampling rate, Hz

n is the number of measurements

Table 5
Raw Exhaust Gas u Values and Component Densities

Fuel	ρ_e	Gas					
		NO _x	CO	HC	CO ₂	O ₂	CH ₄
		ρ_{gas} [kg/m ³]					
		2.053	1.250	(^a)	1.9636	1.4277	0.716
		u_{gas} (^b)					
Diesel (B7)	1.2943	0.001586	0.000966	0.000482	0.001517	0.001103	0.000553
Ethanol (ED95)	1.2768	0.001609	0.00098	0.00078	0.001539	0.001119	0.000561
CNG(^c)	1.2661	0.001621	0.000987	0.000528 (^d)	0.001551	0.001128	0.000565
Propane	1.2805	0.001603	0.000976	0.000512	0.001533	0.001115	0.000559
Butane	1.2832	0.001600	0.000974	0.000505	0.001530	0.001113	0.000558
LPG (^e)	1.2811	0.001602	0.000976	0.00051	0.001533	0.001115	0.000559
Petrol (E10)	1.2931	0.001587	0.000966	0.000499	0.001518	0.001104	0.000553
Ethanol (E85)	1.2797	0.001604	0.000977	0.000730	0.001534	0.001116	0.000559
<p>(^a) depending on fuel</p> <p>(^b) at $\lambda = 2$, dry air, 273 K, 101.3 kPa</p> <p>(^c) u accurate within 0.2 % for mass composition of: C = 66 - 76 %; H = 22 - 25 %; N = 0 - 12 %</p> <p>(^d) NMHC on the basis of CH_{2.93} (for total HC the u gas coefficient of CH₄ shall be used)</p> <p>(^e) u accurate within 0.2 % for mass composition of: C3 = 70 - 90 %; C4 = 10 - 30 %</p>							

8.4.2.4 Calculation of Mass Emission Based on Exact Equations

The mass of the pollutants (g/test) shall be determined by calculating the instantaneous mass emissions from the raw concentrations of the pollutants, the u values and the exhaust gas mass flow, aligned for the transformation time as determined in accordance with clause 8.4.2.2 and integrating the instantaneous values over the cycle. If measured on a dry basis, the dry/wet correction according to clause 8.1 shall be applied to the instantaneous concentration values before any further calculation is done.

For the calculation of NO_x, the mass emission shall be multiplied with the humidity correction factor $k_{h,D}$, or, $k_{h,G}$ as determined according to clause 8.2.

The following equation shall be applied:

$$m_{gas} = \sum_{i=1}^{i=n} u_{gas,i} \times c_{gas,i} \times q_{mew,i} \times \frac{1}{f} \text{ (in g/test)} \quad (37)$$

u_{gas} is calculated from equation 38 or 39

$c_{gas,i}$ is the instantaneous concentration of the component in the exhaust gas, ppm

$q_{mew,i}$ is the instantaneous exhaust mass flow, kg/s

f is the data sampling rate, Hz

n is the number of measurement

The instantaneous u values shall be calculated as follows:

$$u_{gas,i} = M_{gas} / (M_{e,i} \times 1000) \quad (38)$$

$$u_{gas,i} = \rho_{gas} / (\rho_{e,i} \times 1000) \quad (39)$$

$$\rho_{gas} = M_{gas} / 22.414 \quad (40)$$

Where :

M_{gas} is the molar mass of the gas component, g/mol (see Appendix 5 of this Chapter)

$M_{e,i}$ is the instantaneous molar mass of the exhaust gas, g/mol

ρ_{gas} is the density of the gas component, kg/m³

$\rho_{e,i}$ is the instantaneous density of the exhaust gas, kg/m³

The molar mass of the exhaust, M_e , shall be derived for a general fuel composition $CH_\alpha O_\varepsilon N_\delta S_\gamma$ under the assumption of complete combustion, as follows

$$M_{e,i} = \frac{1 + \frac{q_{mf,i}}{q_{maw,i}}}{\frac{q_{mf,i}}{q_{maw,i}} \times \frac{\frac{\alpha}{4} + \frac{\varepsilon}{2} + \frac{\delta}{2}}{12.011 + 1.00794 \times \alpha + 15.9994 \times \varepsilon + 14.0067 \times \delta + 32.065 \times \gamma} + \frac{\frac{H_a \times 10^{-3}}{2 \times 1.00794 + 15.9994} + \frac{1}{M_a}}{1 + H_a \times 10^{-3}}} \quad \dots(41)$$

$q_{maw,i}$ is the instantaneous intake air mass flow rate on wet basis, kg/s

$q_{mf,i}$ is the instantaneous fuel mass flow rate, kg/s

H_a is the intake air humidity, g water per kg dry air

M_a is the molar mass of the dry intake air = 28.965 g/mol

The exhaust density ρ_e shall be derived, as follows:

$$\rho_{e,i} = \frac{1000 + H_a + 1000 \times (q_{mf,i}/q_{mad,i})}{773.4 + 1.2434 \times H_a + k_{fw} \times 1000 \times (q_{mf,i}/q_{mad,i})} \quad (42)$$

$q_{mad,i}$ is the instantaneous intake air mass flow rate on dry basis, kg/s

$q_{mf,i}$ is the instantaneous fuel mass flow rate, kg/s

H_a is the intake air humidity, g water per kg dry air

k_{fw} is the fuel specific factor of wet exhaust (equation 16) in clause 8.1.1

8.4.3 Particulate Determination

8.4.3.1 Data Evaluation

The particulate mass shall be calculated according to equation 27 of clause 8.3 of this Chapter. For the evaluation of the particulate concentration, the total sample mass (m_{sep}) through the filter over the test cycle shall be recorded.

With the prior approval of the Test Agency, the particulate mass may be corrected for the particulate level of the diluent, as determined in clause 7.5.6 of this Chapter, in line with good engineering practice and the specific design features of the particulate measurement system used.

8.4.3.2 Calculation of mass emission

Depending on system design, the mass of particulates (g/test) shall be calculated by either of the methods in clause 8.4.3.2.1 or 8.4.3.2.2 after buoyancy correction of the particulate sample filter according to clause 8.3 of this Chapter.

8.4.3.2.1 Calculation based on sample ratio

$$m_{PM} = m_p / r_s \times 1000 \quad (43)$$

Where:

m_p is the particulate mass sampled over the cycle, mg

r_s is the average sample ratio over the test cycle

With

$$r_s = \frac{m_{se}}{m_{ew}} \times \frac{m_{sep}}{m_{sed}} \quad (44)$$

m_{se} is the sample mass over the cycle, kg

m_{ew} is the total exhaust mass flow over the cycle, kg

m_{sep} is the mass of diluted exhaust gas passing the particulate collection filters, kg

m_{sed} is the mass of diluted exhaust gas passing the dilution tunnel, kg

In case of the total sampling type system, m_{sep} and m_{sed} are identical.

8.4.3.2.2 Calculation based on Dilution Ratio

$$m_{PM} = \frac{m_p}{m_{sep}} \times \frac{m_{edf}}{1000} \quad (45)$$

m_p is the particulate mass sampled over the cycle, mg

m_{sep} is the mass of diluted exhaust gas passing the particulate collection filters, kg

m_{edf} is the mass of equivalent diluted exhaust gas over the cycle, kg

The total mass of equivalent diluted exhaust gas mass over the cycle shall be determined as follows:

$$m_{edf} = \sum_{i=1}^n q_{medf,i} \times \frac{1}{f} \quad (46)$$

$$q_{medf,i} = q_{mew,i} \times r_{d,i} \quad (47)$$

$$r_{d,i} = \frac{q_{mdew,i}}{q_{mdew,i} - q_{mdw,i}} \quad (48)$$

$q_{medf,i}$ is the instantaneous equivalent diluted exhaust mass flow rate, kg/s

$q_{mew,i}$ is the instantaneous exhaust mass flow rate, kg/s

$r_{d,i}$ is the instantaneous dilution ratio

$q_{mdew,i}$ is the instantaneous diluted exhaust mass flow rate, kg/s

$q_{mdw,i}$ is the instantaneous diluent mass flow rate, kg/s

f is the data sampling rate, Hz

n is the number of measurements

8.5 Full flow dilution measurement (CVS)

The concentration signals, either by integration over the cycle or by bag sampling, of the gaseous components shall be used for the calculation of the mass emissions by multiplication with the diluted exhaust mass flow rate. The exhaust mass flow rate shall be measured with a constant volume sampling (CVS) system, which may use a positive displacement pump (PDP), a critical flow venturi (CFV) or a subsonic venturi (SSV) with or without flow compensation.

For bag sampling and particulate sampling, a proportional sample shall be taken from the diluted exhaust gas of the CVS system. For a system without flow compensation, the ratio of sample flow to CVS flow shall not vary by more than ± 2.5 per cent from the set point of the test. For a system with flow compensation, each individual flow rate shall be constant within ± 2.5 per cent of its respective target flow rate.

The complete test set up is schematically shown in Figure 7 below.

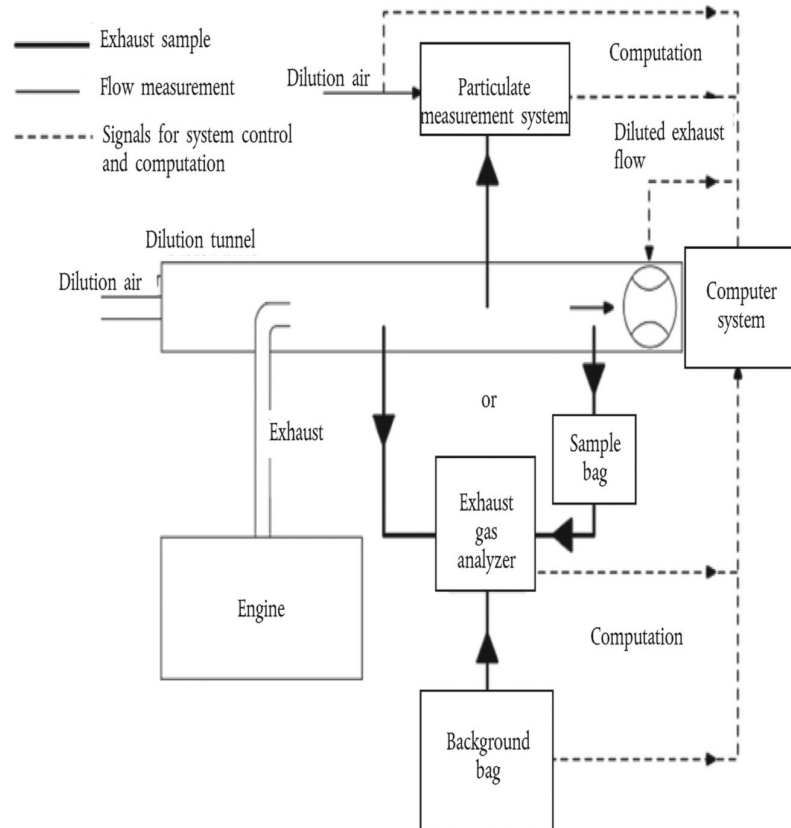


Figure 7

Scheme of Full Flow Measurement System

8.5.1 Determination of the diluted exhaust gas flow

8.5.1.1 Introduction

For calculation of the emissions in the diluted exhaust gas, it is necessary to know the diluted exhaust gas mass flow rate. The total diluted exhaust gas flow over the cycle (kg/test) shall be calculated from the measurement values over the cycle and the corresponding calibration data of the flow measurement device (V_0 for PDP, K_V for CFV, C_d for SSV) by one of the methods described in clauses 8.5.1.2 to 8.5.1.4. If the total sample flow of particulates (m_{sep}) exceeds 0.5 per cent of the total CVS flow (m_{ed}), the CVS flow shall be corrected for m_{sep} or the particulate sample flow shall be returned to the CVS prior to the flow measuring device.

8.5.1.2 PDP-CVS system

The calculation of the mass flow over the cycle is as follows, if the temperature of the diluted exhaust is kept within ± 6 K over the cycle by using a heat exchanger:

$$\begin{aligned} m_{ed} \\ = 1.293 \times V_0 \times n_p \times p_p \times 273 / (101.3 \times T) \end{aligned} \quad (49)$$

Where:

V_0 is the volume of gas pumped per revolution under test conditions, m³/rev

n_P is the total revolutions of pump per test

p_P is the absolute pressure at pump inlet, kPa

T is the average temperature of the diluted exhaust gas at pump inlet, K

If a system with flow compensation is used (i.e. without heat exchanger), the instantaneous mass emissions shall be calculated and integrated over the cycle. In this case, the instantaneous mass of the diluted exhaust gas shall be calculated as follows:

$$m_{ed} = 1.293 \times V_0 \times n_{P,i} \times p_P \times 273 / (101.3 \times T) \quad (50)$$

Where:

$n_{P,i}$ is the total revolutions of pump per time interval

8.5.1.3 CFV-CVS system

The calculation of the mass flow over the cycle is as follows, if the temperature of the diluted exhaust is kept within ± 11 K over the cycle by using a heat exchanger:

$$m_{ed} = 1.293 \times t \times K_V \times p_P / T^{0.5} \quad (51)$$

Where:

t is the cycle time, s

K_V is the calibration coefficient of the critical flow venturi for standard conditions

p_P is the absolute pressure at venturi inlet, kPa

T is the absolute temperature at venturi inlet, K

If a system with flow compensation is used (i.e. without heat exchanger), the instantaneous mass emissions shall be calculated and integrated over the cycle. In this case, the instantaneous mass of the diluted exhaust gas shall be calculated as follows:

$$m_{ed,i} = 1.293 \times \Delta t_i \times K_V \times p_P / T^{0.5} \quad (52)$$

Where:

Δt_i is the time interval

8.5.1.4 SSV-CVS system

The calculation of the mass flow over the cycle shall be as follows, if the temperature of the diluted exhaust is kept within ± 11 K over the cycle by using a heat exchanger

$$m_{ed} = 1.293 \times Q_{SSV} \quad (53)$$

With

$$Q_{SSV} = A_0 d_v^2 C_d p_P \sqrt{\left[\frac{1}{T} (r_P^{1.4286} - r_P^{1.7143}) \times \left(\frac{1}{1 - r_D^4 r_P^{1.4286}} \right) \right]} \quad (54)$$

$$A_0 = 0.006111 \text{ in SI units of } \left(\frac{m^3}{min} \right) \left(\frac{K^2}{kPa} \right) \left(\frac{1}{mm^2} \right)$$

d_v is the diameter of the SSV throat, m

C_d is the discharge coefficient of the SSV

p_P is the absolute pressure at venturi inlet, kPa

T is the temperature at the venturi inlet, K

r_P is the ratio of the SSV throat to inlet absolute, static pressure = $1 - \frac{\Delta P}{P_a}$

r_D is the ratio of the SSV throat diameter, d, to the inlet pipe diameter D

If a system with flow compensation is used (i.e. without heat exchanger), the instantaneous mass emissions shall be calculated and integrated over the cycle. In this case, the instantaneous mass of the diluted exhaust gas shall be calculated as follows

$$m_{ed} = 1.293 \times Q_{SSV} \times \Delta t_i \quad (55)$$

Where:

Δt_i is the time interval, s

The real time calculation shall be initialized with either a reasonable value for C_d , such as 0.98, or a reasonable value of Q_{SSV} . If the calculation is initialized with Q_{SSV} , the initial value of Q_{SSV} shall be used to evaluate the Reynolds number.

During all emissions tests, the Reynolds number at the SSV throat shall be in the range of Reynolds numbers used to derive the calibration curve developed in clause 9.5.4 of this Chapter.

8.5.2 Determination of the Gaseous Components

8.5.2.1 Introduction

The gaseous components in the diluted exhaust gas emitted by the engine submitted for testing shall be measured by the methods described in Appendix 2 of this Chapter. Dilution of the exhaust shall be done with filtered ambient air, synthetic air or nitrogen. The flow capacity of the full flow system shall be large enough to completely eliminate water condensation in the dilution and sampling systems. Data evaluation and calculation procedures are described in clauses 8.5.2.2 and 8.5.2.3.

8.5.2.2 Data evaluation

The emission relevant data shall be recorded and stored in accordance with clause 7.6.6. of this Chapter.

8.5.2.3 Calculation of mass emission

8.5.2.3.1 Systems with constant mass flow

For systems with heat exchanger, the mass of the pollutants shall be determined from the following equation:

$$m_{gas} = u_{gas} \times c_{gas} \times m_{ed} \text{ (in g/test)} \quad (56)$$

Where:

u_{gas} is the respective value of the exhaust component from Table 6

c_{gas} is the average background corrected concentration of the component, ppm

m_{ed} is the total diluted exhaust mass over the cycle, kg

If measured on a dry basis, the dry/wet correction according to clause 8.1. of this Chapter shall be applied.

For the calculation of NO_x, the mass emission shall be multiplied, if applicable, with the humidity correction factor $k_{h,D}$, or $k_{h,G}$, as determined according to clause 8.2. of this Chapter.

The u values are given in Table 6 below. For calculating the u_{gas} values, the density of the diluted exhaust gas has been assumed to be equal to air density. Therefore, the u_{gas} values are identical for single gas components, but different for HC

Table 6
Diluted Exhaust Gas u Values and Component Densities

Fuel	ρ_{de}	Gas					
		NO_x	CO	HC	CO ₂	O ₂	CH ₄
		$\rho_{gas} [kg/m^3]$					
		2.053	1.250	^a	1.9636	1.4277	0.716
		u_{gas}^b					
Diesel (B7)	1.293	0.001588	0.000967	0.000483	0.001519	0.001104	0.000553
Ethanol (ED95)	1.293	0.001588	0.000967	0.000770	0.001519	0.001104	0.000553
CNG ^c	1.293	0.001588	0.000967	0.000517 ^d	0.001519	0.001104	0.000553
Propane	1.293	0.001588	0.000967	0.000507	0.001519	0.001104	0.000553
Butane	1.293	0.001588	0.000967	0.000501	0.001519	0.001104	0.000553
LPG ^e	1.293	0.001588	0.000967	0.000505	0.001519	0.001104	0.000553
Petrol (E10)	1.293	0.001588	0.000967	0.000499	0.001519	0.001104	0.000554
Ethanol (E85)	1.293	0.001588	0.000967	0.000722	0.001519	0.001104	0.000554

^a depending on fuel

^b at $\lambda = 2$, dry air, 273 K, 101.3 kPa

^c u accurate within 0.2 % for mass composition of: C = 66 - 76 %; H = 22 - 25 %; N = 0 - 12 %

^d NMHC on the basis of CH_{2.93} (for total HC the u_{gas} coefficient of CH₄ shall be used)

^e u accurate within 0.2 % for mass composition of: C3 = 70 - 90 %; C4 = 10 - 30 %

Alternatively, the u values may be calculated using the exact calculation method generally described in clause 8.4.2.4 of this Chapter as follows:

$$u_{gas} = \frac{M_{gas}}{M_d \times \left(1 - \frac{1}{D}\right) + M_e \times \left(\frac{1}{D}\right)} \quad (57)$$

Where:

M_{gas} is the molar mass of the gas component, g/mol
(see Appendix 5 of this Chapter)

M_e is the molar mass of the exhaust gas, g/mol

M_d is the molar mass of the diluent = 28.965 g/mol

D is the dilution factor (see clause 8.5.2.3.2)

8.5.2.3.2 Determination of the Background Corrected Concentrations

The average background concentration of the gaseous pollutants in the diluent shall be subtracted from the measured concentrations to get the net concentrations of the pollutants. The average values of the background concentrations can be determined by the sample bag method or by continuous measurement with integration. The following equation shall be used:

$$c_{gas} = c_{gas,e} - c_d \times (1 - (1/D)) \quad (58)$$

Where:

$c_{gas,e}$ is the concentration of the component measured in the diluted exhaust gas, ppm

c_d is the concentration of the component measured in the diluent,
ppm

D is the dilution factor

The dilution factor shall be calculated as follows:

a) For diesel fuelled engines and LPG fuelled gas engines

$$D = \frac{F_S}{c_{CO_2,e} + (c_{HC,e} + c_{CO,e}) \times 10^{-4}} \quad (59)$$

b) For natural gas fuelled gas engines

$$D = \frac{F_S}{c_{CO_2,e} + (c_{NMHC,e} + c_{CO,e}) \times 10^{-4}} \quad (60)$$

$c_{CO_2,e}$ is the wet concentration of CO₂ in the diluted exhaust gas,
per cent vol

$c_{HC,e}$ is the wet concentration of HC in the diluted exhaust gas,
ppm C1

$c_{NMHC,e}$ is the wet concentration of NMHC in the diluted exhaust
gas, ppm C1

$c_{CO,e}$ is the wet concentration of CO in the diluted exhaust gas,
ppm

F_S is the stoichiometric factor

The stoichiometric factor shall be calculated as follows:

$$F_S = 100 \times \frac{1}{1 + \frac{\alpha}{2} + 3.76 \times \left(1 + \frac{\alpha}{4}\right)} \quad (61)$$

Where:

α is the molar hydrogen ratio of the fuel (H/C)

Alternatively, if the fuel composition is not known, the following
stoichiometric factors may be used:

F_S (diesel) = 13.4

F_S (LPG) = 11.6

F_S (NG) = 9.5

F_S (E10) = 13.3

F_S (E85) = 11.5

8.5.2.3.3 System with Flow Compensation

For systems without heat exchanger, the mass of the pollutants
(g/test) shall be determined by calculating the instantaneous mass
emissions and integrating the instantaneous values over the cycle.
Also, the background correction shall be applied directly to the
instantaneous concentration value. The following equation shall be
applied:

$$m_{gas} = \sum_{i=1}^n [(m_{ed,i} \times c_{gas,e} \times u_{gas,e})] - [m_{ed} \times c_d \times (1 - 1/D) \times u_{gas}] \quad (62)$$

Where:

$c_{gas,e}$ is the concentration of the component measured in the diluted exhaust gas, ppm

c_d is the concentration of the component measured in the diluent, ppm

$m_{ed,i}$ is the instantaneous mass of the diluted exhaust gas, kg

m_{ed} is the total mass of diluted exhaust gas over the cycle, kg

u_{gas} is the tabulated value from Table 6 of this Chapter.

D is the dilution factor

8.5.3 Particulate Determination

8.5.3.1 Calculation of mass emission

The particulate mass (g/test) shall be calculated after buoyancy correction of the particulate sample filter according to clause 8.3, as follows:

$$m_{PM} = \frac{m_p}{m_{sep}} \times \frac{m_{ed}}{1000} \quad (63)$$

Where:

m_p is the particulate mass sampled over the cycle, mg

m_{sep} is the mass of diluted exhaust gas passing the particulate collection filters, kg

m_{ed} is the mass of diluted exhaust gas over the cycle, kg

$$m_{sep} = m_{set} - m_{ssd} \quad (64)$$

Where:

m_{set} is the mass of double diluted exhaust gas through particulate filter, kg

m_{ssd} is the mass of secondary diluent, kg

If the particulate background level of the diluent is determined in accordance with clause 7.5.6 of this Chapter, the particulate mass may be background corrected. In this case, the particulate mass (g/test) shall be calculated as follows:

$$m_{PM} = \left[\frac{m_p}{m_{sep}} - \left(\frac{m_b}{m_{sd}} \times \left(1 - \frac{1}{D} \right) \right) \right] \times \frac{m_{ed}}{1000} \quad (65)$$

Where:

- m_{sep} is the mass of diluted exhaust gas passing the particulate collection filters, kg
- m_{ed} is the mass of diluted exhaust gas over the cycle, kg
- m_{sd} is the mass of diluent sampled by background particulate sampler, kg
- m_b is the mass of the collected background particulates of the diluent, mg
- D is the dilution factor as determined in clause 8.5.2.3.2.

8.6 General Calculation

8.6.1 Drift Correction

With respect to drift verification in clause 7.8.4 of this Chapter, the corrected concentration value shall be calculated as follows

$$c_{corr} = c_{ref,z} + (c_{ref,s} - c_{ref,z}) \left[\frac{2 \times c_{gas} - (c_{pre,z} + c_{post,z})}{(c_{pre,s} + c_{post,s}) - (c_{pre,z} + c_{post,z})} \right] \quad (66)$$

- $c_{ref,z}$ is the reference concentration of the zero gas (usually zero), ppm
- $c_{ref,s}$ is the reference concentration of the span gas, ppm
- $c_{pre,z}$ is the pre-test analyzer concentration of the zero gas, ppm
- $c_{pre,s}$ is the pre-test analyzer concentration of the span gas, ppm
- $c_{post,z}$ is the post-test analyzer concentration of the zero gas, ppm
- $c_{post,s}$ is the post-test analyzer concentration of the span gas, ppm
- c_{gas} is the sample gas concentration, ppm

Two sets of specific emission results shall be calculated for each component in accordance with clause 8.6.3, after any other corrections have been applied. One set shall be calculated using uncorrected concentrations and another set shall be calculated using the concentrations corrected for drift according to equation 66.

Depending on the measurement system and calculation method used, the uncorrected emissions results shall be calculated with equations 36, 37, 56, 57 or 62, respectively. For calculation of the corrected emissions, c_{gas} in equations 36, 37, 56, 57 or 62, respectively, shall be replaced with c_{cor} of equation 66. If instantaneous concentration values $c_{gas,i}$ are used in the respective equation, the corrected value shall also be applied as instantaneous value $c_{cor,i}$. In equation 57, the correction shall be applied to both the measured and the background concentration.

The comparison shall be made as a percentage of the uncorrected results. The difference between the uncorrected and the corrected brake-specific emission values shall be within ± 4 per cent of the uncorrected brake-specific emission values or within ± 4 per cent of the respective limit value, whichever is greater. If the drift is greater than 4 per cent, the test shall be voided.

If drift correction is applied, only the drift-corrected emission results shall be used when reporting emissions.

8.6.2

Calculation of NMHC and CH₄

The calculation of NMHC and CH₄ depends on the calibration method used. The FID for the measurement without NMC (lower path of Appendix 2 of this Chapter, Figure 3), shall be calibrated with propane. For the calibration of the FID in series with NMC (upper path of Appendix 2 of this Chapter, Figure 3), the following methods are permitted.

- (a) Calibration gas – propane; propane bypasses NMC;
- (b) Calibration gas – methane; methane passes through NMC.

The concentration of NMHC and CH₄ shall be calculated as follows for (a):

$$c_{NMHC} = \frac{c_{HC(w/NMC)} - c_{HC(w/o NMC)} \times (1 - E_E)}{r_h \times (E_E - E_M)} \quad (67)$$

$$c_{CH_4} = \frac{c_{HC(w/o NMC)} \times (1 - E_M) - c_{HC(w/NMC)}}{(E_E - E_M)} \quad (68)$$

The concentration of NMHC and CH₄ shall be calculated as follows for (b):

$$c_{NMHC} = \frac{c_{HC(w/o NMC)} \times (1 - E_M) - c_{HC(w/NMC)} \times r_h \times (1 - E_M)}{(E_E - E_M)} \quad (67a)$$

$$c_{CH_4} = \frac{c_{HC(w/NMC)} \times r_h \times (1 - E_M) - c_{HC(w/o NMC)} \times (1 - E_E)}{r_h \times (E_E - E_M)} \quad (68a)$$

Where:

$c_{HC(w/NMC)}$ is the HC concentration with sample gas flowing through the NMC, ppm

$c_{HC(w/o NMC)}$ is the HC concentration with sample gas bypassing the NMC, ppm

r_h is the methane response factor as determined per clause 9.3.7.2

E_M is the methane efficiency as determined per clause 9.3.8.1

E_E is the ethane efficiency as determined per clause 9.3.8.2.

If $r_h < 1.05$, it may be omitted in equations 67, 67a and 68a.

8.6.3 Calculation of the specific emissions

The specific emissions e_{gas} or e_{PM} (g/kWh) shall be calculated for each individual component in the following ways depending on the type of test cycle.

For the WHSC, hot WHTC, or cold WHTC, the following equation shall be applied:

$$e = \frac{m}{W_{act}} \quad (69)$$

Where:

m is the mass emission of the component, g/test

W_{act} is the actual cycle work as determined according to clause 7.8.6, kWh

For the WHTC, the final test result shall be a weighted average from cold start test and hot start test according to the following equation:

$$e = \frac{(0.14 \times m_{cold}) + (0.86 \times m_{hot})}{(0.14 \times W_{act,cold}) + (0.86 \times W_{act,hot})} \quad (70)$$

Where:

m_{cold} is the mass emission of the component on the cold start test, g/test

m_{hot} is the mass emission of the component on the hot start test, g/test

$W_{act,cold}$ is the actual cycle work on the cold start test, kWh

$W_{act,hot}$ is the actual cycle work on the hot start test, kWh

If periodic regeneration in accordance with clause 6.6.2 of this Chapter applies, the regeneration adjustment factors $k_{r,u}$ or $k_{r,d}$ shall be multiplied with or be added to, respectively, the specific emissions result e as determined in equations 69 and 70.

9.0 EQUIPMENT SPECIFICATION AND VERIFICATION

This Chapter does not contain details of flow, pressure, and temperature measuring equipment or systems. Instead, only the linearity requirements of such equipment or systems necessary for conducting an emissions test are given in clause 9.2.

9.1 Dynamometer Specification

An engine dynamometer with adequate characteristics to perform the appropriate test cycle described in clause 7.2.1 and 7.2.2 of this Chapter shall be used.

The instrumentation for torque and speed measurement shall allow the measurement accuracy of the shaft power as needed to comply with the cycle validation criteria. Additional calculations may be necessary. The accuracy of the measuring equipment shall be such that the linearity requirements given in clause 9.2, Table 7 below are not exceeded.

9.2 Linearity requirements

The calibration of all measuring instruments and systems shall be traceable to national (international) standards. The measuring instruments and systems shall comply with the linearity requirements given in Table 7 below. The linearity verification according to clause 9.2.1 shall be performed for the gas analyzers at least every three months or whenever a system repair or change is made that could influence calibration. For the other instruments and systems, the linearity verification shall be done as required by internal audit procedures, by the instrument manufacturer or in accordance with ISO 9000 requirements.

Table 7
Linearity Requirements of Instruments and Measurement Systems

Measurement system	$ x_{min} \times (a_1 - 1) + a_0 $	Slope a_1	Standard error SEE	Coefficient of determination r^2
Engine speed	$\leq 0.05 \% \text{ max}$	0.98 – 1.02	$\leq 2 \% \text{ max}$	≥ 0.990
Engine torque	$\leq 1 \% \text{ max}$	0.98 – 1.02	$\leq 2 \% \text{ max}$	≥ 0.990
Fuel flow	$\leq 1 \% \text{ max}$	0.98 – 1.02	$\leq 2 \% \text{ max}$	≥ 0.990
Airflow	$\leq 1 \% \text{ max}$	0.98 – 1.02	$\leq 2 \% \text{ max}$	≥ 0.990
Exhaust gas flow	$\leq 1 \% \text{ max}$	0.98 – 1.02	$\leq 2 \% \text{ max}$	≥ 0.990
Diluent flow	$\leq 1 \% \text{ max}$	0.98 – 1.02	$\leq 2 \% \text{ max}$	≥ 0.990
Diluted exhaust gas flow	$\leq 1 \% \text{ max}$	0.98 – 1.02	$\leq 2 \% \text{ max}$	≥ 0.990
Sample flow	$\leq 1 \% \text{ max}$	0.98 – 1.02	$\leq 2 \% \text{ max}$	≥ 0.990
Gas analyzers	$\leq 0.5 \% \text{ max}$	0.99 – 1.01	$\leq 1 \% \text{ max}$	≥ 0.998
Gas dividers	$\leq .5 \% \text{ max}$	0.98 – 1.02	$\leq 2 \% \text{ max}$	≥ 0.990
Temperatures	$\leq 1 \% \text{ max}$	0.99 – 1.01	$\leq 1 \% \text{ max}$	≥ 0.998
Pressures	$\leq 1 \% \text{ max}$	0.99 – 1.01	$\leq 1 \% \text{ max}$	≥ 0.998
PM balance	$\leq 1 \% \text{ max}$	0.99 – 1.01	$\leq 1 \% \text{ max}$	≥ 0.998

9.2.1 Linearity verification**9.2.1.1 Introduction**

A linearity verification shall be performed for each measurement system listed in Table 7 above. At least 10 reference values, or as specified otherwise, shall be introduced to the measurement system, and the measured values shall be compared to the reference values by using a least squares linear regression in accordance with equation 11 in clause 7.8.7. The maximum limits in Table 7 above refer to the maximum values expected during testing.

9.2.1.2 General Requirements

The measurement systems shall be warmed up according to the recommendations of the instrument manufacturer. The measurement systems shall be operated at their specified temperatures, pressures and flows.

9.2.1.3 Procedure

The linearity verification shall be run for each normally used operating range with the following steps:

- (a) The instrument shall be set at zero by introducing a zero signal. For gas analyzers, purified synthetic air (or nitrogen) shall be introduced directly to the analyzer port;
- (b) The instrument shall be spanned by introducing a span signal. For gas analyzers, an appropriate span gas shall be introduced directly to the analyzer port;
- (c) The zero procedure of (a) shall be repeated;
- (d) The verification shall be established by introducing at least 10 reference values (including zero) that are within the range from zero to the highest values expected during emission testing. For gas analyzers, known gas concentrations in accordance with clause 9.3.3.2 of this Chapter shall be introduced directly to the analyzer port;
- (e) At a recording frequency of at least 1 Hz, the reference values shall be measured and the measured values recorded for 30 seconds;
- (f) The arithmetic mean values over the 30 seconds period shall be used to calculate the least squares linear regression parameters according to equation 11 in clause 7.8.7 of this Chapter;
- (g) The linear regression parameters shall meet the requirements of clause 9.2, Table 7;
- (h) The zero setting shall be rechecked and the verification procedure repeated, if necessary.

9.3 Gaseous Emissions Measurement and Sampling System

9.3.1 Analyzer specifications

9.3.1.1 General

The analyzers shall have a measuring range and response time appropriate for the accuracy required to measure the concentrations of the exhaust gas components under transient and steady state conditions.

The electromagnetic compatibility (EMC) of the equipment shall be on a level is to minimize additional errors.

9.3.1.2 Accuracy

The accuracy, defined as the deviation of the analyzer reading from the reference value, shall not exceed ± 2 per cent of the reading or ± 0.3 per cent of full scale whichever is larger.

9.3.1.3 Precision

The precision, defined as 2,5 times the standard deviation of 10 repetitive responses to a given calibration or span gas, shall be no greater than 1 per cent of full scale concentration for each range used above 155 ppm (or ppm C) or 2 per cent of each range used below 155 ppm (or ppm C).

9.3.1.4 Noise

The analyzer peak-to-peak response to zero and calibration or span gases over any 10 seconds period shall not exceed 2 per cent of full scale on all ranges used.

9.3.1.5 Zero Drift

The drift of the zero response shall be specified by the instrument manufacturer.

9.3.1.6 Span Drift

The drift of the span response shall be specified by the instrument manufacturer.

9.3.1.7 Rise Time

The rise time of the analyzer installed in the measurement system shall not exceed 2,5 seconds.

9.3.1.8 Gas Drying

Exhaust gases may be measured wet or dry. A gas-drying device, if used, shall have a minimal effect on the composition of the measured gases. Chemical dryers are not an acceptable method of removing water from the sample

9.3.2 **Gas Analyzers**

9.3.2.1 **Introduction**

Clauses 9.3.2.2 to 9.3.2.7 describe the measurement principles to be used. A detailed description of the measurement systems is given in Appendix 2 of this Chapter. The gases to be measured shall be analyzed with the following instruments. For non-linear analyzers, the use of linearizing circuits is permitted.

9.3.2.2 **Carbon monoxide (CO) analysis**

The carbon monoxide analyzer shall be of the non-dispersive infrared (NDIR) absorption type.

9.3.2.3 **Carbon dioxide (CO₂) analysis**

The carbon dioxide analyzer shall be of the non-dispersive infrared (NDIR) absorption type.

9.3.2.4 **Hydrocarbon (HC) analysis**

The hydrocarbon analyzer shall be of the heated flame ionization detector (HFID) type with detector, valves, pipework, etc. heated so as to maintain a gas temperature of $463\text{ K} \pm 10\text{ K}$ ($190 \pm 10\text{ }^{\circ}\text{C}$). Optionally, for natural gas fuelled and PI engines, the hydrocarbon analyzer may be of the non-heated flame ionization detector (FID) type depending upon the method used (see Appendix 2 of this Chapter, clause A.2.1.3).

9.3.2.5 **Methane (CH₄) and non-methane hydrocarbon (NMHC) analysis**

The determination of the methane and non-methane hydrocarbon fraction shall be performed with a heated non-methane cutter (NMC) and two FIDs as per Appendix 2 of this Chapter, clause A.2.1.4 and clause A.2.1.5. The concentration of the components shall be determined as per clause 8.6.2 of this Chapter.

9.3.2.6 **Oxides of nitrogen (NO_x) analysis**

Two measurement instruments are specified for NO_x measurement and either instrument may be used provided it meets the criteria specified in clauses 9.3.2.6.1 or 9.3.2.6.2, respectively. For the determination of system equivalency of an alternate measurement procedure in accordance with clause 5.1.1 of this Chapter, only the CLD is permitted.

9.3.2.6.1 **Chemiluminescent detector (CLD)**

If measured on a dry basis, the oxides of nitrogen analyzer shall be of the chemiluminescent detector (CLD) or heated chemiluminescent detector (HCLD) type with a NO₂/NO converter. If measured on a wet basis, a HCLD with converter maintained above 328 K ($55\text{ }^{\circ}\text{C}$) shall be used, provided the water quench check (see clause 9.3.9.2.2)

is satisfied. For both CLD and HCLD, the sampling path shall be maintained at a wall temperature of 328 K to 473 K (55 °C to 200 °C) up to the converter for dry measurement and up to the analyzer for wet measurement.

9.3.2.6.2 **Non-dispersive ultraviolet detector (NDUV)**

A non-dispersive ultraviolet (NDUV) analyzer shall be used to measure NO_x concentration. If the NDUV analyzer measures only NO, a NO₂ /NO converter shall be placed upstream of the NDUV analyzer. The NDUV temperature shall be maintained to prevent aqueous condensation, unless a sample dryer is installed upstream of the NO₂ /NO converter, if used, or upstream of the analyzer.

9.3.2.7 **Air to fuel measurement**

The air to fuel measurement equipment used to determine the exhaust gas flow as specified in clause 8.4.1.6 of this Chapter shall be a wide range air to fuel ratio sensor or lambda sensor of Zirconia type. The sensor shall be mounted directly on the exhaust pipe where the exhaust gas temperature is high enough to eliminate water condensation.

The accuracy of the sensor with incorporated electronics shall be within:

± 3 per cent of reading for $\lambda < 2$

± 5 per cent of reading for $2 \leq \lambda < 5$

± 10 per cent of reading for $5 \leq \lambda$

To fulfil the accuracy specified above, the sensor shall be calibrated as specified by the instrument manufacturer.

9.3.3 **Gases**

The shelf life of all gases shall be respected

9.3.3.1 **Pure Gases**

The required purity of the gases is defined by the contamination limits given below. The following gases shall be available for operation:

a) For raw exhaust gas

Purified nitrogen

(Contamination ≤ 1 ppm C1, ≤ 1 ppm CO, ≤ 400 ppm CO₂, ≤ 0.1 ppm NO)

Purified oxygen

(Purity > 99.5 per cent vol O₂)

Hydrogen-helium mixture (FID burner fuel)

(40 ± 1 per cent hydrogen, balance helium)

(Contamination ≤ 1 ppm C1, ≤ 400 ppm CO₂)

Purified synthetic air
(Contamination ≤ 1 ppm C1, ≤ 1 ppm CO, ≤ 400 ppm CO₂, ≤ 0.1 ppm NO)

(Oxygen content between 18-21 per cent vol.)

b) For dilute exhaust gas (optionally for raw exhaust gas)

Purified nitrogen
(Contamination ≤ 0.05 ppm C1, ≤ 1 ppm CO, ≤ 10 ppm CO₂, ≤ 0.02 ppm NO)

Purified oxygen
(Purity > 99.5 per cent volO₂)

Hydrogen-helium mixture (FID burner fuel)
(40 ± 1 per cent hydrogen, balance helium)
(Contamination ≤ 0.05 ppm C1, ≤ 10 ppm CO₂)

Purified synthetic air
(Contamination ≤ 0.05 ppm C1, ≤ 1 ppm CO, ≤ 10 ppm CO₂, ≤ 0.02 ppm NO)
(Oxygen content between 20.5 – 21.5 per cent vol.)

If gas bottles are not available, a gas purifier may be used, if contamination levels can be demonstrated.

9.3.3.2 Calibration and Span Gases

Mixtures of gases having the following chemical compositions shall be available, if applicable. Other gas combinations are allowed provided the gases do not react with one another. The expiration date of the calibration gases stated by the manufacturer shall be recorded.

C₃H₈ and purified synthetic air (see clause 9.3.3.1);

CO and purified nitrogen;

NO and purified nitrogen;

NO₂ and purified synthetic air;

CO₂ and purified nitrogen;

CH₄ and purified synthetic air;

C₂H₆ and purified synthetic air.

The true concentration of a calibration and span gas shall be within ± 1 per cent of the nominal value, and shall be traceable to national or international standards. All concentrations of calibration gas shall be given on a volume basis (volume per cent or volume ppm).

9.3.3.3 Gas Dividers

The gases used for calibration and span may also be obtained by means of gas dividers (precision blending devices), diluting with purified N₂ or with purified synthetic air. The accuracy of the gas divider shall be such that the concentration of the blended calibration gases is accurate to within ± 2 per cent. This accuracy implies that

primary gases used for blending shall be known to an accuracy of at least ± 1 per cent, traceable to national or international gas standards. The verification shall be performed at between 15 and 50 per cent of full scale for each calibration incorporating a gas divider. An additional verification may be performed using another calibration gas, if the first verification has failed.

Optionally, the blending device may be checked with an instrument which by nature is linear, e.g. using NO gas with a CLD. The span value of the instrument shall be adjusted with the span gas directly connected to the instrument. The gas divider shall be checked at the settings used and the nominal value shall be compared to the measured concentration of the instrument. This difference shall in each point be within ± 1 per cent of the nominal value.

For conducting the linearity verification according to clause 9.2.1 of this Chapter, the gas divider shall be accurate to within ± 1 per cent

9.3.3.4 **Oxygen interference check gases**

Oxygen interference check gases are a blend of propane, oxygen and nitrogen. They shall contain propane with $350 \text{ ppm C} \pm 75 \text{ ppm C}$ hydrocarbon. The concentration value shall be determined to calibration gas tolerances by chromatographic analysis of total hydrocarbons plus impurities or by dynamic blending. The oxygen concentrations required for positive ignition and compression ignition engine testing are listed in Table 8 below with the remainder being purified nitrogen.

Table 8

Oxygen Interference Check Gases

Type of Engine	O ₂ concentration (per cent)
Compression ignition	21 (20 to 22)
Compression and positive ignition	10 (9 to 11)
Compression and positive ignition	5 (4 to 6)
Positive ignition	0 (0 to 1)

9.3.4 **Leak check**

A system leak check shall be performed. The probe shall be disconnected from the exhaust system and the end plugged. The analyzer pump shall be switched on. After an initial stabilization period all flowmeters will read approximately zero in the absence of a leak. If not, the sampling lines shall be checked and the fault corrected

The maximum allowable leakage rate on the vacuum side shall be 0.5 per cent of the in-use flow rate for the portion of the system being checked. The analyzer flows and bypass flows may be used to estimate the in-use flow rates.

Alternatively, the system may be evacuated to a pressure of at least 20 kPa vacuum (80 kPa absolute). After an initial stabilization period the pressure increase Δp (kPa/min) in the system shall not exceed:

$$\Delta p = p/V_s \times 0.005 \times q_{vs} \quad (71)$$

Where:

V is the system volume, l

q_{vs} is the system flow rate, l/min

Another method is the introduction of a concentration step change at the beginning of the sampling line by switching from zero to span gas. If for a correctly calibrated analyzer after an adequate period of time the reading is ≤ 99 per cent compared to the introduced concentration, this points to a leakage problem that shall be corrected.

9.3.5 Response Time Check of the Analytical System

The system settings for the response time evaluation shall be exactly the same as during measurement of the test run (i.e. pressure, flow rates, filter settings on the analyzers and all other response time influences). The response time determination shall be done with gas switching directly at the inlet of the sample probe. The gas switching shall be done in less than 0.1 second. The gases used for the test shall cause a concentration change of at least 60 per cent full scale (FS).

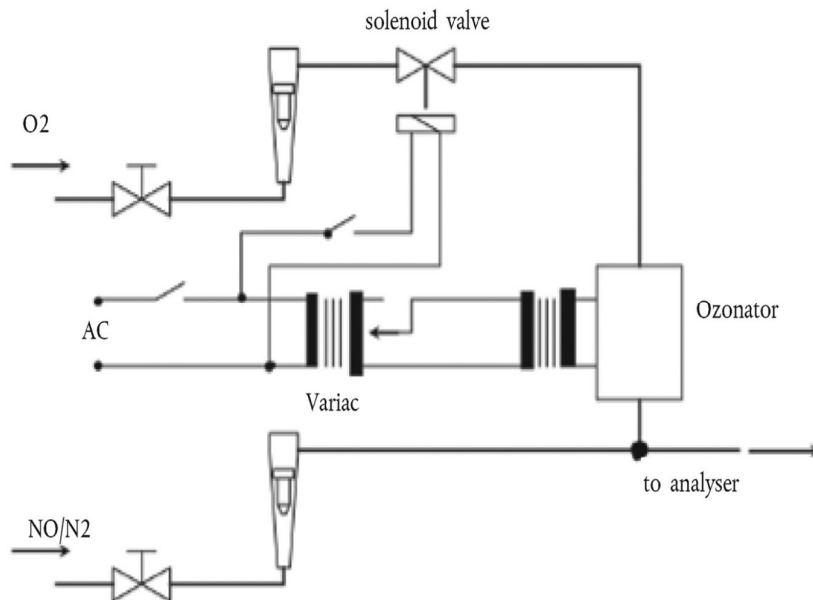
The concentration trace of each single gas component shall be recorded. The response time is defined to be the difference in time between the gas switching and the appropriate change of the recorded concentration. The system response time (t_{90}) consists of the delay time to the measuring detector and the rise time of the detector. The delay time is defined as the time from the change (t_0) until the response is 10 per cent of the final reading (t_{10}). The rise time is defined as the time between 10 per cent and 90 per cent response of the final reading ($t_{90} - t_{10}$).

For time alignment of the analyzer and exhaust flow signals, the transformation time is defined as the time from the change (t_0) until the response is 50 per cent of the final reading (t_{50}).

The system response time shall be ≤ 10 s with a rise time of ≤ 2.5 seconds in accordance with clause 9.3.1.7 for all limited components (CO, NO_x HC or NMHC) and all ranges used. When using a NMC for the measurement of NMHC, the system response time may exceed 10 seconds

9.3.6 Efficiency Test of NO_x converter

The efficiency of the converter used for the conversion of NO₂ into NO is tested as given in clauses 9.3.6.1 to 9.3.6.8 (see Figure 8 below).

**Figure 8****Scheme of NO₂ Converter Efficiency Device****9.3.6.1 Test Setup**

Using the test setup as schematically shown in Figure 8 and the procedure below, the efficiency of the converter shall be tested by means of an ozonator.

9.3.6.2 Calibration

The CLD and the HCLD shall be calibrated in the most common operating range following the manufacturer's specifications using zero and span gas (the NO content of which shall amount to about 80 per cent of the operating range and the NO₂ concentration of the gas mixture to less than 5 per cent of the NO concentration). The NO_x analyzer shall be in the NO mode so that the span gas does not pass through the converter. The indicated concentration has to be recorded.

9.3.6.3 Calculation

The per cent efficiency of the converter shall be calculated as follows:
Where:

$$E_{NO_x} = \left(1 + \frac{a - b}{c - d}\right) \times 100 \quad (72)$$

- a is the NO_x concentration according to clause 9.3.6.6.
- b is the NO_x concentration according to clause 9.3.6.7.
- c is the NO concentration according to clause 9.3.6.4.
- d is the NO concentration according to clause 9.3.6.5.

9.3.6.4 **Adding of oxygen**

Via a T-fitting, oxygen or zero air shall be added continuously to the gas flow until the concentration indicated is about 20 per cent less than the indicated calibration concentration given in clause 9.3.6.2 (the analyzer is in the NO mode).

The indicated concentration (c) shall be recorded. The ozonator is kept deactivated throughout the process.

9.3.6.5 **Activation of the ozonator**

The ozonator shall be activated to generate enough ozone to bring the NO concentration down to about 20 per cent (minimum 10 per cent) of the calibration concentration given in clause 9.3.6.2. The indicated concentration (d) shall be recorded (the analyzer is in the NO mode).

9.3.6.6 **NO_x mode**

The NO analyzer shall be switched to the NO_x mode so that the gas mixture (consisting of NO, NO₂, O₂ and N₂) now passes through the converter. The indicated concentration (a) shall be recorded (the analyzer is in the NO_x mode).

9.3.6.7 **Deactivation of the ozonator**

The ozonator is now deactivated. The mixture of gases described in clause 9.3.6.6 passes through the converter into the detector. The indicated concentration (b) shall be recorded (the analyzer is in the NO_x mode).

9.3.6.8 **NO mode**

Switched to NO mode with the ozonator deactivated, the flow of oxygen or synthetic air shall be shut off. The NO_x reading of the analyzer shall not deviate by more than ± 5 per cent from the value measured according to clause 9.3.6.2 (the analyzer is in the NO mode).

9.3.6.9 **Test interval**

The efficiency of the converter shall be tested at least once per month.

9.3.6.10 **Efficiency requirement**

The efficiency of the converter E NO_x shall not be less than 95 %.

If, with the analyzer in the most common range, the ozonator cannot give a reduction from 80 per cent to 20 per cent according to clause 9.3.6.5, the highest range which will give the reduction shall be used.

9.3.7 Adjustment of the FID

9.3.7.1 Optimization of the detector response

The FID shall be adjusted as specified by the instrument manufacturer. A propane in air span gas shall be used to optimize the response on the most common operating range.

With the fuel and airflow rates set at the manufacturer's recommendations, a 350 ± 75 ppm C span gas shall be introduced to the analyzer. The response at a given fuel flow shall be determined from the difference between the span gas response and the zero gas response. The fuel flow shall be incrementally adjusted above and below the manufacturer's specification. The span and zero response at these fuel flows shall be recorded. The difference between the span and zero response shall be plotted and the fuel flow adjusted to the rich side of the curve. This is the initial flow rate setting which may need further optimization depending on the results of the hydrocarbon response factors and the oxygen interference check according to clauses 9.3.7.2 and 9.3.7.3. If the oxygen interference or the hydrocarbon response factors do not meet the following specifications, the airflow shall be incrementally adjusted above and below the manufacturer's specifications, repeating clauses 9.3.7.2 and 9.3.7.3 for each flow.

The optimization may optionally be conducted using the procedures outlined in SAE paper No 770141.

9.3.7.2 Hydrocarbon Response Factors

A linearity verification of the analyzer shall be performed using propane in air and purified synthetic air according to clause 9.2.1.3 of this Chapter.

Response factors shall be determined when introducing an analyzer into service and after major service intervals. The response factor (r_h) for a particular hydrocarbon species is the ratio of the FID C1 reading to the gas concentration in the cylinder expressed by ppm C1.

The concentration of the test gas shall be at a level to give a response of approximately 80 per cent of full scale. The concentration shall be known to an accuracy of ± 2 per cent in reference to a gravimetric standard expressed in volume. In addition, the gas cylinder shall be preconditioned for 24 hours at a temperature of $298 \text{ K} \pm 5 \text{ K}$ ($25 \text{ }^\circ\text{C} \pm 5 \text{ }^\circ\text{C}$).

The test gases to be used and the relative response factor ranges are as follows:

- a) Methane and purified synthetic air $1.00 \leq r_h \leq 1.15$;
- b) Propylene and purified synthetic air $0.90 \leq r_h \leq 1.1$;
- c) Toluene and purified synthetic air $0.90 \leq r_h \leq 1.1$.

These values are relative to a r_h of 1 for propane and purified synthetic air.

9.3.7.3 Oxygen Interference Check

For raw exhaust gas analyzers only, the oxygen interference check shall be performed when introducing an analyzer into service and after major service intervals.

A measuring range shall be chosen where the oxygen interference check gases will fall in the upper 50 per cent. The test shall be conducted with the oven temperature set as required. Oxygen interference check gas specifications are found in clause 9.3.3.4 of this Chapter.

- a) The analyzer shall be set at zero;
- b) The analyzer shall be spanned with the 0 per cent oxygen blend for positive ignition engines. Compression ignition engine instruments shall be spanned with the 21 per cent oxygen blend.
- c) The zero response shall be rechecked. If it has changed by more than 0.5 per cent of full scale, steps (a) and (b) of this clause shall be repeated.
- d) The 5 per cent and 10 per cent oxygen interference check gases shall be introduced.
- e) The zero response shall be rechecked. If it has changed by more than ± 1 per cent of full scale, the test shall be repeated.
- f) The oxygen interference E_{O_2} shall be calculated for each mixture in step (d) as follows:

$$E_{O_2} = (c_{ref,d} - c) \times 100 / c_{ref,d} \quad (73)$$

With the analyzer response being

$$c = \frac{c_{ref,b} \times c_{FS,b}}{c_{m,b}} \times \frac{c_{m,d}}{c_{FS,d}} \quad (74)$$

Where:

$c_{ref,b}$ is the reference HC concentration in step (b), ppm C

$c_{ref,d}$ is the reference HC concentration in step (d), ppm C

$c_{FS,b}$ is the full scale HC concentration in step (b), ppm C

$c_{FS,d}$ is the full scale HC concentration in step (d), ppm C

$c_{m,b}$ is the measured HC concentration in step (b), ppm C

$c_{m,d}$ is the measured HC concentration in step (d), ppm C

- g) The oxygen interference E_{O_2} shall be less than ± 1.5 per cent for all required oxygen interference check gases prior to testing;
- h) If the oxygen interference E_{O_2} is greater than ± 1.5 per cent, corrective action may be taken by incrementally adjusting the airflow above and below the manufacturer's specifications, the fuel flow and the sample flow;
- i) The oxygen interference shall be repeated for each new setting

9.3.8 Efficiency of The Non-Methane Cutter (NMC)

The NMC is used for the removal of the non-methane hydrocarbons from the sample gas by oxidizing all hydrocarbons except methane. Ideally, the conversion for methane is 0 per cent, and for the other hydrocarbons represented by ethane is 100 per cent. For the accurate measurement of NMHC, the two efficiencies shall be determined and used for the calculation of the NMHC emission mass flow rate (see clause 8.6.2 of this Chapter).

9.3.8.1 Methane Efficiency

Methane calibration gas shall be flown through the FID with and without bypassing the NMC and the two concentrations recorded. The efficiency shall be determined as follows:

$$E_M = 1 - \frac{C_{HC(w/NMC)}}{C_{HC(w/o NMC)}} \quad (75)$$

Where:

$C_{HC(w/NMC)}$ is the HC concentration with CH_4 flowing through the NMC, ppm C

$C_{HC(w/o NMC)}$ is the HC concentration with CH_4 bypassing the NMC, ppm C

9.3.8.2 Ethane Efficiency

Methane calibration gas shall be flown through the FID with and without bypassing the NMC and the two concentrations recorded. The efficiency shall be determined as follows:

$$E_E = 1 - \frac{C_{HC(w/NMC)}}{C_{HC(w/o NMC)}} \quad (76)$$

Where:

$C_{HC(w/NMC)}$ is the HC concentration with C_2H_6 flowing through the NMC, ppm C

$C_{HC(w/o NMC)}$ is the HC concentration with C_2H_6 bypassing the NMC, ppm C

9.3.9 **Interference effects**

Other gases than the one being analyzed can interfere with the reading in several ways. Positive interference occurs in NDIR instruments where the interfering gas gives the same effect as the gas being measured, but to a lesser degree. Negative interference occurs in NDIR instruments by the interfering gas broadening the absorption band of the measured gas, and in CLD instruments by the interfering gas quenching the reaction. The interference checks in clauses 9.3.9.1 and 9.3.9.3 shall be performed prior to an analyzer's initial use and after major service intervals.

9.3.9.1 **CO analyzer interference check**

Water and CO₂ can interfere with the CO analyzer performance. Therefore, a CO₂ span gas having a concentration of 80 to 100 per cent of full scale of the maximum operating range used during testing shall be bubbled through water at room temperature and the analyzer response recorded. The analyzer response shall not be more than 2 per cent of the mean CO concentration expected during testing.

Interference procedures for CO₂ and H₂O may also be run separately. If the CO₂ and H₂O levels used are higher than the maximum levels expected during testing, each observed interference value shall be scaled down by multiplying the observed interference by the ratio of the maximum expected concentration value to the actual value used during this procedure. Separate interference procedures concentrations of H₂O that are lower than the maximum levels expected during testing may be run, but the observed H₂O interference shall be scaled up by multiplying the observed interference by the ratio of the maximum expected H₂O concentration value to the actual value used during this procedure. The sum of the two scaled interference values shall meet the tolerance specified in this clause.

9.3.9.2 **NO_x analyzer quench checks for CLD analyzer**

The two gases of concern for CLD (and HCLD) analyzers are CO₂ and water vapour. Quench responses to these gases are proportional to their concentrations, and therefore require test techniques to determine the quench at the highest expected concentrations experienced during testing. If the CLD analyzer uses quench compensation algorithms that utilize H₂O and/or CO₂ measurement instruments, quench shall be evaluated with these instruments active and with the compensation algorithms applied

9.3.9.2.1 **CO₂ quench check**

A CO₂ span gas having a concentration of 80 to 100 per cent of full scale of the maximum operating range shall be passed through the NDIR analyzer and the CO₂ value recorded as A. It shall then be diluted approximately 50 per cent with NO span gas and passed through the NDIR and CLD, with the CO₂ and NO values recorded as B and C, respectively. The CO₂ shall then be shut off and only the NO span gas be passed through the (H)CLD and the NO value recorded as D.

$$E_{CO_2} = \left[1 - \left(\frac{(C \times A)}{(D \times A) - (D \times B)} \right) \right] \times 100 \quad (77)$$

- A is the undiluted CO₂ concentration measured with NDIR, per cent
 B is the diluted CO₂ concentration measured with NDIR, per cent
 C is the diluted NO concentration measured with (H)CLD, ppm
 D is the undiluted NO concentration measured with (H)CLD, ppm

Alternative methods of diluting and quantifying of CO₂ and NO span gas values such as dynamic mixing/ blending are permitted with the approval of the Test Agency.

9.3.9.2.2 Water Quench Check

This check applies to wet gas concentration measurements only. Calculation of water quench shall consider dilution of the NO span gas with water vapour and scaling of water vapour concentration of the mixture to that expected during testing.

A NO span gas having a concentration of 80 per cent to 100 per cent of full scale of the normal operating range shall be passed through the (H)CLD and the NO value recorded as D. The NO span gas shall then be bubbled through water at room temperature and passed through the (H)CLD and the NO value recorded as C. The water temperature shall be determined and recorded as F. The mixture's saturation vapour pressure that corresponds to the bubbler water temperature (F) shall be determined and recorded as G.

The water vapour concentration (in per cent) of the mixture shall be calculated as follows:

$$H = 100 \times (G/p_b) \quad (78)$$

and recorded as H. The expected diluted NO span gas (in water vapour) concentration shall be calculated as follows:

$$D_e = D \times (1 - H/100) \quad (79)$$

and recorded as D_e . The maximum exhaust water vapour concentration (in per cent) expected during testing shall be estimated from the maximum CO₂ concentration in the exhaust gas A as follows:

$$H_m = \alpha/2 \times A \quad (80)$$

and recorded as H_m

The per cent water quench shall be calculated as follows:

$$E_{H_2O} = 100 \times ((D_e - C)/D_e) \times (H_m/H) \quad (81)$$

- D_e is the expected diluted NO concentration, ppm
 C is the measured diluted NO concentration, ppm
 H_m is the maximum water vapour concentration, per cent
 H is the actual water vapour concentration, per cent

9.3.9.2.3 **Maximum allowable quench**

The combined CO₂ and water quench shall not exceed 2 per cent of full scale.

9.3.9.3 **NO_x analyzer quench check for NDUV analyzer**

Hydrocarbons and H₂O can positively interfere with a NDUV analyzer by causing a response similar to NO_x. If the NDUV analyzer uses compensation algorithms that utilize measurements of other gases to meet this interference verification, simultaneously such measurements shall be conducted to test the algorithms during the analyzer interference verification.

9.3.9.3.1 **Procedure**

The NDUV analyzer shall be started, operated, zeroed, and spanned according to the instrument manufacturer's instructions. It is recommended to extract engine exhaust to perform this verification. A CLD shall be used to quantify NO_x in the exhaust. The CLD response shall be used as the reference value. Also HC shall be measured in the exhaust with a FID analyzer. The FID response shall be used as the reference hydrocarbon value.

Upstream of any sample dryer, if used during testing, the engine exhaust shall be introduced into the NDUV analyzer. Time shall be allowed for the analyzer response to stabilize. Stabilization time may include time to purge the transfer line and to account for analyzer response. While all analyzers measure the sample's concentration, 30 seconds of sampled data shall be recorded, and the arithmetic means for the three analyzers calculated.

The CLD mean value shall be subtracted from the NDUV mean value. This difference shall be multiplied by the ratio of the expected mean HC concentration to the HC concentration measured during the verification, as follows:

$$E_{HC/H_2O} = (c_{NO_x,CLD} - c_{NO_x,NDUV}) \times \left(\frac{c_{HC,e}}{c_{HC,m}} \right) \quad (82)$$

$c_{NO_x,CLD}$ is the measured NO_x concentration with CLD, ppm

$c_{NO_x,NDUV}$ is the measured NO_x concentration with NDUV, ppm

$c_{HC,e}$ is the expected max. HC concentration, ppm

$c_{HC,m}$ is the measured HC concentration, ppm

9.3.9.3.2 **Maximum allowable quench**

The combined HC and water quench shall not exceed 2 per cent of the NO_x concentration expected during testing.

9.3.9.4 **Sample dryer**

A sample dryer removes water, which can otherwise interfere with a NO_x measurement

9.3.9.4.1 **Sample Dryer Efficiency**

For dry CLD analyzers, it shall be demonstrated that for the highest expected water vapour concentration H_m (see clause 9.3.9.2.2), the sample dryer maintains CLD humidity at ≤ 5 g water/kg dry air (or about 0.008 per cent H_2O), which is 100 per cent relative humidity at 3.9 °C and 101.3 kPa. This humidity specification is also equivalent to about 25 per cent relative humidity at 25 °C and 101.3 kPa. This may be demonstrated by measuring the temperature at the outlet of a thermal dehumidifier, or by measuring humidity at a point just upstream of the CLD. Humidity of the CLD exhaust might also be measured as long as the only flow into the CLD is the flow from the dehumidifier.

9.3.9.4.2 **Sample Dryer NO₂ Penetration**

Liquid water remaining in an improperly designed sample dryer can remove NO₂ from the sample. If a sample dryer is used in combination with an NDUV analyzer without an NO₂ /NO converter upstream, it could therefore remove NO₂ from the sample prior NOx measurement.

The sample dryer shall allow for measuring at least 95 per cent of the total NO₂ at the maximum expected concentration of NO₂.

9.3.10 **Sampling for raw gaseous emissions, if applicable**

The gaseous emissions sampling probes shall be fitted at least 0.5 m or three times the diameter of the exhaust pipe - whichever is the larger - upstream of the exit of the exhaust gas system but sufficiently close to the engine as to ensure an exhaust gas temperature of at least 343 K (70 °C) at the probe.

In the case of a multi-cylinder engine with a branched exhaust manifold, the inlet of the probe shall be located sufficiently far downstream so as to ensure that the sample is representative of the average exhaust emissions from all cylinders. In multi-cylinder engines having distinct groups of manifolds, such as in a "Vee" engine configuration, it is recommended to combine the manifolds upstream of the sampling probe. If this is not practical, it is permissible to acquire a sample from the group with the highest CO₂ emission. For exhaust emission calculation the total exhaust mass flow shall be used.

If the engine is equipped with an exhaust after-treatment system, the exhaust sample shall be taken downstream of the exhaust after-treatment system.

9.3.11 **Sampling for dilute gaseous emissions, if applicable**

The exhaust pipe between the engine and the full flow dilution system shall conform to the requirements laid down in Appendix 2 of this Chapter. The gaseous emissions sample probe(s) shall be installed in the dilution tunnel at a point where the diluent and exhaust gas are well mixed, and in close proximity to the particulates sampling probe.

Sampling can generally be done in two ways:

- (a) The emissions are sampled into a sampling bag over the cycle and measured after completion of the test; for HC, the sample bag shall be heated to 464 ± 11 K (191 ± 11 °C), for NO_x, the sample bag temperature shall be above the dew point temperature;
- (b) The emissions are sampled continuously and integrated over the cycle.

The background concentration shall be determined upstream of the dilution tunnel according to (a) or (b), and shall be subtracted from the emissions concentration according to clause 8.5.2.3.2 of this Chapter.

9.4 Particulate Measurement and Sampling System

9.4.1 General specifications

To determine the mass of the particulates, a particulate dilution and sampling system, a particulate sampling filter, a microgram balance, and a temperature and humidity controlled weighing chamber, are required. The particulate sampling system shall be designed to ensure a representative sample of the particulates proportional to the exhaust flow.

9.4.2 General requirements of the dilution system

The determination of the particulates requires dilution of the sample with filtered ambient air, synthetic air or nitrogen (the diluent). The dilution system shall be set as follows:

- a) Completely eliminate water condensation in the dilution and sampling systems;
- b) Maintain the temperature of the diluted exhaust gas between 315 K (42 °C) and 325 K (52 °C) within 20 cm upstream or downstream of the filter holder(s);
- c) The diluent temperature shall be between 293 K and 315 K (20 °C to 42 °C) in close proximity to the entrance into the dilution tunnel;
- d) The minimum dilution ratio shall be within the range of 5:1 to 7:1 and at least 2:1 for the primary dilution stage based on the maximum engine exhaust flow rate;
- e) For a partial flow dilution system, the residence time in the system from the point of diluent introduction to the filter holder(s) shall be between 0.5 and 5 seconds;
- f) For a full flow dilution system, the overall residence time in the system from the point of diluent introduction to the filter holder(s) shall be between 1 and 5 seconds, and the residence time in the secondary dilution system, if used, from the point of secondary diluent introduction to the filter holder(s) shall be at least 0.5 seconds.

Dehumidifying the diluent before entering the dilution system is permitted, and especially useful if diluent humidity is high.

9.4.3 **Particulate Sampling**

9.4.3.1 **Partial flow dilution system**

The particulate sampling probe shall be installed in close proximity to the gaseous emissions sampling probe, but sufficiently distant as to not cause interference. Therefore, the installation provisions of clause 9.3.10 of this Chapter also apply to particulate sampling. The sampling line shall conform to the requirements laid down in Appendix 2 of this Chapter.

In the case of a multi-cylinder engine with a branched exhaust manifold, the inlet of the probe shall be located sufficiently far downstream so as to ensure that the sample is representative of the average exhaust emissions from all cylinders. In multi-cylinder engines having distinct groups of manifolds, such as in a "Vee" engine configuration, it is recommended to combine the manifolds upstream of the sampling probe. If this is not practical, it is permissible to acquire a sample from the group with the highest particulate emission. For exhaust emission calculation the total exhaust mass flow of the manifold shall be used.

9.4.3.2 **Full flow dilution system**

The particulate sampling probe shall be installed in close proximity to the gaseous emissions sampling probe, but sufficiently distant as to not cause interference, in the dilution tunnel. Therefore, the installation provisions of clause 9.3.11 of this Chapter also apply to particulate sampling. The sampling line shall conform to the requirements laid down in Appendix 2 of this Chapter.

9.4.4 **Particulate sampling filters**

The diluted exhaust shall be sampled by a filter that meets the requirements of clause 9.4.4.1 to 9.4.4.3 during the test sequence.

9.4.4.1 **Filter specification**

All filter types shall have a 0.3 µm DOP (di-octylphthalate) or PAO (poly-alpha-olefin) collection efficiency of at least 99 per cent. The sample filter manufacturer's measurements reflected in their product ratings may be used to show this requirement. The filter material shall be either:

- a) Fluorocarbon (PTFE) coated glass fibre, or
- b) Fluorocarbon (PTFE) membrane.

9.4.4.2 **Filter size**

The filter shall be circular with a nominal diameter of 47 mm (tolerance of 46.50 ± 0.6 mm) and an exposed diameter (filter stain diameter) of at least 38 mm.

9.4.4.3 **Filter face velocity**

The face velocity through the filter shall be between 0.90 and 1.00 m/s with less than 5 per cent of the recorded flow values exceeding this range. If the total PM mass on the filter exceeds 400 µg, the filter face velocity may be reduced to 0.50 m/s. The face velocity shall be calculated as the volumetric flow rate of the sample at the pressure upstream of the filter and temperature of the filter face, divided by the filter's exposed area.

9.4.5 **Weighing chamber and analytical balance specifications**

The chamber (or room) environment shall be free of any ambient contaminants (such as dust, aerosol, or semi-volatile material) that could contaminate the particulate filters. The weighing room shall meet the required specifications for at least 60 min before weighing filters.

9.4.5.1 **Weighing Chamber Conditions**

The temperature of the chamber (or room) in which the particulate filters are conditioned and weighed shall be maintained to within $295 \text{ K} \pm 1 \text{ K}$ ($22 \text{ }^{\circ}\text{C} \pm 1 \text{ }^{\circ}\text{C}$) during all filter conditioning and weighing. The humidity shall be maintained to a dew point of $282.5 \text{ K} \pm 1 \text{ K}$ ($9.5 \text{ }^{\circ}\text{C} \pm 1 \text{ }^{\circ}\text{C}$).

If the stabilization and weighing environments are separate, the temperature of the stabilization environment shall be maintained at a tolerance of $295 \text{ K} \pm 3 \text{ K}$ ($22 \text{ }^{\circ}\text{C} \pm 3 \text{ }^{\circ}\text{C}$), but the dew point requirement remains at $282.5 \text{ K} \pm 1 \text{ K}$ ($9.5 \text{ }^{\circ}\text{C} \pm 1 \text{ }^{\circ}\text{C}$).

Humidity and ambient temperature shall be recorded.

9.4.5.2 **Reference filter weighing**

At least two unused reference filters shall be weighed within 12 hours of, but preferably at the same time as the sample filter weighing. They shall be the same material as the sample filters. Buoyancy correction shall be applied to the weighings.

If the weight of any of the reference filters changes between sample filter weighing by more than 10 µg, all sample filters shall be discarded and the emissions test repeated.

The reference filters shall be periodically replaced based on good engineering judgement, but at least once per year.

9.4.5.3 **Analytical Balance**

The analytical balance used to determine the filter weight shall meet the linearity verification criterion of clause 9.2, Table 7 of this Chapter. This implies a precision (standard deviation) of at least 2 µg and a resolution of at least 1 µg (1 digit = 1 µg).

In order to ensure accurate filter weighing, it is recommended that the balance be installed as follows:

- (a) Installed on a vibration-isolation platform to isolate it from external noise and vibration;
- (b) Shielded from convective airflow with a static-dissipating draft shield that is electrically grounded.

9.4.5.4 **Elimination of Static Electricity Effects**

The filter shall be neutralized prior to weighing, e.g. by a Polonium neutralizer or a device of similar effect. If a PTFE membrane filter is used, the static electricity shall be measured and is recommended to be within ± 2.0 V of neutral.

Static electric charge shall be minimized in the balance environment. Possible methods are as follows:

- (a) The balance shall be electrically grounded;
- (b) Stainless steel tweezers shall be used if PM samples are handled manually;
- (c) Tweezers shall be grounded with a grounding strap, or a grounding strap shall be provided for the operator such that the grounding strap shares a common ground with the balance. Grounding straps shall have an appropriate resistor to protect operators from accidental shock.

9.4.5.5 **Additional specifications**

All parts of the dilution system and the sampling system from the exhaust pipe up to the filter holder, which are in contact with raw and diluted exhaust gas, shall be designed to minimize deposition or alteration of the particulates. All parts shall be made of electrically conductive materials that do not react with exhaust gas components, and shall be electrically grounded to prevent electrostatic effects.

9.4.5.6 **Calibration of The Flow Measurement Instrumentation**

Each flowmeter used in a particulate sampling and partial flow dilution system shall be subjected to the linearity verification, as described in clause 9.2.1 of this Chapter, as often as necessary to fulfil the accuracy requirements of this Part. For the flow reference values, an accurate flowmeter traceable to international and/or national standards shall be used. For differential flow measurement calibration see clause 9.4.6.2. of this Chapter.

9.4.6 **Special requirements for the partial flow dilution system**

The partial flow dilution system has to be designed to extract a proportional raw exhaust sample from the engine exhaust stream, thus responding to excursions in the exhaust stream flow rate. For this it is essential that the dilution ratio or the sampling ratio r_d or r_s be determined such that the accuracy requirements of clause 9.4.6.2 are fulfilled.

9.4.6.1 System Response Time

For the control of a partial flow dilution system, a fast system response is required. The transformation time for the system shall be determined by the procedure in clause 9.4.6.6. If the combined transformation time of the exhaust flow measurement (see clause 8.4.1.2 of this Chapter) and the partial flow system is ≤ 0.3 second, online control shall be used. If the transformation time exceeds 0.3 second, look ahead control based on a pre-recorded test run shall be used. In this case, the combined rise time shall be ≤ 1 second and the combined delay time ≤ 10 seconds.

The total system response shall be designed as to ensure a representative sample of the particulates, $q_{mp,i}$, proportional to the exhaust mass flow. To determine the proportionality, a regression analysis of $q_{mp,i}$ versus $q_{mew,i}$ shall be conducted on a minimum 5 Hz data acquisition rate, and the following criteria shall be met:

- (a) The coefficient of determination r^2 of the linear regression between $q_{mp,i}$ and $q_{mew,i}$ shall not be less than 0.95;
- (b) The standard error of estimate of $q_{mp,i}$ on $q_{mew,i}$ shall not exceed 5 per cent of q_{mp} maximum;
- (c) q_{mp} intercept of the regression line shall not exceed ± 2 per cent of q_{mp} maximum.

Look-ahead control is required if the combined transformation times of the particulate system, $t_{50,P}$ and of the exhaust mass flow signal, $t_{50,F}$ are > 0.3 second. In this case, a pre-test shall be run, and the exhaust mass flow signal of the pre-test be used for controlling the sample flow into the particulate system. A correct control of the partial dilution system is obtained, if the time trace of $q_{mew,pre}$ of the pre-test, which controls q_{mp} , is shifted by a "look-ahead" time of $t_{50,P} + t_{50,F}$.

For establishing the correlation between $q_{mp,i}$ and $q_{mew,i}$ the data taken during the actual test shall be used, with $q_{mew,i}$ time aligned by $t_{50,F}$ relative to $q_{mp,i}$ (no contribution from $t_{50,P}$ to the time alignment). That is, the time shift between q_{mew} and q_{mp} is the difference in their transformation times that were determined in clause 9.4.6.6.

9.4.6.2 Specifications for differential flow measurement

For partial flow dilution systems, the accuracy of the sample flow q_{mp} is of special concern, if not measured directly, but determined by differential flow measurement:

$$q_{mp} = q_{medw} - q_{mdw} \quad (83)$$

In this case, the maximum error of the difference shall be such that the accuracy of q_{mp} is within ± 5 per cent when the dilution ratio is

less than 15. It can be calculated by taking root-mean-square of the errors of each instrument.

Acceptable accuracies of q_{mp} can be obtained by either of the following methods:

- (a) The absolute accuracies of q_{mdew} and q_{mdw} are ± 0.2 per cent which guarantees an accuracy of q_{mp} of ≤ 5 per cent at a dilution ratio of 15. However, greater errors will occur at higher dilution ratios;
- (b) Calibration of q_{mdw} relative to q_{mdew} is carried out such that the same accuracies for q_{mp} as in (a) are obtained. For details see clause 9.4.6.3;
- (c) The accuracy of q_{mp} is determined indirectly from the accuracy of the dilution ratio as determined by a tracer gas, e.g. CO₂. Accuracies equivalent to method (a) for q_{mp} are required;
- (d) The absolute accuracy of q_{mdew} and q_{mdw} is within ± 2 per cent of full scale, the maximum error of the difference between q_{mdew} and q_{mdw} is within 0.2 per cent, and the linearity error is within ± 0.2 per cent of the highest q_{mdew} observed during the test.

9.4.6.3

Calibration of Differential Flow Measurement

The flowmeter or the flow measurement instrumentation shall be calibrated in one of the following procedures, such that the probe flow q_{mp} into the tunnel shall fulfil the accuracy requirements of clause 9.4.6.2:

- (a) The flowmeter for q_{mdw} shall be connected in series to the flowmeter for q_{mdew} , the difference between the two flowmeters shall be calibrated for at least five set points with flow values equally spaced between the lowest q_{mdw} value used during the test and the value of q_{mdew} used during the test. The dilution tunnel may be bypassed;
- (b) A calibrated flow device shall be connected in series to the flowmeter for q_{mdew} and the accuracy shall be checked for the value used for the test. The calibrated flow device shall be connected in series to the flowmeter for q_{mdw} , and the accuracy shall be checked for at least five settings corresponding to dilution ratio between 3 and 50, relative to q_{mdew} used during the test;
- (c) The transfer tube (TT) shall be disconnected from the exhaust, and a calibrated flow-measuring device with a suitable range to measure q_{mp} shall be connected to the transfer tube. q_{mdew} shall be set to the value used during the test, and q_{mdw} shall be sequentially set to at least five values corresponding to dilution ratios between 3 and 50. Alternatively, a special calibration flow path may be provided, in which the tunnel is bypassed, but the total and diluent flow through the corresponding meters as in the actual test;

- (d) A tracer gas shall be fed into the exhaust transfer tube TT. This tracer gas may be a component of the exhaust gas, like CO₂ or NO_x. After dilution in the tunnel the tracer gas component shall be measured. This shall be carried out for five dilution ratios between 3 and 50. The accuracy of the sample flow shall be determined from the dilution ratio r_d :

$$q_{mp} = q_{mdew}/r_d \quad (84)$$

The accuracies of the gas analyzers shall be taken into account to guarantee the accuracy of q_{mp} .

9.4.6.4 Carbon flow check

A carbon flow check using actual exhaust is strongly recommended for detecting measurement and control problems and verifying the proper operation of the partial flow system. The carbon flow check should be run at least each time a new engine is installed, or something significant is changed in the test cell configuration.

The engine shall be operated at peak torque load and speed or any other steady state mode that produces 5 per cent or more of CO₂. The partial flow sampling system shall be operated with a dilution factor of about 15 to 1.

If a carbon flow check is conducted, the procedure given in Appendix 4 shall be applied. The carbon flow rates shall be calculated according to equations 112 to 114 in Appendix 4 of this Chapter. All carbon flow rates should agree to within 3 per cent.

9.4.6.5 Pre-test check

A pre-test check shall be performed within 2 hours before the test run in the following way.

The accuracy of the flowmeters shall be checked by the same method as used for calibration (see clause 9.4.6.2) for at least two points, including flow values of q_{mdw} that correspond to dilution ratios between 5 and 15 for the q_{mdew} value used during the test.

If it can be demonstrated by records of the calibration procedure under clause 9.4.6.2 that the flowmeter calibration is stable over a longer period of time, the pre-test check may be omitted.

9.4.6.6 Determination of the Transformation Time

The system settings for the transformation time evaluation shall be exactly the same as during measurement of the test run. The transformation time shall be determined by the following method.

An independent reference flowmeter with a measurement range appropriate for the probe flow shall be put in series with and closely coupled to the probe. This flowmeter shall have a transformation time of less than 100 ms for the flow step size used in the response time measurement, with flow restriction sufficiently low as to not affect the dynamic performance of the partial flow dilution system, and consistent with good engineering practice.

A step change shall be introduced to the exhaust flow (or airflow if exhaust flow is calculated) input of the partial flow dilution system, from a low flow to at least 90 per cent of maximum exhaust flow. The trigger for the step change shall be the same one used to start the look-ahead control in actual testing. The exhaust flow step stimulus and the flowmeter response shall be recorded at a sample rate of at least 10 Hz.

From this data, the transformation time shall be determined for the partial flow dilution system, which is the time from the initiation of the step stimulus to the 50 per cent point of the flowmeter response. In a similar manner, the transformation times of the q_{mp} signal of the partial flow dilution system and of the $q_{mew,i}$ signal of the exhaust flowmeter shall be determined. These signals are used in the regression checks performed after each test (see clause 9.4.6.1).

The calculation shall be repeated for at least 5 rise and fall stimuli, and the results shall be averaged. The internal transformation time (< 100 ms) of the reference flowmeter shall be subtracted from this value. This is the "look-ahead" value of the partial flow dilution system, which shall be applied in accordance with clause 9.4.6.1.

9.5 Calibration of The CVS System

9.5.1 General

The CVS system shall be calibrated by using an accurate flowmeter and a restricting device. The flow through the system shall be measured at different restriction settings, and the control parameters of the system shall be measured and related to the flow.

Various types of flowmeters may be used, e.g. calibrated venturi, calibrated laminar flowmeter, calibrated turbine meter.

9.5.2 Calibration of the positive displacement pump (PDP)

All the parameters related to the pump shall be simultaneously measured along with the parameters related to a calibration venturi which is connected in series with the pump. The calculated flow rate (in m^3/s at pump inlet, absolute pressure and temperature) shall be plotted versus a correlation function which is the value of a specific combination of pump parameters. The linear equation which relates the pump flow and the correlation function shall be determined. If a CVS has a multiple speed drive, the calibration shall be performed for each range used.

Temperature stability shall be maintained during calibration.

Leaks in all the connections and ducting between the calibration venturi and the CVS pump shall be maintained lower than 0.3 per cent of the lowest flow point (highest restriction and lowest PDP speed point).

9.5.2.1 **Data Analysis**

The airflow rate (q_{vCVS}) at each restriction setting (minimum six settings) shall be calculated in standard m^3/s from the flowmeter data using the manufacturer's prescribed method. The airflow rate shall then be converted to pump flow (V_0) in m^3/rev at absolute pump inlet temperature and pressure as follows:

$$V_0 = \frac{q_{vCVS}}{n} \times \frac{T}{273} \times \frac{101.3}{p_p} \quad (85)$$

Where:

q_{vCVS} is the airflow rate at standard conditions (101.3 kPa, 273 K), m^3/s

T is the temperature at pump inlet, K

p_p is the absolute pressure at pump inlet, kPa

n is the pump speed,

To account for the interaction of pressure variations at the pump and the pump slip rate, the correlation function (X_0) between pump speed, pressure differential from pump inlet to pump outlet and absolute pump outlet pressure shall be calculated as follows:

$$X_0 = \frac{1}{n} \times \sqrt{\frac{\Delta p_p}{p_p}} \quad (86)$$

Where:

Δp_p is the pressure differential from pump inlet to pump outlet, kPa

p_p is the absolute outlet pressure at pump outlet, kPa

A linear least-square fit shall be performed to generate the calibration equation as follows:

$$V_0 = D_0 - m \times X_0 \quad (87)$$

D_0 and m are the intercept and slope, respectively, describing the regression lines.

For a CVS system with multiple speeds, the calibration curves generated for the different pump flow ranges shall be approximately parallel, and the intercept values (D_0) shall increase as the pump flow range decreases.

The calculated values from the equation shall be within ± 0.5 per cent of the measured value of V_0 . Values of m will vary from one pump to another. Particulate influx over time will cause the pump slip to decrease, as reflected by lower values for m. Therefore, calibration shall be performed at pump start-up, after major maintenance, and if the total system verification indicates a change of the slip rate.

9.5.3 Calibration of the critical flow venturi (CFV)

Calibration of the CFV is based upon the flow equation for a critical venturi. Gas flow is a function of venturi inlet pressure and temperature.

To determine the range of critical flow, K_v shall be plotted as a function of venturi inlet pressure. For critical (choked) flow, K_v will have a relatively constant value. As pressure decreases (vacuum increases), the venturi becomes unchoked and K_v decreases, which indicates that the CFV is operated outside the permissible range.

9.5.3.1 Data Analysis

The airflow rate (q_{vCVS}) at each restriction setting (minimum 8 settings) shall be calculated in standard m^3/s from the flowmeter data using the manufacturer's prescribed method. The calibration coefficient shall be calculated from the calibration data for each setting as follows:

$$K_v = \frac{q_{vCVS} \times \sqrt{T}}{p_p} \quad (88)$$

Where:

q_{vCVS} is the airflow rate at standard conditions (101.3 kPa, 273 K), m^3/s

T is the temperature at the venturi inlet, K

p_p is the absolute pressure at venturi inlet, kPa

The average K_v and the standard deviation shall be calculated. The standard deviation shall not exceed ± 0.3 per cent of the average K_v .

9.5.4 Calibration of the subsonic venturi (SSV)

Calibration of the SSV is based upon the flow equation for a subsonic venturi. Gas flow is a function of inlet pressure and temperature, pressure drop between the SSV inlet and throat, as shown in equation 53 (see clause 8.5.1.4 of this Chapter).

9.5.4.1 Data analysis

The airflow rate (Q_{SSV}) at each restriction setting (minimum 16 settings) shall be calculated in standard m^3/s from the flowmeter data using the manufacturer's prescribed method. The discharge coefficient shall be calculated from the calibration data for each setting as follows:

$$C_d = \frac{Q_{SSV}}{d_v^2 \times p_p \times \sqrt{\left[\frac{1}{T} (r_p^{1.4286} - r_p^{1.7143}) \times \left(\frac{1}{1 - r_d^4 r_p^{1.4286}} \right) \right]}} \quad (89)$$

Where:

Q_{SSV} is the airflow rate at standard conditions (101.3 kPa, 273 K) m^3/s

T is the temperature at the venturi inlet, K

d_v is the diameter of the SSV throat, m

r_p is the ratio of the SSV throat to inlet absolute static pressure $= 1 - \frac{\Delta p}{p_p}$

r_D is the ratio of the SSV throat diameter, d_v , to the inlet pipe inner diameter D

To determine the range of subsonic flow, C_d shall be plotted as a function of Reynolds number Re, at the SSV throat. The Re at the SSV throat shall be calculated with the following equation:

$$Re = A_1 \times \frac{Q_{SSV}}{d_v \times \mu} \quad (90)$$

With

$$\mu = \frac{b \times T^{1.5}}{S + T} \quad (91)$$

Where:

A_1 is 25.55152 in SI units of $\left(\frac{1}{m^3}\right) \left(\frac{min}{s}\right) \left(\frac{mm}{m}\right)$

Q_{SSV} is the airflow rate at standard conditions (101,3 kPa, 273 K), m^3/s

d_v is the diameter of the SSV throat, m

μ is the absolute or dynamic viscosity of the gas, kg/ms

b is 1.458×10^6 (empirical constant), kg/ms K^{0.5}

S is 110.4 (empirical constant), K

Because Q_{SSV} is an input to the Re equation, the calculations shall be started with an initial guess for Q_{SSV} or C_d of the calibration venturi, and repeated until Q_{SSV} converges. The convergence method shall be accurate to 0.1 per cent of point or better.

For a minimum of sixteen points in the region of subsonic flow, the calculated values of C_d from the resulting calibration curve fit equation shall be within ± 0.5 per cent of the measured C_d for each calibration point.

9.5.5

Total System Verification

The total accuracy of the CVS sampling system and analytical system shall be determined by introducing a known mass of a pollutant gas into the system while it is being operated in the normal manner. The pollutant is analyzed, and the mass calculated according to clause 8.5.2.3 of this Chapter except in the case of propane where a u factor of 0.000472 is used in place of 0.000480 for HC. Either of the following two techniques shall be used.

9.5.5.1 **Metering with A Critical Flow Orifice**

A known quantity of pure gas (carbon monoxide or propane) shall be fed into the CVS system through a calibrated critical orifice. If the inlet pressure is high enough, the flow rate, which is adjusted by means of the critical flow orifice, is independent of the orifice outlet pressure (critical flow). The CVS system shall be operated as in a normal exhaust emission test for about 5 to 10 minutes. A gas sample shall be analyzed with the usual equipment (sampling bag or integrating method), and the mass of the gas calculated.

The mass so determined shall be within ± 3 per cent of the known mass of the gas injected.

9.5.5.2 **Metering by means of a gravimetric technique**

The mass of a small cylinder filled with carbon monoxide or propane shall be determined with a precision of ± 0.01 g. For about 5 to 10 minutes, the CVS system shall be operated as in a normal exhaust emission test, while carbon monoxide or propane is injected into the system. The quantity of pure gas discharged shall be determined by means of differential weighing. A gas sample shall be analyzed with the usual equipment (sampling bag or integrating method), and the mass of the gas calculated.

The mass so determined shall be within ± 3 per cent of the known mass of the gas injected.

10.0 **PARTICLE NUMBER MEASUREMENT TEST PROCEDURE**

10.1 **Sampling**

Particle number emissions shall be measured by continuous sampling from either a partial flow dilution system, as described in Appendix 2 of this Chapter, clause A.2.2.1 and A.2.2.2 or a full flow dilution system as described in Appendix 2 of this Chapter, clause A.2.2.3 and A.2.2.4.

10.1.1 **Diluent Filtration**

Diluent used for both the primary and, where applicable, secondary dilution of the exhaust in the dilution system shall be passed through filters meeting the High-Efficiency Particulate Air (HEPA) filter requirements defined in Appendix 2 of this Chapter, clause A.2.2.2 or A.2.2.4. The diluent may optionally be charcoal scrubbed before being passed to the HEPA filter to reduce and stabilize the hydrocarbon concentrations in the diluent. It is recommended that an additional coarse particle filter is situated before the HEPA filter and after the charcoal scrubber, if used.

10.2 **Compensating for particle number sample flow – full flow dilution systems**

To compensate for the mass flow extracted from the dilution system for particle number sampling the extracted mass flow (filtered) shall be returned to the dilution system. Alternatively, the total mass flow in the dilution system may be mathematically corrected for the particle number sample flow extracted. Where the total mass flow extracted from the dilution system for the sum of particle number sampling and particulate mass sampling is less than 0.5 per cent of the total dilute exhaust gas flow in the dilution tunnel (m_{ed}) this correction, or flow return, may be neglected.

10.3 **Compensating for particle number sample flow – Partial flow dilution systems**

10.3.1 For partial flow dilution systems, the mass flow extracted from the dilution system for particle number sampling shall be accounted for in controlling the proportionality of sampling. This shall be achieved either by feeding the particle number sample flow back into the dilution system upstream of the flow measuring device or by mathematical correction as outlined in clause 10.3.2. In the case of total sampling type partial flow dilution systems, the mass flow extracted for particle number sampling shall also be corrected for in the particulate mass calculation as outlined in clause 10.3.3.

10.3.2 The instantaneous exhaust gas flow rate into the dilution system (q_{mp}), used for controlling the proportionality of sampling, shall be corrected according to one of the following methods:

- (a) In the case where the extracted particle number sample flow is discarded, equation 83 in clause 9.4.6.2. of this Chapter shall be replaced by the following:

$$q_{mp} = q_{medw} - q_{mdw} + q_{ex} \quad (92)$$

Where:

q_{mp} = sample flow of exhaust gas into partial flow dilution system, kg/s,

q_{medw} = diluted exhaust mass flow rate, kg/s,

q_{mdw} = dilution air mass flow rate, kg/s,

q_{ex} = particle number sample mass flow rate, kg/s.

The q_{ex} signal sent to the partial flow system controller shall be accurate to within 0.1 per cent of q_{medw} at all times and should be sent with frequency of at least 1 Hz.

- (b) In the case where the extracted particle number sample flow is fully or partially discarded, but an equivalent flow is fed back to the dilution system upstream of the flow measurement device, equation 83 in clause 9.4.6.2 of this Chapter shall be replaced by the following:

$$q_{mp} = q_{medw} - q_{mdw} + q_{ex} - q_{sw} \quad (93)$$

Where:

q_{mp} = sample flow of exhaust gas into partial flow dilution system, kg/s,

q_{mdew} = diluted exhaust mass flow rate, kg/s,

q_{mdw} = dilution air mass flow rate, kg/s,

q_{ex} = particle number sample mass flow rate, kg/s,

q_{sw} = mass flow rate fed back into dilution tunnel to compensate for particle number sample extraction, kg/s.

The difference between q_{ex} and q_{sw} sent to the partial flow system controller shall be accurate to within 0.1 per cent of q_{mdew} at all times. The signal (or signals) should be sent with frequency of at least 1 Hz.

10.3.3

Correction of PM measurement

When a particle number sample flow is extracted from a total sampling partial flow dilution system, the mass of particulates (m_{PM}) calculated in clause 8.4.3.2.1 or 8.4.3.2.2 of this Chapter shall be corrected as follows to account for the flow extracted. This correction is required even where filtered extracted flow is fed back into the partial flow dilution systems.

$$m_{PM,corr} = m_{PM} \times \frac{m_{sed}}{(m_{sed} - m_{ex})} \quad (94)$$

Where:

$m_{PM,corr}$ = mass of particulates corrected for extraction of particle number sample flow, g/test,

m_{PM} = mass of particulates determined according to clause 8.4.3.2.1 or 8.4.3.2.2 of this Chapter, g/test,

m_{sed} = total mass of diluted exhaust gas passing through the dilution tunnel, kg,

m_{ex} = total mass of diluted exhaust gas extracted from the dilution tunnel for particle number sampling, kg.

10.3.4

Proportionality of Partial Flow Dilution Sampling

For particle number measurement, exhaust mass flow rate, determined according to any of the methods described in clauses 8.4.1.3 to 8.4.1.7 of this Chapter, is used for controlling the partial flow dilution system to take a sample proportional to the exhaust mass flow rate. The quality of proportionality shall be checked by applying a regression analysis between sample and exhaust flow in accordance with clause 9.4.6.1 of this Chapter.

10.4 Determination of particle numbers

10.4.1 Time alignment

For partial flow dilution systems residence time in the particle number sampling and measurement system shall be accounted for by time aligning the particle number signal with the test cycle and the exhaust gas mass flow rate according to the procedure in clause 8.4.2.2 of this Chapter. The transformation time of the particle number sampling and measurement system shall be determined according to clause A.8.1.3.7 of Appendix 8 of this Chapter.

10.4.2 Determination of particle numbers with a partial flow dilution system

Where particle numbers are sampled using a partial flow dilution system according to the procedures set out in clause 8.4. of this Chapter, the number of particles emitted over the test cycle shall be calculated by means of the following equation:

$$N = \frac{m_{edf}}{1.293} \times k \times \bar{c}_s \times \bar{f}_r \times 10^6 \quad (95)$$

Where:

N = number of particles emitted over the test cycle,

m_{edf} = mass of equivalent diluted exhaust gas over the cycle, determined according to clause 8.4.3.2.2, kg/test,

k = calibration factor to correct the particle number counter measurements to the level of the reference instrument where this is not applied internally within the particle number counter. Where the calibration factor is applied internally within the particle number counter, a value of 1 shall be used for k in the above equation,

\bar{c}_s = average concentration of particles from the diluted exhaust gas corrected to standard conditions (273.2 K and 101.33 kPa), particles per cubic centimetre,

\bar{f}_r = mean particle concentration reduction factor of the volatile particle remover specific to the dilution settings used for the test.

\bar{c}_s = shall be calculated from the following equation:

$$\bar{c}_s = \frac{\sum_{i=1}^n c_{s,i}}{n} \quad (96)$$

Where:

$c_{s,i}$ = a discrete measurement of particle concentration in the diluted gas exhaust from the particle counter, corrected for coincidence and to standard conditions (273.2 K and 101.33 kPa), particles per cubic centimetre,

n = number of particle concentration measurements taken over the duration of the test.

10.4.3 **Determination of particle numbers with a full flow dilution system**

Where particle numbers are sampled using a full flow dilution system according to the procedures set out in clause 8.5. of this Chapter, the number of particles emitted over the test cycle shall be calculated by means of the following equation:

$$N = \frac{m_{edf}}{1.293} \times k \times \bar{c}_s \times \bar{f}_r \times 10^6 \quad (97)$$

Where:

N = number of particles emitted over the test cycle,

m_{edf} = total diluted exhaust gas flow over the cycle calculated according to any one of the methods described in clauses 8.5.1.2 to 8.5.1.4 of this Chapter, kg/test,

k = calibration factor to correct the particle number counter measurements to the level of the reference instrument where this is not applied internally within the particle number counter. Where the calibration factor is applied internally within the particle number counter, a value of 1 shall be used for k in the above equation,

\bar{c}_s = average corrected concentration of particles from the diluted exhaust gas corrected to standard conditions (273.2 K and 101.33 kPa), particles per cubic centimetre,

\bar{f}_r = mean particle concentration reduction factor of the volatile particle remover specific to the dilution settings used for the test.

\bar{c}_s = shall be calculated from the following equation:

$$\bar{c}_s = \frac{\sum_{i=1}^n c_{s,i}}{n} \quad (98)$$

Where:

$c_{s,i}$ = a discrete measurement of particle concentration in the diluted gas exhaust from the particle counter, corrected for coincidence and to standard conditions (273.2 K and 101.33 kPa), particles per cubic centimetre,

n = number of particle concentration measurements taken over the duration of the test.

10.4.4 **Test result**

10.4.4.1 **Calculation of the specific emissions**

For each individual WHSC, hot WHTC and cold WHTC the specific emissions in number of particles/kWh shall be calculated as follows:

$$e = \frac{N}{W_{act}} \quad (99)$$

Where:

e = is the number of particles emitted per kWh,

W_{act} = is the actual cycle work according to clause 7.8.6 of this Chapter, in kWh.

10.4.4.2 Exhaust after-treatment systems with periodic regeneration

For engines equipped with periodically regenerating after-treatment systems, the general provisions of clause 6.6.2 of this Chapter apply. The WHTC hot start emissions shall be weighted according to equation 5 where \bar{e} is the average number of particles/kWh without regeneration, and \bar{e}_r is the average number of particles/kWh with regeneration. The calculation of the regeneration adjustment factors shall be done according to equations 6, 6a, 7 or 8, as appropriate.

10.4.4.3 Weighted average WHTC test result

For the WHTC, the final test result shall be a weighted average from cold start and hot start (including periodic regeneration where relevant) tests calculated using one of the following equations:

- (a) In the case of multiplicative regeneration adjustment, or engines without periodically regenerating after-treatment

$$e = k_r \left(\frac{(0.14 \times N_{cold}) + (0.86 \times N_{ho})}{(0.14 \times W_{cold}) + (0.86 \times W_{hot})} \right) \quad (100)$$

- (b) In the case of additive regeneration adjustment hot

$$e = k_r + \left(\frac{(0.14 \times N_{cold}) + (0.86 \times N_{ho})}{(0.14 \times W_{act,cold}) + (0.86 \times W_{act,ho})} \right) \quad (101)$$

Where:

N_{cold} = is the total number of particles emitted over the WHTC cold test cycle,

N_{hot} = is the total number of particles emitted over the WHTC hot test cycle,

$W_{act,cold}$ = is the actual cycle work over the WHTC cold test cycle according to clause 7.8.6 of this Chapter, in kWh,

$W_{act,hot}$ = is the actual cycle work over the WHTC hot test cycle according to clause 7.8.6 of this Chapter, in kWh,

k_r = is the regeneration adjustment, according to clause 6.6.2 of this Chapter, or in the case of engines without periodically regenerating after-treatment $k_r = 1$

10.4.4.4 Rounding of final results

The final WHSC and weighted average WHTC test results shall be rounded in one step to three significant figures in accordance with ASTM E 29–06B. No rounding of intermediate values leading to the final brake specific emission result is permissible.

10.5 Determination of particle number background

10.5.1 At the engine manufacturer's request, dilution tunnel background particle number concentrations may be sampled, prior to or after the test, from a point downstream of the particle and hydrocarbon filters into the particle number measurement system, to determine the tunnel background particle concentrations.

10.5.2 Subtraction of particle number tunnel background concentrations shall not be allowed for type approval, but may be used at the manufacturer's request, with the prior approval of the Test Agency, for conformity of production testing, if it can be demonstrated that tunnel background contribution is significant, which can then be subtracted from the values measured in the diluted exhaust

CHAPTER 3-APPENDIX 1								
WHTC ENGINE DYNAMOMETER SCHEDULE								
Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %
1	0.0	0.0	39	21	0.0	77	57	14.1
2	0.0	0.0	40	19.1	0.0	78	58.1	7.0
3	0.0	0.0	41	13.7	0.0	79	43.3	0.0
4	0.0	0.0	42	2.2	0.0	80	28.5	25.0
5	0.0	0.0	43	0.0	0.0	81	30.4	47.8
6	0.0	0.0	44	0.0	0.0	82	32.1	39.2
7	1.5	8.9	45	0.0	0.0	83	32.7	39.3
8	15.8	30.9	46	0.0	0.0	84	32.4	17.3
9	27.4	1.3	47	0.0	0.0	85	31.6	11.4
10	32.6	0.7	48	0.0	0.0	86	31.1	10.2
11	34.8	1.2	49	0.0	0.0	87	31.1	19.5
12	36.2	7.4	50	0.0	13.1	88	31.4	22.5
13	37.1	6.2	51	13.1	30.1	89	31.6	22.9
14	37.9	10.2	52	26.3	25.5	90	31.6	24.3
15	39.6	12.3	53	35	32.2	91	31.9	26.9
16	42.3	12.5	54	41.7	14.3	92	32.4	30.6
17	45.3	12.6	55	42.2	0.00	93	32.8	32.7
18	48.6	6.0	56	42.8	11.6	94	33.7	32.5
19	40.8	0.00	57	51.00	20.9	95	34.4	29.5
20	33	16.3	58	60.00	9.6	96	34.3	26.5
21	42.5	27.4	59	49.4	0.00	97	34.4	24.7
22	49.3	26.7	60	38.9	16.6	98	35.00	24.9
23	54	18	61	43.4	30.8	99	35.6	25.2
24	57.1	12.9	62	49.4	14.2	100	36.1	24.8
25	58.9	8.6	63	40.5	0	101	36.3	24
26	59.3	6	64	31.5	43.5	102	36.2	23.6
27	59	4.9	65	36.6	78.2	103	36.2	23.5
28	57.9	m	66	40.8	67.6	104	36.8	22.7
29	55.7	m	67	44.7	59.1	105	37.2	20.9
30	52.1	m	68	48.3	52	106	37	19.2
31	46.4	m	69	51.9	63.8	107	36.3	18.4
32	38.6	m	70	54.7	27.9	108	35.4	17.6
33	29	m	71	55.3	18.3	109	35.2	14.9
34	20.8	m	72	55.1	16.3	110	35.4	9.9
35	16.9	m	73	54.8	11.1	111	35.5	4.3
36	16.9	42.5	74	54.7	11.5	112	35.2	6.6
37	18.8	38.4	75	54.8	17.5	113	34.9	10
38	20.7	32.9	76	55.6	18.0	114	34.7	25.1

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Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %
115	34.4	29.3	154	4.3	5.6	193	0	0
116	34.5	20.7	155	5.8	24.4	194	0	0
117	35.2	16.6	156	9.7	20.7	195	0	0
118	35.8	16.2	157	13.6	21.1	196	0	0
119	35.6	20.3	158	15.6	21.5	197	0	0
120	35.3	22.5	159	16.5	21.9	198	0	0
121	35.3	23.4	160	18	22.3	199	0	0
122	34.7	11.9	161	21.1	46.9	200	0	0
123	45.5	0	162	25.2	33.6	201	0	0
124	56.3	m	163	28.1	16.6	202	0	0
125	46.2	m	164	28.8	7	203	0	0
126	50.1	0	165	27.5	5	204	0	0
127	54	m	166	23.1	3	205	0	0
128	40.5	m	167	16.9	1.9	206	0	0
129	27	m	168	12.2	2.6	207	0	0
130	13.5	m	169	9.9	3.2	208	0	0
131	0	0	170	9.1	4	209	0	0
132	0	0	171	8.8	3.8	210	0	0
133	0	0	172	8.5	12.2	211	0	0
134	0	0	173	8.2	29.4	212	0	0
135	0	0	174	9.6	20.1	213	0	0
136	0	0	175	14.7	16.3	214	0	0
137	0	0	176	24.5	8.7	215	0	0
138	0	0	177	39.4	3.3	216	0	0
139	0	0	178	39	2.9	217	0	0
140	0	0	179	38.5	5.9	218	0	0
141	0	0	180	42.4	8	219	0	0
142	0	4.9	181	38.2	6	220	0	0
143	0	7.3	182	41.4	3.8	221	0	0
144	4.4	28.7	183	44.6	5.4	222	0	0
145	11.1	26.4	184	38.8	8.2	223	0	0
146	15	9.4	185	37.5	8.9	224	0	0
147	15.9	0	186	35.4	7.3	225	0	0
148	15.3	0	187	28.4	7	226	0	0
149	14.2	0	188	14.8	7	227	0	0
150	13.2	0	189	0	5.9	228	0	0
151	11.6	0	190	0	0	229	0	0
152	8.4	0	191	0	0	230	0	0
153	5.4	0	192	0	0	231	0	0

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Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %
232	0	0	271	46.8	m	310	0	0
233	0	0	272	41.7	m	311	0	0
234	0	0	273	35.9	m	312	0	0
235	0	0	274	29.2	m	313	0	0
236	0	0	275	20.7	m	314	0	0
237	0	0	276	10.1	m	315	0	0
238	0	0	277	0	m	316	0	0
239	0	0	278	0	0	317	0	0
240	0	0	279	0	0	318	0	0
241	0	0	280	0	0	319	0	0
242	0	0	281	0	0	320	0	0
243	0	0	282	0	0	321	0	0
244	0	0	283	0	0	322	0	0
245	0	0	284	0	0	323	0	0
246	0	0	285	0	0	324	4.5	41
247	0	0	286	0	0	325	17.2	38.9
248	0	0	287	0	0	326	30.1	36.8
249	0	0	288	0	0	327	41	34.7
250	0	0	289	0	0	328	50	32.6
251	0	0	290	0	0	329	51.4	0.1
252	0	0	291	0	0	330	47.8	m
253	0	31.6	292	0	0	331	40.2	m
254	9.4	13.6	293	0	0	332	32	m
255	22.2	16.9	294	0	0	333	24.4	m
256	33	53.5	295	0	0	334	16.8	m
257	43.7	22.1	296	0	0	335	8.1	m
258	39.8	0	297	0	0	336	0	m
259	36	45.7	298	0	0	337	0	0
260	47.6	75.9	299	0	0	338	0	0
261	61.2	70.4	300	0	0	339	0	0
262	72.3	70.4	301	0	0	340	0	0
263	76	m	302	0	0	341	0	0
264	74.3	m	303	0	0	342	0	0
265	68.5	m	304	0	0	343	0	0
266	61	m	305	0	0	344	0	0
267	56	m	306	0	0	345	0	0
268	54	m	307	0	0	346	0	0
269	53	m	308	0	0	347	0	0
270	50.8	m	309	0	0	348	0	0

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Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %
349	0	0	388	24.6	11	427	47.9	0
350	0	0	389	25.2	14.7	428	54.2	m
351	0	0	390	28.6	28.4	429	48.1	m
352	0	0	391	35.5	65	430	47	31.3
353	0	0	392	43.8	75.3	431	49	38.3
354	0	0.5	393	51.2	34.2	432	52	40.1
355	0	4.9	394	40.7	0	433	53.3	14.5
356	9.2	61.3	395	30.3	45.4	434	52.6	0.8
357	22.4	40.4	396	34.2	83.1	435	49.8	m
358	36.5	50.1	397	37.6	85.3	436	51	18.6
359	47.7	21	398	40.8	87.5	437	56.9	38.9
360	38.8	0	399	44.8	89.7	438	67.2	45
361	30	37	400	50.6	91.9	439	78.6	21.5
362	37	63.6	401	57.6	94.1	440	65.5	0
363	45.5	90.8	402	64.6	44.6	441	52.4	31.3
364	54.5	40.9	403	51.6	0	442	56.4	60.1
365	45.9	0	404	38.7	37.4	443	59.7	29.2
366	37.2	47.5	405	42.4	70.3	444	45.1	0
367	44.5	84.4	406	46.5	89.1	445	30.6	4.2
368	51.7	32.4	407	50.6	93.9	446	30.9	8.4
369	58.1	15.2	408	53.8	33	447	30.5	4.3
370	45.9	0	409	55.5	20.3	448	44.6	0
371	33.6	35.8	410	55.8	5.2	449	58.8	m
372	36.9	67	411	55.4	m	450	55.1	m
373	40.2	84.7	412	54.4	m	451	50.6	m
374	43.4	84.3	413	53.1	m	452	45.3	m
375	45.7	84.3	414	51.8	m	453	39.3	m
376	46.5	m	415	50.3	m	454	49.1	0
377	46.1	m	416	48.4	m	455	58.8	m
378	43.9	m	417	45.9	m	456	50.7	m
379	39.3	m	418	43.1	m	457	42.4	m
380	47	m	419	40.1	m	458	44.1	0
381	54.6	m	420	37.4	m	459	45.7	m
382	62	m	421	35.1	m	460	32.5	m
383	52	m	422	32.8	m	461	20.7	m
384	43	m	423	45.3	0	462	10	m
385	33.9	m	424	57.8	m	463	0	0
386	28.4	m	425	50.6	m	464	0	1.5
387	25.5	m	426	41.6	m	465	0.9	41.1

Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %
466	7	46.3	505	40.3	50.9	544	30.8	60.3
467	12.8	48.5	506	43	39.7	545	41.2	62.3
468	17	50.7	507	45.5	20.6	546	36	0
469	20.9	52.9	508	47.3	20.6	547	30.8	32.3
470	26.7	55	509	48.8	22.1	548	33.9	60.3
471	35.5	57.2	510	50.1	22.1	549	34.6	38.4
472	46.9	23.8	511	51.4	42.4	550	37	16.6
473	44.5	0	512	52.5	31.9	551	42.7	62.3
474	42.1	45.7	513	53.7	21.6	552	50.4	28.1
475	55.6	77.4	514	55.1	11.6	553	40.1	0
476	68.8	100	515	56.8	5.7	554	29.9	8
477	81.7	47.9	516	42.4	0	555	32.5	15
478	71.2	0	517	27.9	8.2	556	34.6	63.1
479	60.7	38.3	518	29	15.9	557	36.7	58
480	68.8	72.7	519	30.4	25.1	558	39.4	52.9
481	75	m	520	32.6	60.5	559	42.8	47.8
482	61.3	m	521	35.4	72.7	560	46.8	42.7
483	53.5	m	522	38.4	88.2	561	50.7	27.5
484	45.9	58	523	41	65.1	562	53.4	20.7
485	48.1	80	524	42.9	25.6	563	54.2	13.1
486	49.4	97.9	525	44.2	15.8	564	54.2	0.4
487	49.7	m	526	44.9	2.9	565	53.4	0
488	48.7	m	527	45.1	m	566	51.4	m
489	45.5	m	528	44.8	m	567	48.7	m
490	40.4	m	529	43.9	m	568	45.6	m
491	49.7	0	530	42.4	m	569	42.4	m
492	59	m	531	40.2	m	570	40.4	m
493	48.9	m	532	37.1	m	571	39.8	5.8
494	40	m	533	47	0	572	40.7	39.7
495	33.5	m	534	57	m	573	43.8	37.1
496	30	m	535	45.1	m	574	48.1	39.1
497	29.1	12	536	32.6	m	575	52	22
498	29.3	40.4	537	46.8	0	576	54.7	13.2
499	30.4	29.3	538	61.5	m	577	56.4	13.2
500	32.2	15.4	539	56.7	m	578	57.5	6.6
501	33.9	15.8	540	46.9	m	579	42.6	0
502	35.3	14.9	541	37.5	m	580	27.7	10.9
503	36.4	15.1	542	30.3	m	581	28.5	21.3
504	38	15.3	543	27.3	32.3	582	29.2	23.9

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Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %
583	29.5	15.2	622	33.8	38.4	661	42.3	46
584	29.7	8.8	623	42.1	m	662	57.1	74.1
585	30.4	20.8	624	34.1	m	663	72.1	34.2
586	31.9	22.9	625	33	37.1	664	66.9	0
587	34.3	61.4	626	36.4	38.4	665	60.4	41.8
588	37.2	76.6	627	43.3	17.1	666	69.1	79
589	40.1	27.5	628	35.7	0	667	77.1	38.3
590	42.3	25.4	629	28.1	11.6	668	63.1	0
591	43.5	32	630	36.5	19.2	669	49.1	47.9
592	43.8	6	631	45.2	8.3	670	53.4	91.3
593	43.5	m	632	36.5	0	671	57.5	85.7
594	42.8	m	633	27.9	32.6	672	61.5	89.2
595	41.7	m	634	31.5	59.6	673	65.5	85.9
596	40.4	m	635	34.4	65.2	674	69.5	89.5
597	39.3	m	636	37	59.6	675	73.1	75.5
598	38.9	12.9	637	39	49	676	76.2	73.6
599	39	18.4	638	40.2	m	677	79.1	75.6
600	39.7	39.2	639	39.8	m	678	81.8	78.2
601	41.4	60	640	36	m	679	84.1	39
602	43.7	54.5	641	29.7	m	680	69.6	0
603	46.2	64.2	642	21.5	m	681	55	25.2
604	48.8	73.3	643	14.1	m	682	55.8	49.9
605	51	82.3	644	0	0	683	56.7	46.4
606	52.1	0	645	0	0	684	57.6	76.3
607	52	m	646	0	0	685	58.4	92.7
608	50.9	m	647	0	0	686	59.3	99.9
609	49.4	m	648	0	0	687	60.1	95
610	47.8	m	649	0	0	688	61	46.7
611	46.6	m	650	0	0	689	46.6	0
612	47.3	35.3	651	0	0	690	32.3	34.6
613	49.2	74.1	652	0	0	691	32.7	68.6
614	51.1	95.2	653	0	0	692	32.6	67
615	51.7	m	654	0	0	693	31.3	m
616	50.8	m	655	0	0	694	28.1	m
617	47.3	m	656	0	3.4	695	43	0
618	41.8	m	657	1.4	22	696	58	m
619	36.4	m	658	10.1	45.3	697	58.9	m
620	30.9	m	659	21.5	10	698	49.4	m
621	25.5	37.1	660	32.2	0	699	41.5	m

AIS-137 (Part 4)

Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %
700	48.4	0	739	0	0	778	29.7	15.1
701	55.3	m	740	0	0	779	34.8	26.9
702	41.8	m	741	0	0	780	40	13.6
703	31.6	m	742	0	0	781	42.2	m
704	24.6	m	743	0	0	782	42.1	m
705	15.2	m	744	0	0	783	40.8	m
706	7	m	745	0	0	784	37.7	37.6
707	0	0	746	0	0	785	47	35
708	0	0	747	0	0	786	48.8	33.4
709	0	0	748	0	0	787	41.7	m
710	0	0	749	0	0	788	27.7	m
711	0	0	750	0	0	789	17.2	m
712	0	0	751	0	0	790	14	37.6
713	0	0	752	0	0	791	18.4	25
714	0	0	753	0	0	792	27.6	17.7
715	0	0	754	0	0	793	39.8	6.8
716	0	0	755	0	0	794	34.3	0
717	0	0	756	0	0	795	28.7	26.5
718	0	0	757	0	0	796	41.5	40.9
719	0	0	758	0	0	797	53.7	17.5
720	0	0	759	0	0	798	42.4	0
721	0	0	760	0	0	799	31.2	27.3
722	0	0	761	0	0	800	32.3	53.2
723	0	0	762	0	0	801	34.5	60.6
724	0	0	763	0	0	802	37.6	68
725	0	0	764	0	0	803	41.2	75.4
726	0	0	765	0	0	804	45.8	82.8
727	0	0	766	0	0	805	52.3	38.2
728	0	0	767	0	0	806	42.5	0
729	0	0	768	0	0	807	32.6	30.5
730	0	0	769	0	0	808	35	57.9
731	0	0	770	0	0	809	36	77.3
732	0	0	771	0	22	810	37.1	96.8
733	0	0	772	4.5	25.8	811	39.6	80.8
734	0	0	773	15.5	42.8	812	43.4	78.3
735	0	0	774	30.5	46.8	813	47.2	73.4
736	0	0	775	45.5	29.3	814	49.6	66.9
737	0	0	776	49.2	13.6	815	50.2	62
738	0	0	777	39.5	0	816	50.2	57.7

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Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %
817	50.6	62.1	856	42.5	74.8	895	0	0
818	52.3	62.9	857	46.6	74.2	896	0	0
819	54.8	37.5	858	50.7	76.2	897	0	0
820	57	18.3	859	54.8	75.1	898	0	0
821	42.3	0	860	58.7	36.3	899	0	0
822	27.6	29.1	861	45.2	0	900	0	0
823	28.4	57	862	31.8	37.2	901	0	5.8
824	29.1	51.8	863	33.8	71.2	902	2.5	27.9
825	29.6	35.3	864	35.5	46.4	903	12.4	29
826	29.7	33.3	865	36.6	33.6	904	19.4	30.1
827	29.8	17.7	866	37.2	20	905	29.3	31.2
828	29.5	m	867	37.2	m	906	37.1	10.4
829	28.9	m	868	37	m	907	40.6	4.9
830	43	0	869	36.6	m	908	35.8	0
831	57.1	m	870	36	m	909	30.9	7.6
832	57.7	m	871	35.4	m	910	35.4	13.8
833	56	m	872	34.7	m	911	36.5	11.1
834	53.8	m	873	34.1	m	912	40.8	48.5
835	51.2	m	874	33.6	m	913	49.8	3.7
836	48.1	m	875	33.3	m	914	41.2	0
837	44.5	m	876	33.1	m	915	32.7	29.7
838	40.9	m	877	32.7	m	916	39.4	52.1
839	38.1	m	878	31.4	m	917	48.8	22.7
840	37.2	42.7	879	45	0	918	41.6	0
841	37.5	70.8	880	58.5	m	919	34.5	46.6
842	39.1	48.6	881	53.7	m	920	39.7	84.4
843	41.3	0.1	882	47.5	m	921	44.7	83.2
844	42.3	m	883	40.6	m	922	49.5	78.9
845	42	m	884	34.1	m	923	52.3	83.8
846	40.8	m	885	45.3	0	924	53.4	77.7
847	38.6	m	886	56.4	m	925	52.1	69.6
848	35.5	m	887	51	m	926	47.9	63.6
849	32.1	m	888	44.5	m	927	46.4	55.2
850	29.6	m	889	36.4	m	928	46.5	53.6
851	28.8	39.9	890	26.6	m	929	46.4	62.3
852	29.2	52.9	891	20	m	930	46.1	58.2
853	30.9	76.1	892	13.3	m	931	46.2	61.8
854	34.3	76.5	893	6.7	m	932	47.3	62.3
855	38.3	75.5	894	0	0	933	49.3	57.1

Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %
934	52.6	58.1	973	39.9	41.8	1012	17.9	m
935	56.3	56	974	40.3	38.2	1013	16.2	1.9
936	59.9	27.2	975	40.8	35	1014	17.8	7.5
937	45.8	0	976	41.9	32.4	1015	25.2	18
938	31.8	28.8	977	43.2	26.4	1016	39.7	6.5
939	32.7	56.5	978	43.5	m	1017	38.6	0
940	33.4	62.8	979	42.9	m	1018	37.4	5.4
941	34.6	68.2	980	41.5	m	1019	43.4	9.7
942	35.8	68.6	981	40.9	m	1020	46.9	15.7
943	38.6	65	982	40.5	m	1021	52.5	13.1
944	42.3	61.9	983	39.5	m	1022	56.2	6.3
945	44.1	65.3	984	38.3	m	1023	44	0
946	45.3	63.2	985	36.9	m	1024	31.8	20.9
947	46.5	30.6	986	35.4	m	1025	38.7	36.3
948	46.7	11.1	987	34.5	m	1026	47.7	47.5
949	45.9	16.1	988	33.9	m	1027	54.5	22
950	45.6	21.8	989	32.6	m	1028	41.3	0
951	45.9	24.2	990	30.9	m	1029	28.1	26.8
952	46.5	24.7	991	29.9	m	1030	31.6	49.2
953	46.7	24.7	992	29.2	m	1031	34.5	39.5
954	46.8	28.2	993	44.1	0	1032	36.4	24
955	47.2	31.2	994	59.1	m	1033	36.7	m
956	47.6	29.6	995	56.8	m	1034	35.5	m
957	48.2	31.2	996	53.5	m	1035	33.8	m
958	48.6	33.5	997	47.8	m	1036	33.7	19.8
959	48.8	m	998	41.9	m	1037	35.3	35.1
960	47.6	m	999	35.9	m	1038	38	33.9
961	46.3	m	1000	44.3	0	1039	40.1	34.5
962	45.2	m	1001	52.6	m	1040	42.2	40.4
963	43.5	m	1002	43.4	m	1041	45.2	44
964	41.4	m	1003	50.6	0	1042	48.3	35.9
965	40.3	m	1004	57.8	m	1043	50.1	29.6
966	39.4	m	1005	51.6	m	1044	52.3	38.5
967	38	m	1006	44.8	m	1045	55.3	57.7
968	36.3	m	1007	48.6	0	1046	57	50.7
969	35.3	5.8	1008	52.4	m	1047	57.7	25.2
970	35.4	30.2	1009	45.4	m	1048	42.9	0
971	36.6	55.6	1010	37.2	m	1049	28.2	15.7
972	38.6	48.5	1011	26.3	m	1050	29.2	30.5

Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %
1051	31.1	52.6	1090	47.8	20.6	1129	31.7	33.9
1052	33.4	60.7	1091	47.2	3.8	1130	32	29.9
1053	35	61.4	1092	45.6	4.4	1131	32.1	m
1054	35.3	18.2	1093	44.6	4.1	1132	31.4	m
1055	35.2	14.9	1094	44.1	m	1133	30.3	m
1056	34.9	11.7	1095	42.9	m	1134	29.8	m
1057	34.5	12.9	1096	40.9	m	1135	44.3	0
1058	34.1	15.5	1097	39.2	m	1136	58.9	m
1059	33.5	m	1098	37	m	1137	52.1	m
1060	31.8	m	1099	35.1	2	1138	44.1	m
1061	30.1	m	1100	35.6	43.3	1139	51.7	0
1062	29.6	10.3	1101	38.7	47.6	1140	59.2	m
1063	30	26.5	1102	41.3	40.4	1141	47.2	m
1064	31	18.8	1103	42.6	45.7	1142	35.1	0
1065	31.5	26.5	1104	43.9	43.3	1143	23.1	m
1066	31.7	m	1105	46.9	41.2	1144	13.1	m
1067	31.5	m	1106	52.4	40.1	1145	5	m
1068	30.6	m	1107	56.3	39.3	1146	0	0
1069	30	m	1108	57.4	25.5	1147	0	0
1070	30	m	1109	57.2	25.4	1148	0	0
1071	29.4	m	1110	57	25.4	1149	0	0
1072	44.3	0	1111	56.8	25.3	1150	0	0
1073	59.2	m	1112	56.3	25.3	1151	0	0
1074	58.3	m	1113	55.6	25.2	1152	0	0
1075	57.1	m	1114	56.2	25.2	1153	0	0
1076	55.4	m	1115	58	12.4	1154	0	0
1077	53.5	m	1116	43.4	0	1155	0	0
1078	51.5	m	1117	28.8	26.2	1156	0	0
1079	49.7	m	1118	30.9	49.9	1157	0	0
1080	47.9	m	1119	32.3	40.5	1158	0	0
1081	46.4	m	1120	32.5	12.4	1159	0	0
1082	45.5	m	1121	32.4	12.2	1160	0	0
1083	45.2	m	1122	32.1	6.4	1161	0	0
1084	44.3	m	1123	31	12.4	1162	0	0
1085	43.6	m	1124	30.1	18.5	1163	0	0
1086	43.1	m	1125	30.4	35.6	1164	0	0
1087	42.5	25.6	1126	31.2	30.1	1165	0	0
1088	43.3	25.7	1127	31.5	30.8	1166	0	0
1089	46.3	24	1128	31.5	26.9	1167	0	0

Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %
1168	0	0	1207	54.9	9.9	1246	68.1	43.5
1169	0	0	1208	44.9	0	1247	55.2	0
1170	0	0	1209	34.9	47.4	1248	42.3	37.2
1171	0	0	1210	42.7	82.7	1249	43	73.6
1172	0	0	1211	52	81.2	1250	43.5	65.1
1173	0	0	1212	61.8	82.7	1251	43.8	53.1
1174	0	0	1213	71.3	39.1	1252	43.9	54.6
1175	0	0	1214	58.1	0	1253	43.9	41.2
1176	0	0	1215	44.9	42.5	1254	43.8	34.8
1177	0	0	1216	46.3	83.3	1255	43.6	30.3
1178	0	0	1217	46.8	74.1	1256	43.3	21.9
1179	0	0	1218	48.1	75.7	1257	42.8	19.9
1180	0	0	1219	50.5	75.8	1258	42.3	m
1181	0	0	1220	53.6	76.7	1259	41.4	m
1182	0	0	1221	56.9	77.1	1260	40.2	m
1183	0	0	1222	60.2	78.7	1261	38.7	m
1184	0	0	1223	63.7	78	1262	37.1	m
1185	0	0	1224	67.2	79.6	1263	35.6	m
1186	0	0	1225	70.7	80.9	1264	34.2	m
1187	0	0	1226	74.1	81.1	1265	32.9	m
1188	0	0	1227	77.5	83.6	1266	31.8	m
1189	0	0	1228	80.8	85.6	1267	30.7	m
1190	0	0	1229	84.1	81.6	1268	29.6	m
1191	0	0	1230	87.4	88.3	1269	40.4	0
1192	0	0	1231	90.5	91.9	1270	51.2	m
1193	0	0	1232	93.5	94.1	1271	49.6	m
1194	0	0	1233	96.8	96.6	1272	48	m
1195	0	0	1234	100	m	1273	46.4	m
1196	0	20.4	1235	96	m	1274	45	m
1197	12.6	41.2	1236	81.9	m	1275	43.6	m
1198	27.3	20.4	1237	68.1	m	1276	42.3	m
1199	40.4	7.6	1238	58.1	84.7	1277	41	m
1200	46.1	m	1239	58.5	85.4	1278	39.6	m
1201	44.6	m	1240	59.5	85.6	1279	38.3	m
1202	42.7	14.7	1241	61	86.6	1280	37.1	m
1203	42.9	7.3	1242	62.6	86.8	1281	35.9	m
1204	36.1	0	1243	64.1	87.6	1282	34.6	m
1205	29.3	15	1244	65.4	87.5	1283	33	m
1206	43.8	22.6	1245	66.7	87.8	1284	31.1	m

AIS-137 (Part 4)

Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %
1285	29.2	m	1324	40.3	0	1363	35.1	m
1286	43.3	0	1325	39.3	1	1364	33.7	m
1287	57.4	32.8	1326	38.3	15.2	1365	32.4	m
1288	59.9	65.4	1327	37.6	57.8	1366	31.1	m
1289	61.9	76.1	1328	37.3	73.2	1367	29.9	m
1290	65.6	73.7	1329	37.3	59.8	1368	28.7	m
1291	69.9	79.3	1330	37.4	52.2	1369	29	58.6
1292	74.1	81.3	1331	37.4	16.9	1370	29.7	88.5
1293	78.3	83.2	1332	37.1	34.3	1371	31	86.3
1294	82.6	86	1333	36.7	51.9	1372	31.8	43.4
1295	87	89.5	1334	36.2	25.3	1373	31.7	m
1296	91.2	90.8	1335	35.6	m	1374	29.9	m
1297	95.3	45.9	1336	34.6	m	1375	40.2	0
1298	81	0	1337	33.2	m	1376	50.4	m
1299	66.6	38.2	1338	31.6	m	1377	47.9	m
1300	67.9	75.5	1339	30.1	m	1378	45	m
1301	68.4	80.5	1340	28.8	m	1379	43	m
1302	69	85.5	1341	28	29.5	1380	40.6	m
1303	70	85.2	1342	28.6	100	1381	55.5	0
1304	71.6	85.9	1343	28.8	97.3	1382	70.4	41.7
1305	73.3	86.2	1344	28.8	73.4	1383	73.4	83.2
1306	74.8	86.5	1345	29.6	56.9	1384	74	83.7
1307	76.3	42.9	1346	30.3	91.7	1385	74.9	41.7
1308	63.3	0	1347	31	90.5	1386	60	0
1309	50.4	21.2	1348	31.8	81.7	1387	45.1	41.6
1310	50.6	42.3	1349	32.6	79.5	1388	47.7	84.2
1311	50.6	53.7	1350	33.5	86.9	1389	50.4	50.2
1312	50.4	90.1	1351	34.6	100	1390	53	26.1
1313	50.5	97.1	1352	35.6	78.7	1391	59.5	0
1314	51	100	1353	36.4	50.5	1392	66.2	38.4
1315	51.9	100	1354	37	57	1393	66.4	76.7
1316	52.6	100	1355	37.3	69.1	1394	67.6	100
1317	52.8	32.4	1356	37.6	49.5	1395	68.4	76.6
1318	47.7	0	1357	37.8	44.4	1396	68.2	47.2
1319	42.6	27.4	1358	37.8	43.4	1397	69	81.4
1320	42.1	53.5	1359	37.8	34.8	1398	69.7	40.6
1321	41.8	44.5	1360	37.6	24	1399	54.7	0
1322	41.4	41.1	1361	37.2	m	1400	39.8	19.9
1323	41	21	1362	36.3	m	1401	36.3	40

Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %
1402	36.7	59.4	1441	39.2	100	1480	56.1	94.9
1403	36.6	77.5	1442	40.9	100	1481	56.3	86.2
1404	36.8	94.3	1443	42.4	99.5	1482	56.2	64.1
1405	36.8	100	1444	43.8	98.7	1483	56	46.1
1406	36.4	100	1445	45.4	97.3	1484	56.2	33.4
1407	36.3	79.7	1446	47	96.6	1485	56.5	23.6
1408	36.7	49.5	1447	47.8	96.2	1486	56.3	18.6
1409	36.6	39.3	1448	48.8	96.3	1487	55.7	16.2
1410	37.3	62.8	1449	50.5	95.1	1488	56	15.9
1411	38.1	73.4	1450	51	95.9	1489	55.9	21.8
1412	39	72.9	1451	52	94.3	1490	55.8	20.9
1413	40.2	72	1452	52.6	94.6	1491	55.4	18.4
1414	41.5	71.2	1453	53	65.5	1492	55.7	25.1
1415	42.9	77.3	1454	53.2	0	1493	56	27.7
1416	44.4	76.6	1455	53.2	m	1494	55.8	22.4
1417	45.4	43.1	1456	52.6	m	1495	56.1	20
1418	45.3	53.9	1457	52.1	m	1496	55.7	17.4
1419	45.1	64.8	1458	51.8	m	1497	55.9	20.9
1420	46.5	74.2	1459	51.3	m	1498	56	22.9
1421	47.7	75.2	1460	50.7	m	1499	56	21.1
1422	48.1	75.5	1461	50.7	m	1500	55.1	19.2
1423	48.6	75.8	1462	49.8	m	1501	55.6	24.2
1424	48.9	76.3	1463	49.4	m	1502	55.4	25.6
1425	49.9	75.5	1464	49.3	m	1503	55.7	24.7
1426	50.4	75.2	1465	49.1	m	1504	55.9	24
1427	51.1	74.6	1466	49.1	m	1505	55.4	23.5
1428	51.9	75	1467	49.1	8.3	1506	55.7	30.9
1429	52.7	37.2	1468	48.9	16.8	1507	55.4	42.5
1430	41.6	0	1469	48.8	21.3	1508	55.3	25.8
1431	30.4	36.6	1470	49.1	22.1	1509	55.4	1.3
1432	30.5	73.2	1471	49.4	26.3	1510	55	m
1433	30.3	81.6	1472	49.8	39.2	1511	54.4	m
1434	30.4	89.3	1473	50.4	83.4	1512	54.2	m
1435	31.5	90.4	1474	51.4	90.6	1513	53.5	m
1436	32.7	88.5	1475	52.3	93.8	1514	52.4	m
1437	33.7	97.2	1476	53.3	94	1515	51.8	m
1438	35.2	99.7	1477	54.2	94.1	1516	50.7	m
1439	36.3	98.8	1478	54.9	94.3	1517	49.9	m
1440	37.7	100	1479	55.7	94.6	1518	49.1	m

AIS-137 (Part 4)

Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %
1519	47.7	m	1559	56.6	38.2	1598	56.9	41.8
1520	47.3	m	1560	56.2	37.9	1599	56.6	41.9
1521	46.9	m	1561	56.6	37.5	1600	56.7	42.6
1522	46.9	m	1562	56.4	36.7	1601	56.7	42.6
1523	47.2	m	1563	56.5	34.8	1602	56.7	41.5
1524	47.8	m	1564	56.5	35.8	1603	56.7	42.2
1525	48.2	0	1565	56.5	36.2	1604	56.5	42.2
1526	48.8	23	1566	56.5	36.7	1605	56.8	41.9
1527	49.1	67.9	1567	56.7	37.8	1606	56.5	42
1528	49.4	73.7	1568	56.7	37.8	1607	56.7	42.1
1529	49.8	75	1569	56.6	36.6	1608	56.4	41.9
1530	50.4	75.8	1570	56.8	36.1	1609	56.7	42.9
1531	51.4	73.9	1571	56.5	36.8	1610	56.7	41.8
1532	52.3	72.2	1572	56.9	35.9	1611	56.7	41.9
1533	53.3	71.2	1573	56.7	35	1612	56.8	42
1534	54.6	71.2	1574	56.5	36	1613	56.7	41.5
1535	55.4	68.7	1575	56.4	36.5	1614	56.6	41.9
1536	56.7	67	1576	56.5	38	1615	56.8	41.6
1537	57.2	64.6	1577	56.5	39.9	1616	56.6	41.6
1538	57.3	61.9	1578	56.4	42.1	1617	56.9	42
1539	57	59.5	1579	56.5	47	1618	56.7	40.7
1540	56.7	57	1580	56.4	48	1619	56.7	39.3
1541	56.7	69.8	1581	56.1	49.1	1620	56.5	41.4
1542	56.8	58.5	1582	56.4	48.9	1621	56.4	44.9
1543	56.8	47.2	1583	56.4	48.2	1622	56.8	45.2
1544	57	38.5	1584	56.5	48.3	1623	56.6	43.6
1545	57	32.8	1585	56.5	47.9	1624	56.8	42.2
1546	56.8	30.2	1586	56.6	46.8	1625	56.5	42.3
1547	57	27	1587	56.6	46.2	1626	56.5	44.4
1548	56.9	26.2	1588	56.5	44.4	1627	56.9	45.1
1549	56.7	26.2	1589	56.8	42.9	1628	56.4	45
1550	57	26.6	1590	56.5	42.8	1629	56.7	46.3
1551	56.7	27.8	1591	56.7	43.2	1630	56.7	45.5
1552	56.7	29.7	1592	56.5	42.8	1631	56.8	45
1553	56.8	32.1	1593	56.9	42.2	1632	56.7	44.9
1554	56.5	34.9	1594	56.5	43.1	1633	56.6	45.2
1555	56.6	34.9	1595	56.5	42.9	1634	56.8	46
1556	56.3	35.8	1596	56.7	42.7	1635	56.5	46.6
1557	56.6	36.6	1597	56.6	41.5	1636	56.6	48.3
1558	56.2	37.6						

AIS-137 (Part 4)

Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %	Time (s)	Normal speed %	Normal torque %
1637	56.4	48.6	1676	56.9	60.9	1715	56.6	6.5
1638	56.6	50.3	1677	57.1	57.4	1716	56.5	10
1639	56.3	51.9	1678	57.1	54.3	1717	56.6	12.4
1640	56.5	54.1	1679	57	48.6	1718	56.5	14.5
1641	56.3	54.9	1680	57.4	44.1	1719	56.6	16.3
1642	56.4	55	1681	57.4	40.2	1720	56.3	18.1
1643	56.4	56.2	1682	57.6	36.9	1721	56.6	20.7
1644	56.2	58.6	1683	57.5	34.2	1722	56.1	22.6
1645	56.2	59.1	1684	57.4	31.1	1723	56.3	25.8
1646	56.2	62.5	1685	57.5	25.9	1724	56.4	27.7
1647	56.4	62.8	1686	57.5	20.7	1725	56	29.7
1648	56	64.7	1687	57.6	16.4	1726	56.1	32.6
1649	56.4	65.6	1688	57.6	12.4	1727	55.9	34.9
1650	56.2	67.7	1689	57.6	8.9	1728	55.9	36.4
1651	55.9	68.9	1690	57.5	8	1729	56	39.2
1652	56.1	68.9	1691	57.5	5.8	1730	55.9	41.4
1653	55.8	69.5	1692	57.3	5.8	1731	55.5	44.2
1654	56	69.8	1693	57.6	5.5	1732	55.9	46.4
1655	56.2	69.3	1694	57.3	4.5	1733	55.8	48.3
1656	56.2	69.8	1695	57.2	3.2	1734	55.6	49.1
1657	56.4	69.2	1696	57.2	3.1	1735	55.8	49.3
1658	56.3	68.7	1697	57.3	4.9	1736	55.9	47.7
1659	56.2	69.4	1698	57.3	4.2	1737	55.9	47.4
1660	56.2	69.5	1699	56.9	5.5	1738	55.8	46.9
1661	56.2	70	1700	57.1	5.1	1739	56.1	46.8
1662	56.4	69.7	1701	57	5.2	1740	56.1	45.8
1663	56.2	70.2	1702	56.9	5.5	1741	56.2	46
1664	56.4	70.5	1703	56.6	5.4	1742	56.3	45.9
1665	56.1	70.5	1704	57.1	6.1	1743	56.3	45.9
1666	56.5	69.7	1705	56.7	5.7	1744	56.2	44.6
1667	56.2	69.3	1706	56.8	5.8	1745	56.2	46
1668	56.5	70.9	1707	57	6.1	1746	56.4	46.2
1669	56.4	70.8	1708	56.7	5.9	1747	55.8	m
1670	56.3	71.1	1709	57	6.6	1748	55.5	m
1671	56.4	71	1710	56.9	6.4	1749	55	m
1672	56.7	68.6	1711	56.7	6.7	1750	54.1	m
1673	56.8	68.6	1712	56.9	6.9	1751	54	m
1674	56.6	68	1713	56.8	5.6	1752	53.3	m
1675	56.8	65.1	1714	56.6	5.1	1753	52.6	m

AIS-137 (Part 4)

Time (s)	Normal speed %	Normal torque %		Time (s)	Normal speed %	Normal torque %		Time (s)	Normal speed %	Normal torque %
1754	51.8	m		1770	49.1	m		1786	31.6	m
1755	50.7	m		1771	46.2	m		1787	25.8	m
1756	49.9	m		1772	43.1	m		1788	19.9	m
1757	49.1	m		1773	39.9	m		1789	14	m
1758	47.7	m		1774	36.6	m		1790	8.1	m
1759	46.8	m		1775	33.6	m		1791	2.2	m
1760	45.7	m		1776	30.5	m		1792	0	0
1761	44.8	m		1777	42.8	0		1793	0	0
1762	43.9	m		1778	55.2	m		1794	0	0
1763	42.9	m		1779	49.9	m		1795	0	0
1764	41.5	m		1780	44	m		1796	0	0
1765	39.5	m		1781	37.6	m		1797	0	0
1766	36.7	m		1782	47.2	0		1798	0	0
1767	33.8	m		1783	56.8	m		1799	0	0
1768	31	m		1784	47.5	m		1800	0	0
1769	40	0		1785	42.9	m		M= motoring		

CHAPTER 3 - APPENDIX 2

MEASUREMENT EQUIPMENT

A2.1 This Appendix contains the basic requirements and the general descriptions of the sampling and analyzing systems for gaseous and particulate emissions measurement. Since various configurations can produce equivalent results, exact conformance with the figures of this Appendix is not required. Components such as instruments, valves, solenoids, pumps, flow devices and switches may be used to provide additional information and coordinate the functions of the component systems. Other components which are not needed to maintain the accuracy on some systems may be excluded if their exclusion is based upon good engineering judgment.

A 2.1.1 Analytical System

A2.1.2 Description of the analytical system

Analytical system for the determination of the gaseous emissions in the raw exhaust gas (Figure 1 of this Appendix) or in the diluted exhaust gas (Figure 2 of this Appendix) are described based on the use of:

- (a) HFID or FID analyzer for the measurement of hydrocarbons;
- (b) NDIR analyzers for the measurement of carbon monoxide and carbon dioxide;
- (c) HCLD or CLD analyzer for the measurement of the oxides of nitrogen.

The sample for all components should be taken with one sampling probe and internally split to the different analyzers. Optionally, two sampling probes located in close proximity may be used. Care shall be taken that no unintended condensation of exhaust components (including water and sulphuric acid) occurs at any point of the analytical system.

A2.1.3

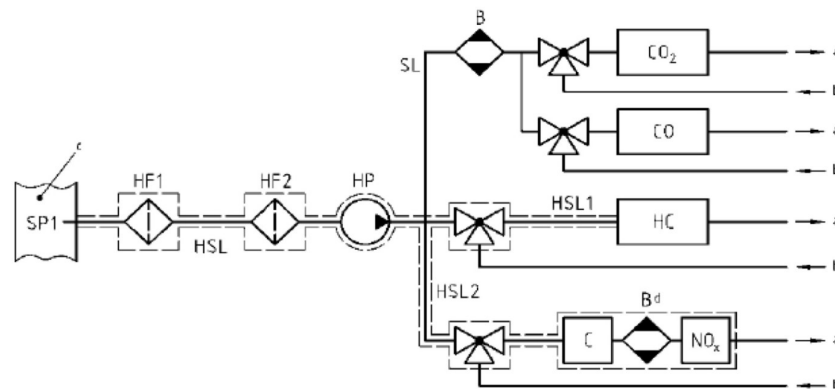


Figure 1

**Schematic Flow Diagram of Raw Exhaust Gas Analysis System for
CO, CO₂, NO_x, HC**

a = vent b = zero, span gas c = exhaust pipe d = optional

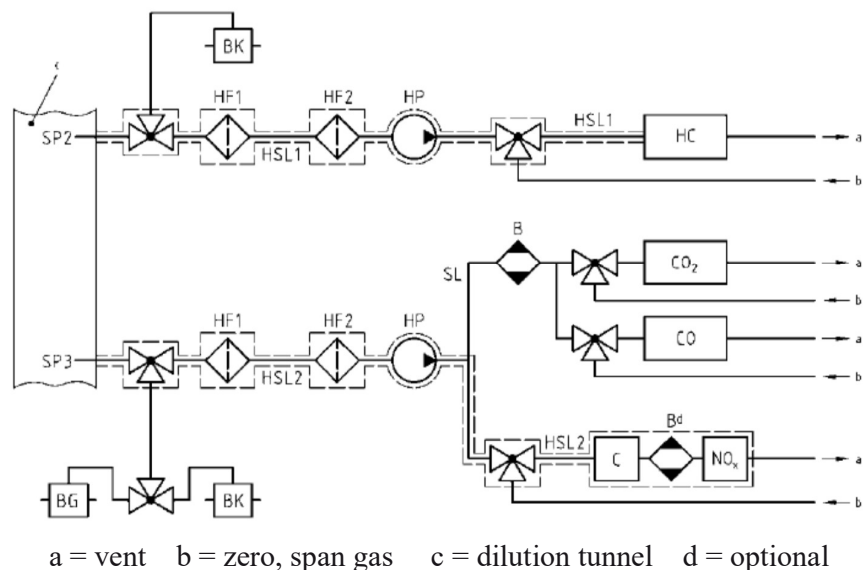


Figure 2
Schematic Flow Diagram Of Diluted Exhaust Gas Analysis System
for CO, CO₂ , NO_x , HC

A2.1.3 Components of Figures 1 and 2 of this Appendix.

EP Exhaust pipe

SP Raw exhaust gas sampling probe (Figure 1 of this Appendix only)

A stainless steel straight closed end multi-hole probe is recommended. The inside diameter shall not be greater than the inside diameter of the sampling line. The wall thickness of the probe shall not be greater than 1 mm. There shall be a minimum of three holes in three different radial planes sized to sample approximately the same flow. The probe shall extend across at least 80 per cent of the diameter of the exhaust pipe. One or two sampling probes may be used.

SP2 Dilute Exhaust Gas HC Sampling Probe (Figure 2 of this Appendix only)

The probe shall:

- (a) Be defined as the first 254 mm to 762 mm of the heated sampling line HSL1;
- (b) Have a 5 mm minimum inside diameter;
- (c) Be installed in the dilution tunnel DT (Figure 7) at a point where the diluent and exhaust gas are well mixed (i.e. approximately 10 tunnel diameters downstream of the point where the exhaust enters the dilution tunnel);
- (d) Be sufficiently distant (radially) from other probes and the tunnel wall so as to be free from the influence of any wakes or eddies;
- (e) Be heated so as to increase the gas stream temperature to $463\text{ K} \pm 10\text{ K}$ ($190\text{ }^{\circ}\text{C} \pm 10\text{ }^{\circ}\text{C}$) at the exit of the probe, or to $385\text{ K} \pm 10\text{ K}$ ($112\text{ }^{\circ}\text{C} \pm 10\text{ }^{\circ}\text{C}$) for positive ignition engines;
- (f) Non-heated in case of FID measurement (cold).

SP3 Dilute exhaust gas CO, CO₂, NO_x sampling probe (Figure 2 of this Appendix only)

The probe shall:

- (a) Be in the same plane as SP2;
- (b) Be sufficiently distant (radially) from other probes and the tunnel wall so as to be free from the influence of any wakes or eddies;
- (c) Be heated and insulated over its entire length to a minimum temperature of 328 K (55 °C) to prevent water condensation.

HF1 Heated pre filter (optional)

The temperature shall be the same as HSL1.

HF2 Heated Filter

The filter shall extract any solid particles from the gas sample prior to the analyzer. The temperature shall be the same as HSL1. The filter shall be changed as needed.

HSL1 Heated Sampling Line

The sampling line provides a gas sample from a single probe to the split point(s) and the HC analyzer.

The sampling line shall:

- (a) Have a 4 mm minimum and a 13.5 mm maximum inside diameter;
- (b) Be made of stainless steel or PTFE;
- (c) Maintain a wall temperature of 463 K \pm 10 K (190 °C \pm 10 °C) as measured at every separately controlled heated section, if the temperature of the exhaust gas at the sampling probe equal to or below 463 K (190 °C);
- (d) Maintain a wall temperature greater than 453 K (180 °C), if the temperature of the exhaust gas at the sampling probe is above 463 K (190 °C);
- (e) Maintain a gas temperature of 463 K \pm 10 K (190 °C \pm 10 °C) immediately before the heated filter HF2 and the HFID.

HSL2 Heated NO_x Sampling Line

The sampling line shall:

- (a) Maintain a wall temperature of 328 K to 473 K (55 °C to 200 °C), up to the converter for dry measurement, and up to the analyzer for wet measurement;
- (b) Be made of stainless steel or PTFE.

HP Heated Sampling Pump

The pump shall be heated to the temperature of HSL.

SL Sampling Line for CO and CO₂

The line shall be made of PTFE or stainless steel. It may be heated or unheated.

HC HFID Analyser

Heated flame ionization detector (HFID) or flame ionization detector (FID) for the determination of the hydrocarbons. The temperature of the HFID shall be kept at 453 K to 473 K (180 °C to 200 °C).

CO, CO₂ NDIR analyzer

NDIR analyzers for the determination of carbon monoxide and carbon dioxide (optional for the determination of the dilution ratio for PT measurement).

NO_x CLD analyzer or NDUV analyzer

CLD, HCLD or NDUV analyzer for the determination of the oxides of nitrogen. If a HCLD is used it shall be kept at a temperature of 328 K to 473 K (55 °C to 200 °C).

B Sample dryer (optional for NO measurement)

To cool and condense water from the exhaust sample. It is optional if the analyzer is free from water vapour interference as determined in clause 9.3.9.2.2 of this Chapter. If water is removed by condensation, the sample gas temperature or dew point shall be monitored either within the water trap or downstream. The sample gas temperature or dew point shall not exceed 280 K (7 °C). Chemical dryers are not allowed for removing water from the sample.

BK Background Bag (Optional : Figure 2 of this Appendix only)

For the measurement of the background concentrations.

BG Sample Bag (Optional : Figure 2 of this Appendix only)

For the measurement of the sample concentrations.

A2.1.4 Non-Methane Cutter Method (NMC)

The cutter oxidizes all hydrocarbons except CH₄ to CO₂ and H₂O, so that by passing the sample through the NMC only CH₄ is detected by the HFID. In addition to the usual HC sampling train (see Figures 1 and 2 of this Appendix), a second HC sampling train shall be installed equipped with a cutter as laid out in Figure 3 of this Appendix. This allows simultaneous measurement of total HC, CH₄ and NMHC.

The cutter shall be characterized at or above 600 K (327 °C) prior to test work with respect to its catalytic effect on CH₄ and C₂H₆ at H₂O values representative of exhaust stream conditions. The dew point and O₂ level of the sampled exhaust stream shall be known. The relative response of the FID to CH₄ and C₂H₆ shall be determined in accordance with clause 9.3.8 of this Chapter.

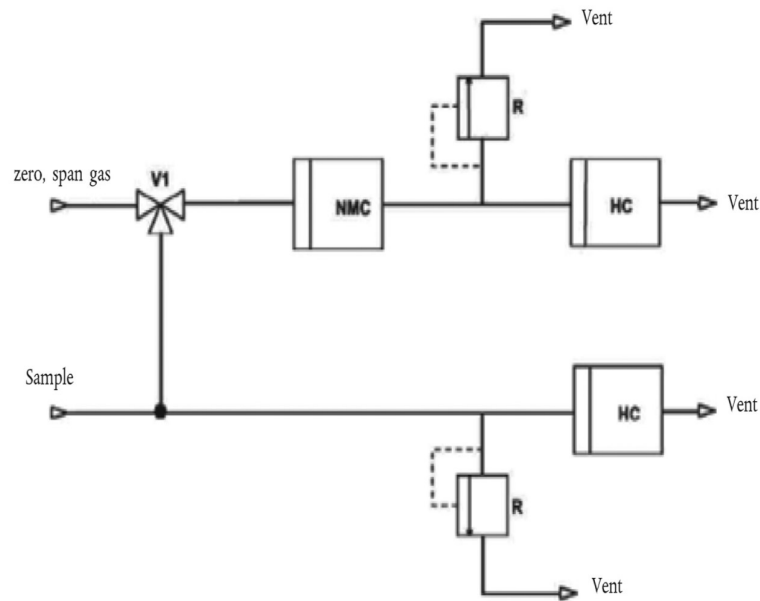


Figure 3

Schematic Flow Diagram of Methane Analysis with the NMC

A2.1.5 Components of Figure 3 above

NMC Non methane Cutter

To oxidize all hydrocarbons except methane.

HC

Heated flame ionization detector or flame ionization detector (FID) to measure the HC and CH₄ concentrations. The temperature of the HFID shall be kept at 453 K to 473 K (180 °C to 200 °C).

V1 selector valve

To select zero and spam gas

R Pressure Regulator

To control the pressure in the sampling line and the flow to the HFID

A2.2 Dilution and Particulate Sampling System

A2.2.1 Description of partial flow system

A dilution system is described based upon the dilution of a part of the exhaust stream. Splitting of the exhaust stream and the following dilution process may be done by different dilution system types. For subsequent collection of the particulates, the entire dilute exhaust gas or only a portion of the dilute exhaust gas is passed to the particulate sampling system. The first method is referred to as total sampling type, the second method as fractional sampling type. The calculation of the dilution ratio depends upon the type of system used.

With the total sampling system as shown in Figure 4 of this Appendix, raw exhaust gas is transferred from the exhaust pipe (EP) to the dilution tunnel (DT) through the sampling probe (SP) and the transfer tube (TT). The total flow through the tunnel is adjusted with the flow controller FC2 and the sampling pump (P) of the particulate sampling system (see Figure 8 of this Appendix). The diluent flow is controlled by the flow controller FC1, which may use q_{mew} or q_{maw} and q_{mf} as command signals, for the desired exhaust split. The sample flow into DT is the difference of the total flow and the diluent flow. The diluent flow rate is measured with the flow measurement device FM1, the total flow rate with the flow measurement device FM3 of the particulate sampling system (see Figure 8 of this Appendix). The dilution ratio is calculated from these two flow rates.

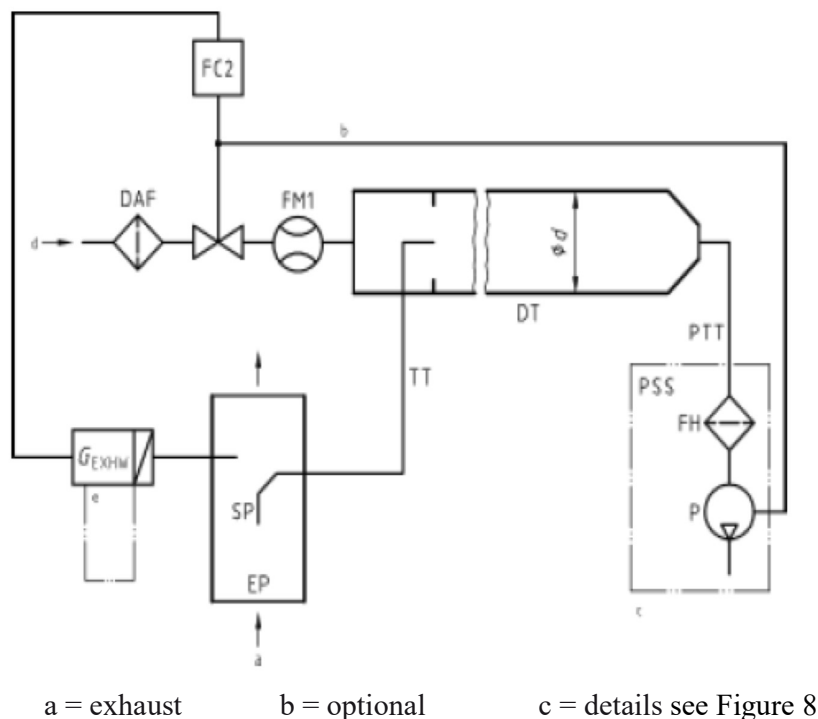


Figure 4
Scheme of Partial Flow Dilution System (Total Sampling Type)

With the fractional sampling system as shown in Figure 5 of this Appendix, raw exhaust gas is transferred from the exhaust pipe EP to the dilution tunnel DT through the sampling probe SP and the transfer tube TT. The total flow through the tunnel is adjusted with the flow controller FC1 connected either to the diluent flow or to the suction blower for the total tunnel flow. The flow controller FC1 may use q_{mew} or q_{maw} and q_{mf} as command signals for the desired exhaust split. The sample flow into DT is the difference of the total flow and the diluent flow. The diluent flow rate is measured with the flow measurement device FM1, the total flow rate with the flow measurement device FM2. The dilution ratio is calculated from these two flow rates. From DT, a particulate sample is taken with the particulate sampling system (see Figure 8 of this Appendix).

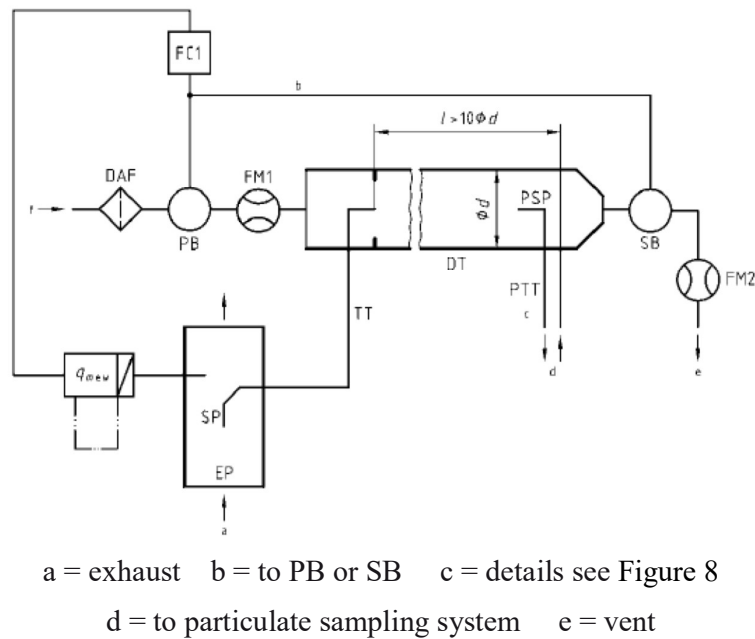


Figure 5
Scheme of Partial Flow Dilution System (Fractional Sampling Type)

A2.2.2 Components of Figures 4 and 5 above

EP Exhaust Pipe

The exhaust pipe may be insulated. To reduce the thermal inertia of the exhaust, pipe a thickness to diameter ratio of 0.015 or less is recommended. The use of flexible sections shall be limited to a length to diameter ratio of 12 or less. Bends shall be minimized to reduce inertial deposition. If the system includes a test bed silencer the silencer may also be insulated. It is recommended to have a straight pipe of six pipe diameters upstream and three pipe diameters downstream of the tip of the probe.

SP Sampling Probe

The type of probe shall be either of the following:

- (a) Open tube facing upstream on the exhaust pipe centerline;
- (b) Open tube facing downstream on the exhaust pipe centerline;
- (c) Multiple hole probe as described under SP in clause A.2.1.3;
- (d) Hatted probe facing upstream on the exhaust pipe centerline as shown in Figure 6 of this Appendix.

The minimum inside diameter of the probe tip shall be 4 mm. The minimum diameter ratio between exhaust pipe and probe shall be four.

When using probe type (a), an inertial pre-classifier (cyclone or impactor) with at 50 per cent cut point between 2.5 and 10 μm shall be installed immediately upstream of the filter holder.

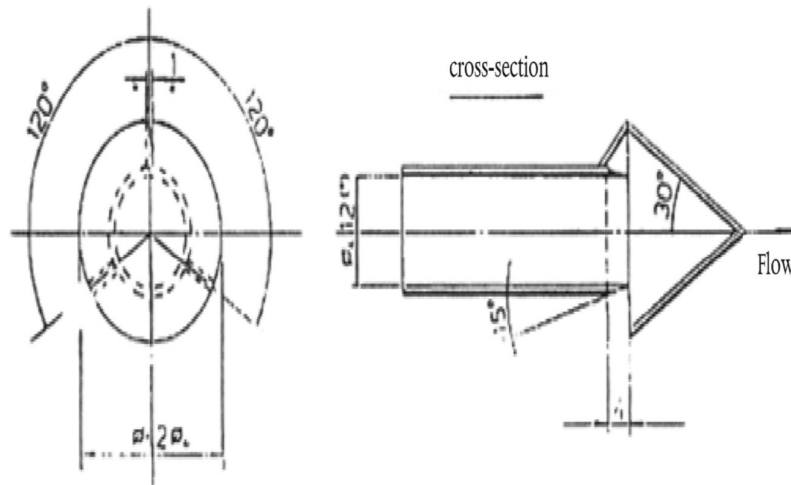


Figure 6
Scheme of Hatted Probe

TT Exhaust Transfer Tube

The transfer tube shall be as short as possible, but:

- (a) Not more than 0.26 m in length, if insulated for 80 per cent of the total length, as measured between the end of the probe and the dilution stage;

or

- (b) Not more than 1 m in length, if heated above 150 °C for 90 per cent of the total length, as measured between the end of the probe and the dilution stage.

It shall be equal to or greater than the probe diameter, but not more than 25 mm in diameter, and exiting on the centerline of the dilution tunnel and pointing downstream.

With respect to point (a) above, insulation shall be done with material with a maximum thermal conductivity of 0.05 W/mK with a radial insulation thickness corresponding to the diameter of the probe.

FC1 Flow Controller

A flow controller shall be used to control the diluent flow through the pressure blower PB and/or the suction blower SB. It may be connected to the exhaust flow sensor signals specified in clause 8.4.1 of this Chapter. The flow controller may be installed upstream or downstream of the respective blower. When using a pressurized air supply, FC1 directly controls the airflow

FM1 Flow Measurement Device

Gas meter or other flow instrumentation to measure the diluent flow. FM1 is optional if the pressure blower PB is calibrated to measure the flow.

DAF Diluent Filter

The diluent (ambient air, synthetic air, or nitrogen) shall be filtered with a high-efficiency (HEPA) filter that has an initial minimum collection efficiency of 99.97 per cent according to EN 1822-1 (filter class H14 or better), ASTM F 1471-93 or equivalent standard.

FM2 Flow Measurement Device (Fractional Sampling Type, Figure 5 of this Appendix Only)

Gas meter or other flow instrumentation to measure the diluted exhaust gas flow. FM2 is optional if the suction blower SB is calibrated to measure the flow.

PB Pressure Blower (Fractional Sampling Type Figure 5 of this Appendix Only)

To control the diluent flow rate, PB may be connected to the flow controllers FC1 or FC2. PB is not required when using a butterfly valve. PB may be used to measure the diluent flow, if calibrated.

SB Suction Blower (Fractional Sampling Type Figure 5 of this Appendix Only)

SB may be used to measure the diluted exhaust gas flow, if calibrated.

DT Dilution Tunnel (Partial flow)

The dilution tunnel:

- (a) Shall be of a sufficient length to cause complete mixing of the exhaust and diluent under turbulent flow conditions (Reynolds number, Re , greater than 4 000, where Re is based on the inside diameter of the dilution tunnel) for a fractional sampling system, i.e. complete mixing is not required for a total sampling system;
- (b) Shall be constructed of stainless steel;
- (c) May be heated to no greater than 325 K (52 °C) wall temperature;
- (d) May be insulated

PSP Particulate Sampling Probe (Fractional Sampling Type, Figure 5 of this Appendix Only)

The particulate sampling probe is the leading section of the particulate transfer tube PTT (see clause A.2.2.6) and:

- (a) Shall be installed facing upstream at a point where the diluent and exhaust gas are well mixed, i.e. on the dilution tunnel DT centreline approximately 10 tunnel diameters downstream of the point where the exhaust enters the dilution tunnel;
- (b) Shall be 8 mm in minimum inside diameter;
- (c) May be heated to no greater than 325 K (52 °C) wall temperature by direct heating or by diluent pre-heating, provided the diluent temperature does not exceed 325 K (52 °C) prior to the introduction of the exhaust into the dilution tunnel;
- (d) May be insulated.

A 2.2.3 Description of Full Flow Dilution System

A dilution system is described based upon the dilution of the total amount of raw exhaust gas in the dilution tunnel DT using the CVS (constant volume sampling) concept, and is shown in Figure 7 below.

The diluted exhaust gas flow rate shall be measured either with a positive displacement pump (PDP), with a critical flow venturi (CFV) or with a subsonic venturi (SSV). A heat exchanger (HE) or electronic flow compensation (EFC) may be used for proportional particulate sampling and for flow determination. Since particulate mass determination is based on the total diluted exhaust gas flow, it is not necessary to calculate the dilution ratio.

For subsequent collection of the particulates, a sample of the dilute exhaust gas shall be passed to the double dilution particulate sampling system (see Figure 9 of this Appendix). Although partly a dilution system, the double dilution system is described as a modification of a particulate sampling system, since it shares most of the parts with a typical particulate sampling system.

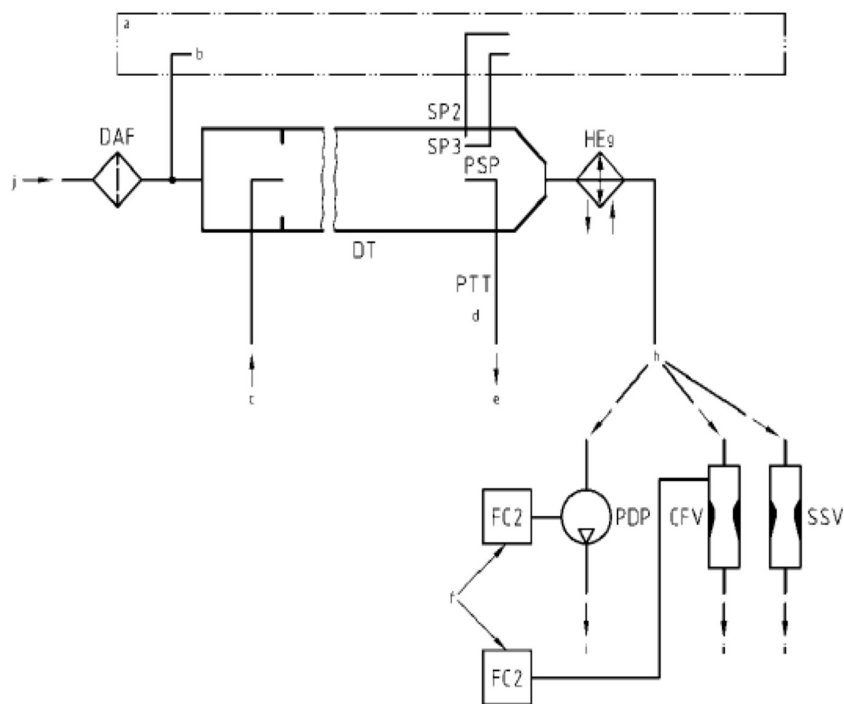


Figure 7

Scheme of Full Flow Dilution System (CVS)

a = analyzer system b = background air c = exhaust

d = details see Figure 9 e = to double dilution system

f = if EFC is used i = vent g = optional h = or

A2.2.4 Components of Figure 7 above.**EP Exhaust Pipe**

The exhaust pipe length from the exit of the engine exhaust manifold, turbocharger outlet or after-treatment device to the dilution tunnel shall be not more than 10 m. If the system exceeds 4 m in length, then all tubing in excess of 4 m shall be insulated, except for an in-line smoke meter, if used. The radial thickness of the insulation shall be at least 25 mm. The thermal conductivity of the insulating material shall have a value no greater than 0.1 W/mK measured at 673 K. To reduce the thermal inertia of the exhaust, pipe a thickness-to-diameter ratio of 0.015 or less is recommended. The use of flexible sections shall be limited to a length-to-diameter ratio of 12 or less.

PDP Positive Displacement Pump

The PDP meters total diluted exhaust flow from the number of the pump revolutions and the pump displacement. The exhaust system backpressure shall not be artificially lowered by the PDP or diluent inlet system. Static exhaust backpressure measured with the PDP system operating shall remain within ± 1.5 kPa of the static pressure measured without connection to the PDP at identical engine speed and load. The gas mixture temperature immediately ahead of the PDP shall be within ± 6 K of the average operating temperature observed during the test, when no flow compensation (EFC) is used. Flow compensation is only permitted, if the temperature at the inlet to the PDP does not exceed 323 K (50 °C).

CFV Critical Flow Venturi

CFV measures total diluted exhaust flow by maintaining the flow at choked conditions (critical flow). Static exhaust backpressure measured with the CFV system operating shall remain within ± 1.5 kPa of the static pressure measured without connection to the CFV at identical engine speed and load. The gas mixture temperature immediately ahead of the CFV shall be within ± 11 K of the average operating temperature observed during the test, when no flow compensation (EFC) is used.

SSV Subsonic Venturi

SSV measures total diluted exhaust flow by using the gas flow function of a subsonic venturi in dependence of inlet pressure and temperature and pressure drop between venturi inlet and throat. Static exhaust backpressure measured with the SSV system operating shall remain within ± 1.5 kPa of the static pressure measured without connection to the SSV at identical engine speed and load. The gas mixture temperature immediately ahead of the SSV shall be within ± 11 K of the average operating temperature observed during the test, when no flow compensation (EFC) is used.

HE Heat Exchanger (Optional)

The heat exchanger shall be of sufficient capacity to maintain the temperature within the limits required above. If EFC is used, the heat exchanger is not required.

EFC Electronic Flow Compensation (Optional)

If the temperature at the inlet to the PDP, CFV or SSV is not kept within the limits stated above, a flow compensation system is required for continuous measurement of the flow rate and control of the proportional sampling into the double dilution system. For that purpose, the continuously measured flow rate signals are used to maintain the proportionality of the sample flow rate through the particulate filters of the double dilution system (see Figure 9 of this Appendix) within ± 2.5 per cent.

DT Dilution Tunnel (Full Flow)

The dilution tunnel:

- (a) Shall be small enough in diameter to cause turbulent flow (Reynolds number, Re , greater than 4000, where Re is based on the inside diameter of the dilution tunnel) and of sufficient length to cause complete mixing of the exhaust and diluent;
- (b) May be insulated;
- (c) May be heated up to a wall temperature sufficient to eliminate aqueous condensation.

The engine exhaust shall be directed downstream at the point where it is introduced into the dilution tunnel, and thoroughly mixed. A mixing orifice may be used.

For the double dilution system, a sample from the dilution tunnel is transferred to the secondary dilution tunnel where it is further diluted, and then passed through the sampling filters (Figure 9 of this Appendix). The secondary dilution system shall provide sufficient secondary diluent to maintain the doubly diluted exhaust stream at a temperature between 315 K (42 °C) and 325 K (52 °C) immediately before the particulate filter.

DAF Diluent Filter

The diluent (ambient air, synthetic air, or nitrogen) shall be filtered with a high-efficiency (HEPA) filter that has an initial minimum collection efficiency of 99.97 per cent according to EN 1822-1 (filter class H14 or better), ASTM F 1471-93 or equivalent standard.

PSP Particulate Sampling Probe

The probe is the leading section of PTT and:

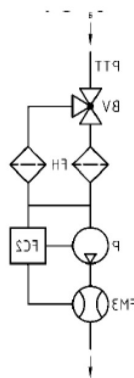
- (a) Shall be installed facing upstream at a point where the diluent and exhaust gases are well mixed, i.e. on the dilution tunnel DT centreline of the dilution systems, approximately 10 tunnel diameters downstream of the point where the exhaust enters the dilution tunnel;
- (b) Shall be of 8 mm minimum inside diameter;
- (c) May be heated to no greater than 325 K (52 °C) wall temperature by direct heating or by diluent pre-heating, provided the air temperature does not exceed 325 K (52 °C) prior to the introduction of the exhaust in the dilution tunnel;
- (d) May be insulated.

A2.2.5 Description of particulate sampling system

The particulate sampling system is required for collecting the particulates on the particulate filter and is shown in Figures 8 and 9 of this Appendix. In the case of total sampling partial flow dilution, which consists of passing the entire diluted exhaust sample through the filters, the dilution and sampling systems usually form an integral unit (see Figure 4 of this Appendix). In the case of fractional sampling partial flow dilution or full flow dilution, which consists of passing through the filters only a portion of the diluted exhaust, the dilution and sampling systems usually form different units.

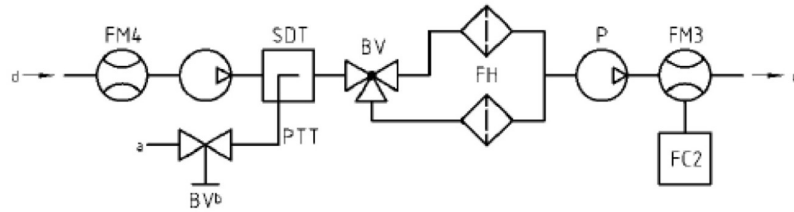
For a partial flow dilution system, a sample of the diluted exhaust gas is taken from the dilution tunnel DT through the particulate sampling probe PSP and the particulate transfer tube PTT by means of the sampling pump P, as shown in Figure 8 below. The sample is passed through the filter holder(s) FH that contain the particulate sampling filters. The sample flow rate is controlled by the flow controller FC3.

For of full flow dilution system, a double dilution particulate sampling system shall be used, as shown in Figure 9 of this Appendix. A sample of the diluted exhaust gas is transferred from the dilution tunnel DT through the particulate sampling probe PSP and the particulate transfer tube PTT to the secondary dilution tunnel SDT, where it is diluted once more. The sample is then passed through the filter holder(s) FH that contain the particulate sampling filters. The diluent flow rate is usually constant whereas the sample flow rate is controlled by the flow controller FC3. If electronic flow compensation EFC (see Figure 7) is used, the total diluted exhaust gas flow is used as command signal for FC3.



a = from dilution tunnel

Figure 8
Scheme of Particulate Sampling System



a = diluted exhaust from DT b = optional c = vent
d = secondary diluent.

Figure 9

Scheme of Double Dilution Particulate Sampling System

A2.2.6 Components of Figure 8 (Partial Flow System Only) and Figure 9 (Full Flow System Only)

PTT Particulate Transfer Tube

The transfer tube:

- (a) Shall be inert with respect to PM;
- (b) May be heated to no greater than 325 K (52 °C) wall temperature;
- (c) May be insulated.

SDT Secondary Dilution Tunnel (Figure 9 above Only)

The secondary dilution tunnel:

- (a) Shall be of sufficient length and diameter so as to comply with the residence time requirements of clause 9.4.2(f) of this Chapter;
- (b) May be heated to no greater than 325 K (52 °C) wall temperature;
- (c) May be insulated.

FH Filter Holder

The filter holder:

- (a) Shall have a 12.5 °C (from center) divergent cone angle to transition from the transfer line diameter to the exposed diameter of the filter face;
- (b) May be heated to no greater than 325 K (52 °C) wall temperature;
- (c) May be insulated.

Multiple filter changers (auto changers) are acceptable, as long as there is no interaction between sampling filters.

PTFE Membrane Filters shall be Installed in a Specific Cassette within the Filter Holder.

An inertial pre-classifier with a 50 per cent cut point between 2.5 µm and 10 µm shall be installed immediately upstream of the filter holder, if an open tube sampling probe facing upstream is used.

P Sampling Pump

FC2 Flow Controller

A flow controller shall be used for controlling the particulate sample flow rate.

FM3 Flow Measurement Device

Gas meter or flow instrumentation to determine the particulate sample flow through the particulate filter. It may be installed upstream or downstream of the sampling pump P.

FM4 Flow Measurement Device

Gas meter or flow instrumentation to determine the secondary diluent flow through the particulate filter.

Ball Valve (optional)

The ball valve shall have an inside diameter not less than the inside diameter of the particulate transfer tube PTT, and a switching time of less than 0.5 second

CHAPTER 3 - APPENDIX 3

STATISTICS

A3.1 Mean Value and Standard Deviation

The arithmetic mean value shall be calculated as follows:

$$\bar{x} = \frac{\sum_{i=1}^n x_i}{n} \quad (102)$$

The standard deviation can be calculated as follows:

$$s = \frac{\sum_{i=1}^n (x_i - \bar{x})^2}{n - 1} \quad (103)$$

A3.2 Regression Analysis

The slope of the regression shall be calculated as follows:

$$a_1 = \frac{\sum_{i=1}^n (y_i - \bar{y}) \times (x_i - \bar{x})}{\sum_{i=1}^n (x_i - \bar{x})^2} \quad (104)$$

The y intercept of the regression shall be calculated as follows:

$$a_0 = \bar{y} - (a_1 \times \bar{x}) \quad (105)$$

The standard error of estimate (SEE) shall be calculated as follows:

$$SEE = \frac{\sqrt{\sum_{i=1}^n [y_i - a_0 - (a_1 \times x_i)]^2}}{n - 2} \quad (106)$$

The coefficient of determination shall be calculated as follows:

$$r^2 = 1 - \frac{\sum_{i=1}^n [y_i - a_0 - (a_1 \times x_i)]^2}{\sum_{i=1}^n (y_i - \bar{y})^2} \quad (107)$$

A3.3 Determination of System Equivalency

The determination of system equivalency according to clause 5.1.1 of this Chapter shall be based on a seven sample pair (or larger) correlation study between the candidate system and one of the accepted reference systems of this Chapter using the appropriate test cycle(s). The equivalency criteria to be applied shall be the F-test and the two-sided Student t-test.

This statistical method examines the hypothesis that the sample standard deviation and sample mean value for an emission measured with the candidate system do not differ from the sample standard deviation and sample mean value for that emission measured with the reference system. The hypothesis shall be tested on the basis of a 10 per cent significance level of the F and t values. The critical F and t values for seven to ten sample pairs are given in Table 1 of this Appendix. If the F and t values calculated according to the equation below are greater than the critical F and t values, the candidate system is not equivalent

The following procedure shall be followed. The subscripts R and C refer to the reference and candidate system, respectively:

- (a) Conduct at least seven tests with the candidate and reference systems operated in parallel. The number of tests is referred to as n_R and n_C ;
- (b) Calculate the mean values \bar{x}_R and \bar{x}_C and the standard deviations s_R and s_C ;
- (c) Calculate the F value, as follows:

$$F = \frac{s_{major}^2}{s_{minor}^2} \quad (108)$$

(the greater of the two standard deviations s_R or s_C shall be in the numerator);

- (d) Calculate the t value, as follows:

$$t = \frac{|\bar{x}_C - \bar{x}_R|}{\sqrt{\frac{s_C^2}{n_C} + \frac{s_R^2}{n_R}}} \quad (109)$$

- (e) Compare the calculated F and t values with the critical F and t values corresponding to the respective number of tests indicated in Table 1 of this Appendix. If larger sample sizes are selected, consult statistical tables for 10 per cent significance (90 per cent confidence) level;
- (f) Determine the degrees of freedom (d_f), as follows:

For the F-test: $d_{f1} = n_R - 1, d_{f2} = n_C - 1$ (110)

For the t -test: $d_f = (n_C + n_R - 2)/2$ (111)
- (g) Determine the equivalency, as follows:
 - (i) If $F < F_{crit}$ and $t < t_{crit}$, then the candidate system is equivalent to the reference system of this Chapter;
 - (ii) If $F \geq F_{crit}$ or $t \geq t_{crit}$, then the candidate system is different from the reference system of this Chapter.

Table 1
 t and F Values for Selected Sample Sizes

Sample Size	F-test		t-test	
	d_f	F_{crit}	d_f	t_{crit}
7	6.6	3.055	6	1.943
8	7.7	2.785	7	1.895
9	8.8	2.589	8	1.860
10	9.9	2.440	9	1.833

CHAPTER 3 - APPENDIX 4

CARBON FLOW CHECK

A4.1 Introduction

All but a tiny part of the carbon in the exhaust comes from the fuel, and all but a minimal part of this is manifest in the exhaust gas as CO₂. This is the basis for a system verification check based on CO₂ measurements.

The flow of carbon into the exhaust measurement systems is determined from the fuel flow rate. The flow of carbon at various sampling points in the emissions and particulate sampling systems is determined from the CO₂ concentrations and gas flow rates at those points.

In this sense, the engine provides a known source of carbon flow, and observing the same carbon flow in the exhaust pipe and at the outlet of the partial flow PM sampling system verifies leak integrity and flow measurement accuracy. This check has the advantage that the components are operating under actual engine test conditions of temperature and flow.

Figure 1 below shows the sampling points at which the carbon flows shall be checked. The specific equations for the carbon flows at each of the sample points are given below.

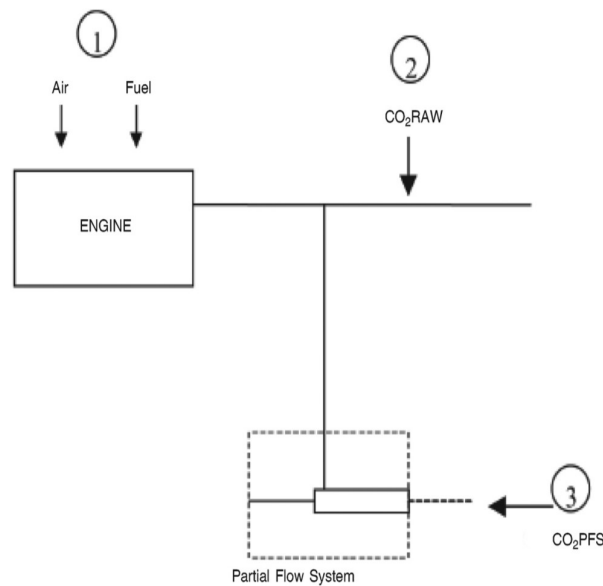


Figure 1
Measuring Points for Carbon Flow Check

A 4.2 Carbon Flow Rate into the Engine (Location 1)

The carbon mass flow rate into the engine for a fuel CH_aO_e is given by:

$$q_{mcf} = \frac{12.011}{12.011 + 1.00794\alpha + 15.9994\epsilon} \cdot q_{mf} \quad (112)$$

Where:

q_{mf} is the fuel mass flow rate, kg/s

A 4.3 Carbon Flow Rate in the Raw Exhaust (Location 2)

The carbon mass flow rate in the exhaust pipe of the engine shall be determined from the raw CO₂ concentration and the exhaust gas mass flow rate:

$$q_{mCe} = \left(\frac{c_{CO_2,r} - c_{CO_2,a}}{100} \right) \times q_{mew} \times \frac{12.011}{M_e} \quad (113)$$

Where:

$c_{CO_2,r}$ is the wet CO₂ concentration in the raw exhaust gas, per cent

$c_{CO_2,a}$ is the wet CO₂ concentration in the ambient air, per cent

q_{mew} is the exhaust gas mass flow rate on wet basis, kg/s

M_e is the molar mass of exhaust gas, g/mol

If CO₂ is measured on a dry basis it shall be converted to a wet basis according to clause 8.1 of this Chapter

A 4.4 Carbon Flow Rate in the Dilution System (Location 3)

For the partial flow dilution system, the splitting ratio also needs to be taken into account. The carbon flow rate shall be determined from the dilute CO₂ concentration, the exhaust gas mass flow rate and the sample flow rate:

$$q_{mCp} = \left(\frac{c_{CO_2,d} - c_{CO_2,a}}{100} \right) \times q_{mdew} \times \frac{12.011}{M_e} \times \frac{q_{mew}}{q_{mp}} \quad (114)$$

$c_{CO_2,d}$ is the wet CO₂ concentration in the dilute exhaust gas at the outlet of the dilution tunnel, per cent

$c_{CO_2,a}$ is the wet CO₂ concentration in the ambient air, per cent

q_{mew} is the exhaust gas mass flow rate on wet basis, kg/s

q_{mp} is the sample flow of exhaust gas into partial flow dilution system, kg/s

M_e is the molar mass of exhaust gas, g/mol

If CO₂ is measured on a dry basis, it shall be converted to wet basis according to clause 8.1 of this Chapter.

A 4.5 Calculation of the Molar Mass of the Exhaust Gas

The molar mass of the exhaust gas shall be calculated according to equation 41 (see clause 8.4.2.4 of this Chapter).

Alternatively, the following exhaust gas molar masses may be used:

M_e (diesel) = 28.9 g/mol

M_e (LPG) = 28.6 g/mol

M_e (NG) = 28.3 g/mol

CHAPTER 3 - APPENDIX 5

EXAMPLE OF CALCULATION PROCEDURE

A 5.1 Speed and Torque Denormalization Procedure

As an example, the following test point shall be denormalized:

per cent speed = 43 per cent

per cent torque = 82 per cent

Given the following values:

$n_{lo} = 1\,015\text{ min}^{-1}$

$n_{hi} = 2\,200\text{ min}^{-1}$

$n_{pref} = 1\,300\text{ min}^{-1}$

$n_{idle} = 600\text{ min}^{-1}$

results in:

$$actual\ speed = \frac{43 \times (0.45 \times 1015 + 0.45 \times 1300 + 0.1 \times 2200 - 600) \times 2.0327}{100} + 600 = 1.178\text{min}^{-1}$$

With the maximum torque of 700 Nm observed from the mapping curve at $1,178\text{ min}^{-1}$

$$actual\ torque = \frac{82 \times 700}{100} = 574\text{ Nm}$$

A 5.2 Basic Data for Stoichiometric Calculations

Atomic mass of hydrogen	1.00794 g/atom
Atomic mass of carbon	12.011 g/atom
Atomic mass of sulphur	32.065 g/atom
Atomic mass of nitrogen	14.0067 g/atom
Atomic mass of oxygen	15.9994 g/atom
Atomic mass of argon	39.9 g/atom
Molar mass of water	18.01534 g/mol
Molar mass of carbon dioxide	44.01 g/mol
Molar mass of carbon monoxide	28.011 g/mol
Molar mass of oxygen	31.9988 g/mol
Molar mass of nitrogen	28.011 g/mol
Molar mass of nitric oxide	30.008 g/mol
Molar mass of nitrogen dioxide	46.01 g/mol
Molar mass of sulphur dioxide	64.066 g/mol
Molar mass of dry air	28.965 g/mol

Assuming no compressibility effects, all gases involved in the engine intake/combustion/exhaust process can be considered to be ideal and any volumetric calculations shall therefore be based on a molar volume of 22.414 l/mol according to Avogadro's hypothesis.

A 5.3 Gaseous Emissions (Diesel Fuel)

The measurement data of an individual point of the test cycle (data sampling rate of 1 Hz) for the calculation of the instantaneous mass emission are shown below. In this example, CO and NO_x are measured on a dry basis, HC on a wet basis. The HC concentration is given in propane equivalent (C3) and has to be multiplied by 3 to result in the C1 equivalent. The calculation procedure is identical for the other points of the cycle.

The calculation example shows the rounded intermediate results of the different steps for better illustration. It should be noted that for actual calculation, rounding of intermediate results is not permitted (see clause 8. of this Chapter).

T _{a,i} (K)	H _{a,i} (g/kg)	W _{act} (kWh)	q _{mew,i} (kg/s)	q _{maw,i} (kg/s)	q _{mf,i} (kg/s)	c _{HC,i} ppm	c _{CO, i} ppm	c _{NOx,i} ppm
295	8.0	40	0.155	0.150	0.005	10	40	500

The following fuel composition is considered:

Component	Molar ratio	Per cent mass
H	$\alpha = 1.8529$	$w_{ALF} = 13.45$
C	$\beta = 1.0000$	$w_{BET} = 86.50$
S	$\gamma = 0.0002$	$w_{GAM} = 0.050$
N	$\delta = 0.0000$	$w_{DEL} = 0.000$
O	$\varepsilon = 0.0000$	$w_{EPS} = 0.000$

Step 1: Dry/wet correction (clause 8.1 of this Chapter):

Equation 16:

$$kf = 0.055584 \times 13.45 - 0.0001083 \times 86.5 - 0.0001562 \times 0.05 = 0.7382$$

Equation 13:

$$k_{w,a} = \left(1 - \frac{1.2434 \times 8 + 111.12 \times 13.45 \times \frac{0.005}{0.148}}{773.4 + 1.2434 \times 8 + \frac{0.005}{0.148} \times 0.7382 \times 1,000} \right) \times 1.008 = 0.9331$$

Equation 12:

$$c_{CO,i}(\text{wet}) = 40 \times 0.9331 = 37.3 \text{ ppm}$$

$$c_{NOx,i}(\text{wet}) = 500 \times 0.9331 = 466.6 \text{ ppm}$$

Step 2: NO_x correction for temperature and humidity (clause 8.2.1 of this Chapter):

Equation 23:

$$k_{h,D} = \frac{15.698 \times 8,00}{1000} + 0.832 = 0.9576$$

Step 3: Calculation of the instantaneous emission of each individual point of the cycle (clause 8.4.2.3 of this Chapter):

Equation 36:

$$m_{HC,i} = 10 \times 3 \times 0.155 = 4.650$$

$$m_{CO,i} = 37.3 \times 0.155 = 5.782$$

$$m_{NOx,i} = 466.6 \times 0.9576 \times 0.155 = 69.26$$

Step 4: Calculation of the mass emission over the cycle by integration of the instantaneous emission values and the u values from Table 5 (clause 8.4.2.3 of this Chapter):

The following calculation is assumed for the WHTC cycle (1,800 s) and the same emission in each point of the cycle.

Equation 36:

$$m_{HC} = 0.000479 \times \sum_{i=1}^{1800} 4.650 = 4.01 \text{ g/test}$$

$$m_{CO} = 0.000966 \times \sum_{i=1}^{1800} 5.782 = 10.05 \text{ g/test}$$

$$m_{NOx} = 0.001586 \times \sum_{i=1}^{1800} 69.26 = 197.72 \text{ g/test}$$

Step 5: Calculation of the specific emissions (clause 8.6.3 of this Chapter):

Equation 69:

$$e_{HC} = 4.01/40 = 0.10 \text{ g/kWh}$$

$$e_{CO} = 10.05/40 = 0.25 \text{ g/kWh}$$

$$e_{NOx} = 197.72/40 = 4.94 \text{ g/kWh}$$

A5.4 Particulate Emission (Diesel Fuel)

P _{b,b} (kPa)	P _{b,a} (kPa)	W _{act} (kWh)	Q _{mew,i} (kg/s)	Q _{mf,i} (kg/s)	Q _{mdw,i} (kg/s)	Q _{mdew,i} (kg/s)	m _{uncor,b} (mg)	m _{uncor,a} (mg)	m _{sep} (kg)
99	100	40	0.155	0.005	0.0015	0.0020	90.000	91.700	1.515

Step 1: Calculation of m_{edf} (clause 8.4.3.2.2 of this Chapter):

Equation 48: $r_{d,I} = 0.002 / (0.002 - 0.0015) = 4$

Equation 47: $q_{\text{medf},I} = 0.155 \times 4 = 0.620 \text{ kg/s}$

Equation 46: $m_{\text{edf}} = \sum_{i=1}^{1800} 0.620 = 1,116 \text{ kg/test}$

Step 2: Buoyancy correction of the particulate mass (clause 8.3 of this Chapter):

Before test:

Equation 26:

$$\rho_{a,b} = \frac{99 \times 28.836}{8.3144 \times 295} = 1.164 \text{ kg /m}^3$$

Equation 25:

$$m_{f,T} = 90.0000 \times \frac{\left(1 - \frac{1.164}{8000}\right)}{\left(1 - \frac{1.164}{2300}\right)} = 90.0325 \text{ mg}$$

After test:

Equation 26:

$$\rho_{a,a} = \frac{100 \times 28.836}{8.3144 \times 295} = 1.176 \text{ kg /m}^3$$

Equation 25:

$$m_{f,G} = 91.7000 \times \frac{\left(1 - \frac{1.176}{8000}\right)}{\left(1 - \frac{1.176}{2300}\right)} = 91.7334 \text{ mg}$$

Equation 27:

$$m_p = 91.7334 \text{ mg} - 90.0325 \text{ mg} = 1.7009 \text{ mg}$$

Step 3: Calculation of the particulate mass emission (clause 8.4.3.2.2 of this Chapter):

Equation 45:

$$m_{PM} = \frac{1.7009 \times 1.116}{1.515 \times 1000} = 1.253 \text{ g/test}$$

Step 4: Calculation of the specific emission (clause 8.6.3 of this Chapter):

Equation 69:

$$e_{PM} = 1.253/40 = 0.031 \text{ g/kWh}$$

A 5.5 λ - Shift factor (S_λ)**A5.5.1 Calculation of the λ -shift factor (S_λ) ⁽¹⁾**

$$S_\lambda = \frac{2}{\left(1 - \frac{\text{inert}\%}{100}\right)\left(n + \frac{m}{4}\right) - \frac{O_2^*}{100}}$$

Where:

S_λ = λ -shift factor;

inert % = per cent by volume of inert gases in the fuel (i.e. N₂, CO₂, He, etc.);

O₂ * = per cent by volume of original oxygen in the fuel;

n and m = refer to average C_nH_m representing the fuel hydrocarbons, i.e.:

$$n = \frac{1 \times \left[\frac{CH_4\%}{100}\right] + 2 \times \left[\frac{C_2\%}{100}\right] + 3 \times \left[\frac{C_3\%}{100}\right] + 4 \times \left[\frac{C_4\%}{100}\right] + 5 \times \left[\frac{C_5\%}{100}\right] + \dots}{\frac{1 - \text{diluent}\%}{100}}$$

$$m = \frac{4 \times \left[\frac{CH_4\%}{100}\right] + 4 \times \left[\frac{C_2H_4\%}{100}\right] + 6 \times \left[\frac{C_3H_6\%}{100}\right] + \dots + 8 \times \left[\frac{C_4H_8\%}{100}\right] + \dots}{\frac{1 - \text{diluent}\%}{100}}$$

Where:

CH₄ = per cent by volume of methane in the fuel;

C₂ = per cent by volume of all C₂ hydrocarbons (e.g.: C₂H₆, C₂H₄, etc.) in the fuel;

C₃ = per cent by volume of all C₃ hydrocarbons (e.g.: C₃H₈, C₃H₆, etc.) in the fuel;

C₄ = per cent by volume of all C₄ hydrocarbons (e.g.: C₄H₁₀, C₄H₈, etc.) in the fuel;

C₅ = per cent by volume of all C₅ hydrocarbons (e.g.: C₅H₁₂, C₅H₁₀, etc.) in the fuel;

diluent = per cent by volume of dilution gases in the fuel (i.e.: O₂ *, N₂, CO₂, He, etc.).

1. Stoichiometric Air/Fuel ratios of automotive fuels - SAE J1829, June 1987. John B. Heywood, Internal combustion engine fundamentals, McGraw-Hill, 1988, Chapter 3.4 "Combustion stoichiometry" (pp. 68 to 72).

A5.5.2 Examples for the calculation of the λ -shift factor S_λ :Example 1: G25: CH₄ = 86 per cent, N₂ = 14 per cent (by volume)

$$n = \frac{1 \times \left[\frac{\text{CH}_4 \%}{100} \right] + 2 \times \left[\frac{\text{C}_2 \%}{100} \right] + \dots}{\frac{1 - \text{diluent \%}}{100}} = \frac{1 \times 0.86}{1 - \frac{14}{100}} = \frac{0.86}{0.86} = 1$$

$$m = \frac{4 \times \left[\frac{\text{CH}_4 \%}{100} \right] + 4 \times \left[\frac{\text{C}_2\text{H}_4 \%}{100} \right] + \dots}{\frac{1 - \text{diluent \%}}{100}} = \frac{4 \times 0.86}{0.86} = 4$$

$$S_\lambda = \frac{2}{\left(1 - \frac{\text{inert \%}}{100}\right) \left(n + \frac{m}{4}\right) - \frac{\text{O}_2^*}{100}} = \frac{2}{\left(1 - \frac{14}{100}\right) \times \left(1 + \frac{4}{4}\right)} = 1.16$$

Example 2: G_R : CH₄ = 87 per cent, C₂H₆ = 13 per cent (by volume)

$$n = \frac{1 \times \left[\frac{\text{CH}_4 \%}{100} \right] + 2 \times \left[\frac{\text{C}_2 \%}{100} \right] + \dots}{\frac{1 - \text{diluent \%}}{100}} = \frac{1 \times 0.87 + 2 \times 0.13}{1 - \frac{0}{100}} = \frac{1.13}{1} = 1.13$$

$$m = \frac{4 \times \left[\frac{\text{CH}_4 \%}{100} \right] + 4 \times \left[\frac{\text{C}_2\text{H}_4 \%}{100} \right] + \dots}{\frac{1 - \text{diluent \%}}{100}} = \frac{4 \times 0.87 + 6 \times 0.13}{1} = 4.26$$

$$S_\lambda = \frac{2}{\left(1 - \frac{\text{inert \%}}{100}\right) \left(n + \frac{m}{4}\right) - \frac{\text{O}_2^*}{100}} = \frac{2}{\left(1 - \frac{0}{100}\right) \times \left(1.13 + \frac{4.26}{4}\right)} = 0.911$$

	<p>Example 3: USA: CH₄ = 89 per cent, C₂H₆ = 4.5 per cent, C₃H₈ = 2.3 per cent, C₆H₁₄ = 0.2 per cent, O₂ = 0.6 per cent, N₂ = 4 per cent</p>
	$n = \frac{1 \times \left[\frac{\text{CH}_4\%}{100} \right] + 2 \times \left[\frac{\text{C}_2\%}{100} \right] + \dots}{1 - \frac{\text{diluent}\%}{100}} = \frac{1 \times 0.89 + 2 \times 0.045 + 3 \times 0.023 + 4 \times 0.002}{1 - \frac{0.64 + 4}{100}} = 1.11$ $m = \frac{4 \times \left[\frac{\text{CH}_4\%}{100} \right] + 4 \times \left[\frac{\text{C}_2\text{H}_4\%}{100} \right] + 6 \times \left[\frac{\text{C}_2\text{H}_6\%}{100} \right] + \dots + 8 \times \left[\frac{\text{C}_3\text{H}_8\%}{100} \right]}{1 - \frac{\text{diluent}\%}{100}} =$ $= \frac{4 \times 0.89 + 4 \times 0.045 + 8 \times 0.023 + 14 \times 0.002}{1 - \frac{0.6 + 4}{100}} = 4.24$ $S_\lambda = \frac{2}{\left(1 - \frac{\text{inert}\%}{100}\right) \left(n + \frac{m}{4}\right) - \frac{\text{O}_2^*}{100}} = \frac{2}{\left(1 - \frac{4}{100}\right) \times \left(1.11 + \frac{4.24}{4}\right) - \frac{0.6}{100}} = 0.96$

CHAPTER 3 - APPENDIX 6
INSTALLATION OF AUXILIARIES AND
EQUIPMENT FOR EMISSION TEST

Sr. Number	Auxiliaries	Fitted for emission test
1	Inlet system	
	Inlet manifold	Yes
	Crank case emission control system	Yes
	Control devices for dual induction inlet manifold system	Yes
	Air flow meter	Yes
	Air inlet duct work	Yes, or test cell equipment
	Air filter	Yes, or test cell equipment
	Inlet silencer	Yes, or test cell equipment
	Speed limiting device	Yes
2	Induction-heating device for inlet manifold	Yes, if possible to be set in the most favorable condition
3	Exhaust system	
	Exhaust manifold	Yes
	Connecting pipes	Yes
	Silencer	Yes
	Tail pipe	Yes
	Exhaust brake	No, or fully open
	Pressure charging device	Yes
4	Fuel supply pump	Yes
5	Equipment for gas engines	
	Electronic control system, air flow meter, etc.	Yes
	Pressure reducer	Yes
	Evaporator	Yes
	Mixer	Yes

6	Fuel injection equipment	
	Prefilter	Yes
	Filter	Yes
	Pump	Yes
	High pressure pipe	Yes
	Injector	Yes
	Air inlet valve	Yes
	Electronic control system, sensors etc.	Yes
	Governor/control system	Yes
	Automatic full load stops for the control rack depending on atmospheric conditions	Yes
7	Liquid cooling equipment	
	Radiator	No
	Fan	No
	Fan cowl	No
	Water pump	Yes
	Thermostat	Yes, may be fixed fully open
8	Air cooling	
	Cowl	No
	Fan or Blower	No
	Temperature regulating device	No
9	Electrical equipment	
	Generator	No
	Coil or coils	Yes
	Wiring	Yes
	Electronic control system	Yes

10	Intake air charging equipment	
	Compressor driven either directly by the engine and/or by the exhaust gases	Yes
	Charge air cooler	Yes, or test cell system
	Coolant pump or fan (engine driven)	No
	Coolant flow control device	Yes
11	Anti-pollution device (exhaust after-treatment system)	Yes
12	Starting equipment	Yes, or test cell system
13	Lubricating oil pump	Yes

CHAPTER 3 - APPENDIX 7

PROCEDURE FOR THE MEASUREMENT OF AMMONIA

A7.1 This Appendix describes the procedure for measurement of ammonia (NH₃). For non-linear analysers, the use of linearising circuits shall be permitted.

A.7.2. Two measurement principles are specified for NH₃ measurement and either principle may be used provided it meets the criteria specified in clause A.7.2.1. or A.7.2.2., respectively. Gas dryers shall not be permitted for NH₃ measurement.

A.7.2.1. Laser Diode Spectrometer (LDS)

A.7.2.1.1. Measurement principle

The LDS employs the single line spectroscopy principle. The NH₃ absorption line is chosen in the near infrared spectral range and scanned by a single-mode diode laser.

A.7.2.1.2 Installation

The analyser shall be installed either directly in the exhaust pipe (in-situ) or within an analyser cabinet using extractive sampling in accordance with the instrument manufacturer's instructions. If installed in an analyser cabinet, the sample path (sampling line, pre-filter(s) and valves) shall be made of stainless steel or PTFE and shall be heated to 463±10 K (190±10°C) in order to minimize NH₃ losses and sampling artefacts. In addition, the sampling line shall be as short as practically possible.

Influence from exhaust temperature and pressure, installation environment and vibrations on the measurement shall be minimized, or compensation techniques be used.

If applicable, sheath air used in conjunction with in-situ measurement for protection of the instrument, shall not affect the concentration of any exhaust component measured downstream of the device, or sampling of other exhaust components shall be made upstream of the device.

A.7.2.1.3. Cross interference

The spectral resolution of the laser shall be within 0.5 cm⁻¹ in order to minimize cross interference from other gases present in the exhaust gas.

A.7.2.2. Fourier Transform Infrared (hereinafter FTIR) analyser

A.7.2.2.1 Measurement principle

The FTIR employs the broad waveband infrared spectroscopy principle. It allows simultaneous measurement of exhaust components whose standardized spectra are available in the instrument. The absorption spectrum (intensity/wavelength) is calculated from the measured interferogram (intensity/time) by means of the Fourier transform method.

A.7.2.2.2. Installation and sampling

The FTIR shall be installed in accordance with the instrument manufacturer's instructions. The NH_3 wavelength shall be selected for evaluation. The sample path (sampling line, pre-filter(s) and valves) shall be made of stainless steel or PTFE and shall be heated to 463 ± 10 K ($190 \pm 10^\circ\text{C}$) in order to minimize NH_3 losses and sampling artefacts. In addition, the sampling line shall be as short as practically possible

A.7.2.2.3. Cross interference

The spectral resolution of the NH_3 wavelength shall be within 0.5 cm^{-1} in order to minimize cross interference from other gases present in the exhaust gas.

A.7.3. Emissions Test Procedure and Evaluation**A.7.3.1 Checking the analysers**

Prior to the emissions test, the analyser range shall be selected. Emission analysers with automatic or manual range switching shall be permitted. During the test cycle, the range of the analysers shall not be switched.

Zero and span response shall be determined, if the provisions of clause A.7.3.4.2. do not apply for the instrument. For the span response, a NH_3 gas that meets the specifications of clause A.7.4.2.7. shall be used. The use of reference cells that contain NH_3 span gas is permitted.

A.7.3.2 Collection of emission relevant data

At the start of the test sequence, the NH_3 data collection shall be started, simultaneously. The NH_3 concentration shall be measured continuously and stored with at least 1 Hz on a computer system.

A.7.3.3. Operations after test

At the completion of the test, sampling shall continue until system response times have elapsed. Determination of analyser's drift according to clause A.7.3.4.1. shall only be required if the information in clause A.7.3.4.2. is not available

A.7.3.4.	Analyser drift
A7.3.4.1	As soon as practical but no later than 30 minutes after the test cycle is complete or during the soak period, the zero and span responses of the analyser shall be determined. The difference between the pre-test and post-test results shall be less than 2 per cent of full scale.
A7.3.4.2	Determination of analyser drift is not required in the following situations:
	<p>(a) if the zero and span drift specified by the instrument manufacturer in clauses A.7.4.2.3. and A.7.4.2.4. meets the requirements of clause A.7.3.4.1.,</p> <p>(b) the time interval for zero and span drift specified by the instrument manufacturer in clauses A.7.4.2.3. and A.7.4.2.4. exceeds the duration of the test.</p>
A7.3.5	Data evaluation
	<p>The average NH₃ concentration (ppm/test) shall be determined by integrating the instantaneous values over the cycle. The following equation shall be applied:</p> $c_{\text{NH}_3} = \frac{1}{n} \sum_{i=1}^{i=n} c_{\text{NH}_3,i} \quad \text{in (ppm/test)} \quad (115)$ <p>where:</p> <p>$c_{\text{NH}_3,i}$ is the instantaneous NH₃ concentration in the exhaust gas, ppm</p> <p>n is the number of measurements</p> <p>For the WHTC, the final test result shall be determined with the following equation:</p> $c_{\text{NH}_3} = (0.14 \times c_{\text{NH}_3,\text{cold}}) + (0.86 \times c_{\text{NH}_3,\text{hot}}) \quad (116)$ <p>where:</p> <p>$c_{\text{NH}_3,\text{cold}}$ is the average NH₃ concentration of the cold start test, ppm</p> <p>$c_{\text{NH}_3,\text{hot}}$ is the average NH₃ concentration of the hot start test, ppm</p>

A 7.4 Analyser Specification and Verification**A.7.4.1. Linearity requirements**

The analyser shall comply with the linearity requirements specified in Table 7 of this Chapter. The linearity verification in accordance with clause 9.2.1. of this Chapter, shall be performed at least every 12 months or whenever a system repair or change is made that could influence calibration. With the prior approval of the Test Agency, less than 10 reference points are permitted, if an equivalent accuracy can be demonstrated.

For the linearity verification, a NH_3 gas that meets the specifications of clause A.7.4.2.7. shall be used. The use of reference cells that contain NH_3 span gas shall be permitted.

Instruments, whose signals are used for compensation algorithms, shall meet the linearity requirements specified in Table 7 of this Chapter. Linearity verification shall be done as required by internal audit procedures, by the instrument manufacturer or in accordance with ISO 9000 requirements

A 7.4.2 Analyser specifications

The analyser shall have a measuring range and response time appropriate for the accuracy required to measure the concentration of NH_3 under transient and steady state conditions

A7.4.2.1 Minimum detection limit

The analyser shall have a minimum detection limit of < 2 ppm under all conditions of testing

A7.4.2.2 Accuracy

The accuracy, defined as the deviation of the analyser reading from the reference value, shall not exceed ± 3 per cent of the reading or ± 2 ppm, whichever is larger.

A7.4.2.3 Zero drift

The drift of the zero response and the related time interval shall be specified by the instrument manufacturer.

A7.4.2.4 Span drift

The drift of the span response and the related time interval shall be specified by the instrument manufacturer.

A7.4.2.5 System response time

The system response time shall be ≤ 20 s

A7.4.2.6 Rise time

The rise time of the analyser shall be ≤ 5 s

A7.4.2.7 NH₃ calibration gas

A gas mixture with the following chemical composition shall be available.

NH₃ and purified nitrogen

The true concentration of the calibration gas shall be within ± 3 per cent of the nominal value. The concentration of NH₃ shall be given on a volume basis (volume percent or volume ppm).

The expiration date of the calibration gases stated by the manufacturer shall be recorded.

A7.5 Alternative systems

Other systems or analysers may be approved by the Test Agency, if it is found that they yield equivalent results in accordance with clause 5.1.1 of this Chapter.

"Results" shall refer to average cycle specific NH₃ concentrations.

CHAPTER 3 - APPENDIX 8

PARTICLE NUMBER EMISSIONS MEASUREMENT EQUIPMENT

A8.1 Specification

A8.1.1 System Overview

A8.1.1.1 The particle sampling system shall consist of a probe or sampling point extracting a sample from a homogeneously mixed flow in a dilution system as described in Appendix 2 of this Chapter, clause A.2.2.1 and A.2.2.2 or A.2.2.3 and A.2.2.4, a volatile particle remover (VPR) upstream of a particle number counter (PNC) and suitable transfer tubing.

A8.1.1.2 It is recommended that a particle size pre-classifier (e.g. cyclone, impactor, etc.) be located prior to the inlet of the VPR. However, a sample probe acting as an appropriate size-classification device, such as that shown in Appendix 2 of this Chapter, Figure 6, is an acceptable alternative to the use of a particle size pre-classifier. In the case of partial flow dilution systems, it is acceptable to use the same pre-classifier for particulate mass and particle number sampling, extracting the particle number sample from the dilution system downstream of the pre-classifier. Alternatively, separate pre-classifiers may be used, extracting the particle number sample from the dilution system upstream of the particulate mass pre-classifier.

A8.1.2 General Requirements

8.1.2.1 The particle sampling point shall be located within a dilution system

The sampling probe tip or particle sampling point and particle transfer tube (PTT) together comprise the particle transfer system (PTS). The PTS conducts the sample from the dilution tunnel to the entrance of the VPR. The PTS shall meet the following conditions:

In the case of full flow dilution systems and partial flow dilution systems of the fractional sampling type (as described in Appendix 2 of this Chapter, clause A.2.2.1) the sampling probe shall be installed near the tunnel centre line, 10 to 20 tunnel diameters downstream of the gas inlet, facing upstream into the tunnel gas flow with its axis at the tip parallel to that of the dilution tunnel. The sampling probe shall be positioned within the dilution tract so that the sample is taken from a homogeneous diluent/exhaust mixture.

In the case of partial flow dilution systems of the total sampling type (as described in Appendix 2 of this Chapter, clause A.2.2.1) the particle sampling point or sampling probe shall be located in

the particulate transfer tube, upstream of the particulate filter holder, flow measurement device and any sample/bypass bifurcation point. The sampling point or sampling probe shall be positioned so that the sample is taken from a homogeneous diluent/exhaust mixture. The dimensions of the particle sampling probe should be sized not to interfere with the operation of the partial flow dilution system.

Sample gas drawn through the PTS shall meet the following conditions:

In the case of full flow dilution systems, it shall have a flow Reynolds number (Re) of $< 1\,700$;

In the case of partial flow dilution systems, it shall have a flow Reynolds number (Re) of $< 1\,700$ in the PTT i.e. downstream of the sampling probe or point;

It shall have a residence time in the PTS of ≤ 3 seconds.

Any other sampling configuration for the PTS for which equivalent particle penetration at 30 nm can be demonstrated will be considered acceptable.

The outlet tube (OT) conducting the diluted sample from the VPR to the inlet of the PNC shall have the following properties:

It shall have an internal diameter of ≥ 4 mm;

Sample Gas flow through the OT shall have a residence time of ≤ 0.8 second.

Any other sampling configuration for the OT for which equivalent particle penetration at 30 nm can be demonstrated will be considered acceptable.

A8.1.2.2 The VPR shall include devices for sample dilution and for volatile particle removal.

A8.1.2.3 All parts of the dilution system and the sampling system from the exhaust pipe up to the PNC, which are in contact with raw and diluted exhaust gas, shall be designed to minimize deposition of the particles. All parts shall be made of electrically conductive materials that do not react with exhaust gas components, and shall be electrically grounded to prevent electrostatic effects.

A8.1.2.4 The particle sampling system shall incorporate good aerosol sampling practice that includes the avoidance of sharp bends and abrupt changes in cross-section, the use of smooth internal surfaces and the minimization of the length of the sampling line. Gradual changes in the cross-section are permissible.

A.8.1.3 Specific Requirements

- A.8.1.3.1 The particle sample shall not pass through a pump before passing through the PNC.
- A.8.1.3.2 A sample pre-classifier is recommended.
- A.8.1.3.3 The sample preconditioning unit shall:
 - A.8.1.3.3.1 Be capable of diluting the sample in one or more stages to achieve a particle number concentration below the upper threshold of the single particle count mode of the PNC and a gas temperature below 35 °C at the inlet to the PNC;
 - A.8.1.3.3.2 Include an initial heated dilution stage which outputs a sample at a temperature of ≥ 150 °C and ≤ 400 °C, and dilutes by a factor of at least 10;
 - A.8.1.3.3.3 Control heated stages to constant nominal operating temperatures, within the range specified in clause A.8.1.3.3.2, to a tolerance of ± 10 °C. Provide an indication of whether or not heated stages are at their correct operating temperatures;
 - A.8.1.3.3.4 Achieve a particle concentration reduction factor (fr(di)), as defined in clause A.8.2.2.2 below, for particles of 30 nm and 50 nm electrical mobility diameters, that is no more than 30 per cent and 20 per cent respectively higher, and no more than 5 per cent lower than that for particles of 100 nm electrical mobility diameter for the VPR as a whole;
 - A.8.1.3.3.5 Also achieve > 99.0 per cent vaporization of 30 nm tetracontane ($\text{CH}_3(\text{CH}_2)_{38}\text{CH}_3$) particles, with an inlet concentration of $\geq 10000 \text{ cm}^{-3}$, by means of heating and reduction of partial pressures of the tetracontane.
- A.8.1.3.4 The PNC shall:
 - A.8.1.3.4.1 Operate under full flow operating conditions;
 - A.8.1.3.4.2 Have a counting accuracy of ± 10 per cent across the range 1 cm^{-3} to the upper threshold of the single particle count mode of the PNC against a traceable standard. At concentrations below 100 cm^{-3} measurements averaged over extended sampling periods may be required to demonstrate the accuracy of the PNC with a high degree of statistical confidence;
 - A.8.1.3.4.3 Have a readability of at least $0.1 \text{ particle cm}^{-3}$ at concentrations below 100 cm^{-3} ;
 - A.8.1.3.4.4 Have a linear response to particle concentrations over the full measurement range in single particle count mode;
 - A.8.1.3.4.5 Have a data reporting frequency equal to or greater than 0.5 Hz;

- A.8.1.3.4.6 Have a t_{90} response time over the measured concentration range of less than 5 s;
- A.8.1.3.4.7 Incorporate a coincidence correction function up to a maximum 10 per cent correction, and may make use of an internal calibration factor as determined in clause A.8.2.1.3, but shall not make use of any other algorithm to correct for or define the counting efficiency;
- A.8.1.3.4.8 Have counting efficiencies at particle sizes of 23 nm (± 1 nm) and 41 nm (± 1 nm) electrical mobility diameter of 50 per cent (± 12 per cent) and > 90 per cent respectively. These counting efficiencies may be achieved by internal (for example; control of instrument design) or external (for example; size pre-classification) means;
- A.8.1.3.4.9 If the PNC makes use of a working liquid, it shall be replaced at the frequency specified by the instrument manufacturer.
- A.8.1.3.5. Where they are not held at a known constant level at the point at which PNC flow rate is controlled, the pressure and/or temperature at inlet to the PNC shall be measured and reported for the purposes of correcting particle concentration measurements to standard conditions.
- A.8.1.3.6. The sum of the residence time of the PTS, VPR and OT plus the t_{90} response time of the PNC shall be no greater than 20 s.
- A.8.1.3.7 The transformation time of the entire particle number sampling system (PTS, VPR, OT and PNC) shall be determined by aerosol switching directly at the inlet of the PTS. The aerosol switching shall be done in less than 0.1 s. The aerosol used for the test shall cause a concentration change of at least 60 per cent full scale (FS).

The concentration trace shall be recorded. For time alignment of the particle number concentration and exhaust flow signals, the transformation time is defined as the time from the change (t_0) until the response is 50 per cent of the final reading (t_{50}).

A.8.1.4 Recommended System Description

The following paragraph contains the recommended practice for measurement of particle number. However, any system meeting the performance specifications in clause A.8.1.2 and A.8.1.3 is acceptable

Figures 1 and 2 of this Appendix are schematic drawings of the recommended particle sampling system configures for partial and full flow dilution systems respectively

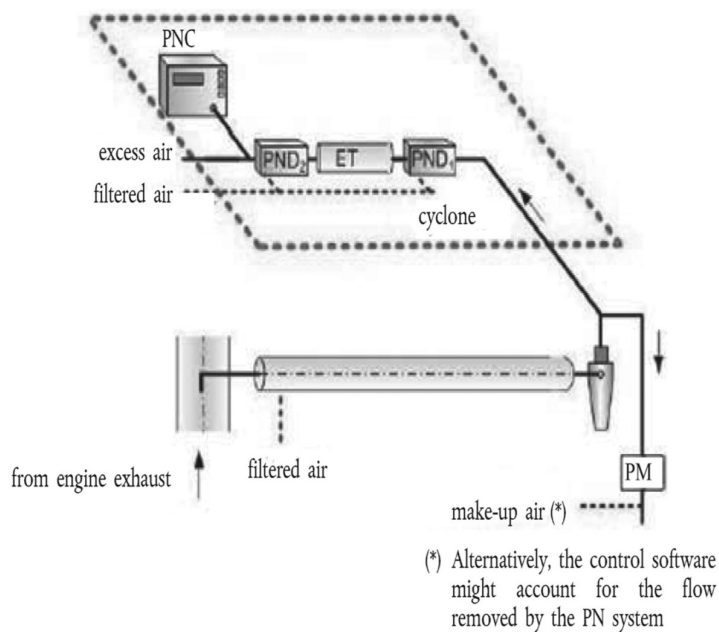


Figure 1

Schematic of Recommended Particle Sampling System – Partial Flow Sampling

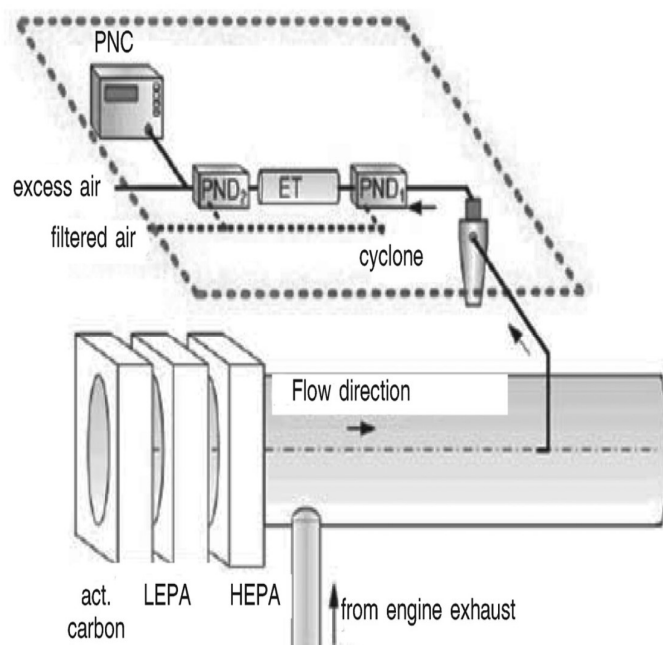


Figure 2

Schematic of Recommended Particle Sampling System – Full Flow Sampling

A.8.1.4.1 **Sampling System Description**

The particle sampling system shall consist of a sampling probe tip or particle sampling point in the dilution system, a particle transfer tube (PTT), a particle pre-classifier (PCF) and a volatile particle remover (VPR) upstream of the particle number concentration measurement (PNC) unit. The VPR shall include devices for sample dilution (particle number diluters: PND1 and PND2) and particle evaporation (Evaporation tube, ET). The sampling probe for the test gas flow shall be so arranged within the dilution tract that a representative sample gas flow is taken from a homogeneous air/exhaust mixture. The sum of the residence time of the system plus the T90 response time of the PNC shall be no greater than 20 s.

A8.1.4.2 **Particle Transfer System**

The sampling probe tip (PSP) and particle transfer tube (PTT) together comprise the particle transfer system (PTS). The PTS conducts the sample from the dilution tunnel to the entrance to the first particle number diluter. The PTS shall meet the following conditions:

In the case of full flow dilution systems and partial flow dilution systems of the fractional sampling type (as described in Appendix 2 of this Chapter, clause A.2.2.1) the sampling probe shall be installed near the tunnel centre line, 10 to 20 tunnel diameters downstream of the gas inlet, facing upstream into the tunnel gas flow with its axis at the tip parallel to that of the dilution tunnel. The sampling probe shall be positioned within the dilution tract so that the sample is taken from a homogeneous diluent/exhaust mixture.

In the case of partial flow dilution systems of the total sampling type (as described in Appendix 2 of this Chapter, clause A.2.2.1) the particle sampling point shall be located in the particulate transfer tube, upstream of the particulate filter holder, flow measurement device and any sample/bypass bifurcation point. The sampling point or sampling probe shall be positioned so that the sample is taken from a homogeneous diluent/exhaust mixture.

It shall have an internal diameter of ≥ 8 mm.

Sample gas drawn through the PTS shall meet the following conditions:

It shall have a flow Reynolds number (Re) of < 1700 ;

It shall have a residence time in the PTS of ≤ 3 seconds.

Any other sampling configuration for the PTS for which equivalent particle penetration for particles of 30 nm electrical mobility diameter can be demonstrated will be considered acceptable.

The outlet tube (OT) conducting the diluted sample from the

VPR to the inlet of the PNC shall have the following properties:

It shall have an internal diameter of ≥ 4 mm;

Sample Gas flow through the POT shall have a residence time of ≤ 0.8 seconds.

Any other sampling configuration for the OT for which equivalent particle penetration for particles of 30 nm electrical mobility diameter can be demonstrated will be considered acceptable.

A.8.1.4.3

Particle Pre-classifier

The recommended particle pre-classifier shall be located upstream of the VPR. The pre-classifier 50% cut point particle diameter shall be between 2.5 μm and 10 μm at the volumetric flow rate selected for sampling particle number emissions. The pre-classifier shall allow at least 99 % of the mass concentration of 1 μm particles entering the pre-classifier to pass through the exit of the pre-classifier at the volumetric flow rate selected for sampling particle number emissions. In the case of partial flow dilution systems, it is acceptable to use the same pre-classifier for particulate mass and particle number sampling, extracting the particle number sample from the dilution system downstream of the pre-classifier. Alternatively, separate pre-classifiers may be used, extracting the particle number sample from the dilution system upstream of the particulate mass pre-classifier

A.8.1.4.4

Volatile Particle Remover (VPR)

The VPR shall comprise one particle number diluter (PND_1), an evaporation tube and a second diluter (PND_2) in series. This dilution function is to reduce the number concentration of the sample entering the particle concentration measurement unit to less than the upper threshold of the single particle counts mode of the PNC and to suppress nucleation within the sample. The VPR shall provide an indication of whether or not PND_1 and the evaporation tube are at their correct operating temperatures.

The VPR shall achieve $> 99.0\%$ vaporization of 30 nm tetracontane ($\text{CH}_3(\text{CH}_2)_{38}\text{CH}_3$) particles, with an inlet concentration of $\geq 10,000 \text{ cm}^{-3}$, by means of heating and reduction of partial pressures of the tetracontane. It shall also achieve a particle concentration reduction factor (f_r) for particles of 30 nm and 50 nm electrical mobility diameters, that is no more than 30% and 20% respectively higher, and no more than 5% lower than that for particles of 100 nm electrical mobility diameter for the VPR as a whole.

A.8.1.4.4.1 First Particle Number Dilution Device (PND₁)

The first particle number dilution device shall be specifically designed to dilute particle number concentration and operate at a (wall) temperature of 150 °C – 400 °C. The wall temperature set point should be held at a constant nominal operating temperature, within this range, to a tolerance of ± 10 °C and not exceed the wall temperature of the ET (clause A.8.1.4.4.2). The diluter should be supplied with HEPA filtered dilution air and be capable of a dilution factor of 10 to 200 times.

A.8.1.4.4.2 Evaporation Tube

The entire length of the ET shall be controlled to a wall temperature greater than or equal to that of the first particle number dilution device and the wall temperature held at a fixed nominal operating temperature between 300 °C and 400 °C, to a tolerance of ± 10 °C.

A.8.1.4.4.3 Second Particle Number Dilution Device (PND₂)

PND₂ shall be specifically designed to dilute particle number concentration. The diluter shall be supplied with HEPA filtered dilution air and be capable of maintaining a single dilution factor within a range of 10 to 30 times. The dilution factor of PND₂ shall be selected in the range between 10 and 15 such that particle number concentration downstream of the second diluter is less than the upper threshold of the single particle counts mode of the PNC and the gas temperature prior to entry to the PNC is < 35 °C.

A.8.1.4.5 Particle Number Counter (PNC)

The PNC shall meet the requirements of clause A.8.1.3.4.

A.8.2 Calibration/Validation of the Particle Sampling System**A.8.2.1 Calibration of the Particle Number Counter**

A.8.2.1.1 The Test Agency shall ensure the existence of a calibration certificate for the PNC demonstrating compliance with a traceable standard within a 12 month period prior to the emissions test.

A.8.2.1.2 The PNC shall also be recalibrated and a new calibration certificate issued following any major maintenance.

A.8.2.1.3 Calibration shall be traceable to a standard calibration method:

- (a) By comparison of the response of the PNC under calibration with that of a calibrated aerosol electrometer when simultaneously sampling electrostatically classified calibration particles; or
- (b) By comparison of the response of the PNC under calibration with that of a second PNC which has been directly calibrated by the above method.

In the electrometer case, calibration shall be undertaken using at least six standard concentrations spaced as uniformly as possible across the PNC's measurement range. These points will include a nominal zero concentration point produced by attaching HEPA filters of at least class H13 of EN 1822:2008, or equivalent performance, to the inlet of each instrument. With no calibration factor applied to the PNC under calibration, measured concentrations shall be within $\pm 10\%$ of the standard concentration for each concentration used, with the exception of the zero point, otherwise the PNC under calibration shall be rejected. The gradient from a linear regression of the two data sets shall be calculated and recorded. A calibration factor equal to the reciprocal of the gradient shall be applied to the PNC under calibration. Linearity of response is calculated as the square of the Pearson product moment correlation coefficient (R^2) of the two data sets and shall be equal to or greater than 0.97. In calculating both the gradient and R^2 the linear regression shall be forced through the origin (zero concentration on both instruments).

In the reference PNC case, calibration shall be undertaken using at least six standard concentrations across the PNC's measurement range. At least three points shall be at concentrations below $1,000 \text{ cm}^{-3}$, the remaining concentrations shall be linearly spaced between $1,000 \text{ cm}^{-3}$ and the maximum of the PNC's range in single particle count mode. These points will include a nominal zero concentration point produced by attaching HEPA filters of at least class H13 of EN 1822:2008, or equivalent performance, to the inlet of each instrument. With no calibration factor applied to the PNC under calibration, measured concentrations shall be within $\pm 10\%$ of the standard concentration for each concentration, with the exception of the zero point, otherwise the PNC under calibration shall be rejected. The gradient from a linear regression of the two data sets shall be calculated and recorded. A calibration factor equal to the reciprocal of the gradient shall be applied to the PNC under calibration. Linearity of response is calculated as the square of the Pearson product moment correlation coefficient (R^2) of the two data sets and shall be equal to or greater than 0.97. In calculating both the gradient and R^2 the linear regression shall be forced through the origin. (zero concentration on both instruments).

- A.8.2.1.4 Calibration shall also include a check, against the requirements in clause A.8.1.3.4.8., on the PNC's detection efficiency with particles of 23 nm electrical mobility diameter. A check of the counting efficiency with 41 nm particles is not required.

A.8.2.2 Calibration/Validation of the Volatile Particle Remover

- A.8.2.2.1 Calibration of the VPR's particle concentration reduction factors across its full range of dilution settings, at the instrument's fixed nominal operating temperatures, shall be required when the unit is new and following any major maintenance. The periodic validation requirement for the VPR's particle concentration reduction factor is limited to a check at a single setting, typical of that used for measurement on diesel particulate filter equipped vehicles. The Test Agency shall ensure the existence of a calibration or validation certificate for the volatile particle remover within a 6 month period prior to the emissions test. If the volatile particle remover incorporates temperature conformity alarms a 12 month validation interval shall be permissible.

The VPR shall be characterized for particle concentration reduction factor with solid particles of 30 nm, 50 nm and 100 nm electrical mobility diameter. Particle concentration reduction factors ($f_r(d)$) for particles of 30 nm and 50 nm electrical mobility diameters shall be no more than 30% and 20% higher respectively, and no more than 5% lower than that for particles of 100 nm electrical mobility diameter. For the purposes of validation, the mean particle concentration reduction factor shall be within $\pm 10\%$ of the mean particle concentration reduction factor (\bar{f}_r) determined during the primary calibration of the VPR.

- A.8.2.2.2 The test aerosol for these measurements shall be solid particles of 30, 50 and 100 nm electrical mobility diameter and a Minimum concentration of 5,000 cm⁻³ particles at the VPR inlet. Particle concentrations shall be measured upstream and downstream of the components.

The particle concentration reduction factor at each particle size ($f_r(d_i)$) shall be calculated as follows:

$$f_r(d_i) = \frac{N_{in}(d_i)}{N_{out}(d_i)} \quad (117)$$

Where:

$N_{in}(d_i)$ = upstream particulate number concentration for particulates of diameter d_i ;

$N_{out}(d_i)$ = downstream particulate number concentration for particulates of diameter d_i ; and

d_i = particulate electrical mobility diameter (30, 50 or 207/460

100 nm).

$N_{in}(di)$ and $N_{out}(di)$ shall be corrected to the same conditions.

The mean particle concentration reduction ($\overline{f_r}$) at a given dilution setting shall be calculated as follows:

$$\overline{f_r} = \frac{f_r(30nm) + f_r(50nm) + f_r(100nm)}{3} \quad (118)$$

It is recommended that the VPR is calibrated and validated as a complete unit

- A.8.2.2.3 The Test Agency shall ensure the existence of a validation certificate for the VPR demonstrating effective volatile particle removal efficiency within a 6month period prior to the emissions test. If the volatile particle remover incorporates temperature conformity alarms a 12 month validation interval shall be permissible. The VPR shall demonstrate greater than 99.0% removal of tetracontane ($CH_3(CH_2)_{38}CH_3$) particles of at least 30 nm electrical mobility diameter with an inlet concentration of $\geq 10,000 \text{ cm}^{-3}$ when operated at its minimum dilution setting and manufacturers recommended operating temperature.

A.8.2.3 Particle Number System Check Procedures

- A.8.2.3.1 Prior to each test, the particle counter shall report a measured concentration of less than $0.5 \text{ particles cm}^{-3}$ when a HEPA filter of at least class H13 of EN 1822:2008, or equivalent performance, is attached to the inlet of the entire particle sampling system (VPR and PNC).
- A.8.2.3.2 On a monthly basis, the flow into the particle counter shall report a measured value within 5% of the particle counter nominal flow rate when checked with a calibrated flow meter.
- A.8.2.3.3 Each day, following the application of a HEPA filter of at least class H13 of EN 1822:2008, or equivalent performance, to the inlet of the particle counter, the particle counter shall report a concentration of $\leq 0.2 \text{ cm}^{-3}$. Upon removal of this filter, the particle counter shall show an increase in measured concentration to at least $100 \text{ particles cm}^{-3}$ when challenged with ambient air and a return to $\leq 0.2 \text{ cm}^{-3}$ on replacement of the HEPA filter.
- A.8.2.3.4 Prior to the start of each test, it shall be confirmed that the measurement system indicates that the evaporation tube, where featured in the system, has reached its correct operating temperature.
- 2.3.5 Prior to the start of each test, it shall be confirmed that the measurement system indicates that the diluter PND_1 has reached its correct operating temperature.

CHAPTER 4

TECHNICAL SPECIFICATION OF REFERENCE FUELS

As per Gazette Notification G.S.R. 889(E) dated 16th September 2016 published by Ministry of Road Transport and Highways under CMVR)

4.1 Technical Specification of Reference Hydrogen Fuel.

Characteristics	Units	Limits		Test Method
		Minimum	Maximum	
Hydrogen Purity	% mole	98	100	ISO 14687-1
Total Hydrocarbon	μmol/mol	0	100	ISO 14687-1
Water ⁽¹⁾	μmol/mol	0	2	ISO 14687-1
Oxygen	μmol/mol	0	2	ISO 14687-1
Argon	μmol/mol	0	2	ISO 14687-1
Nitrogen	μmol/mol	0	2	ISO 14687-1
CO	μmol/mol	0	1	ISO 14687-1
Sulphur	μmol/mol	0	2	ISO 14687-1
Permanent Particulates ⁽³⁾				ISO 14687-1

⁽¹⁾ Not to be condensed

⁽²⁾ Combined water, oxygen, nitrogen, argon: 1.900 μmol/mol.

⁽³⁾ The hydrogen shall not contain dust, sand, dirt, gums, oils or other substances in an amount sufficient to damage the fuelling station equipment of the vehicle (engine) being fuelled.

4.2 Specification of Commercial Gasoline Fuel

Characteristics	Unit	Requirements	
		Regular	Premium
Color, visual		Orange	Red
Density @ 15°C	Kg/m ³	720-775	720-775
Distillation:			
a) Recovery up to 70 °C (E 70)	% volume	10-55 (summer) 10-58 (other months)	10-55 (summer) 10-58 (other months)
b) Recovery up to 100 °C (E 100)	% volume	40-70	40-70

c) Recovery up to 150 °C (E 150)	% volume	75 min	75 min
d) Final Boiling Point (FBP), max	°C	210	210
e) Residue, max	% volume	2	2
Research Octane Number (RON) min		91	95
Motor Octane Number (MON), min		85	85
Gum content (solvent washed), max	mg/100ml	4	4
Oxidation Stability, min	minutes	360	360
Sulphur, total, max	mg/kg	10	10
Lead content (as Pb), max	g/l	0.005	0.005
Reid Vapour Pressure (RVP) @ 38°C, max	kPa	67	67
Vapour Lock Index (VLI)			
a) Summer, max		1050	1050
b) Other months, max		1100	1100
Benzene Content, max	% volume	1	1
Copper strip corrosion for 3 hrs @ 50°C, max	Rating	Class 1	Class 1
Olefin content, max	% volume	21	18
Aromatics content, max	% volume	35	35
Oxygen content, max	% mass	3.7	4.5
Oxygenates Content			
a) Methanol, max	% volume	3	3
b) Ethanol, max	% volume	10	10
c) Iso-propyl alcohol, max	% volume	10	10
d) Iso-Butyl alcohol, max	% volume	10	10
e) Tertiary-butyl alcohol, max	% volume	7	7
f) Ethers containing 5 or more carbon atoms per molecule, max	% volume	15	15
g) Other oxygenates, max	% volume	8	8
<p>Note :</p> <ol style="list-style-type: none"> 1. Test methods and other provisions and details along with the requirements as given above shall be issued by Bureau of Indian Standards. 2. The aromatic content, (max) shall be permitted upto 40% in North Eastern States till 01.04.2023 			

4.3 Specification of Commercial Diesel Fuel

Characteristics	Unit	Requirements
Ash, max	% mass	0.01
Carbon Residue (Ramsbottom) on 10 % residue, max	% mass	0.3 without additives
Cetane number (CN), min		51
Cetane Index (CI), min		46
Distillation :		
95% vol. recovery at $^{\circ}\text{C}$, max	$^{\circ}\text{C}$	360
Flash point :		
a) Abel, min	$^{\circ}\text{C}$	35
Kinematic Viscosity @ 40°C	Cst	2.0-4.5
Density @ 15°C , max	kg/m^3	845
Total Sulphur, max.	mg/kg	10
Water content, max	mg/kg	200
Cold filter Plugging point (CFPP)		
a) Summer, max	$^{\circ}\text{C}$	18
b) Winter, max	$^{\circ}\text{C}$	6
Total contaminations, max	mg/kg	24
Oxidation stability, max	g/m^3	25
Polycyclic Aromatic Hydrocarbon (PAH), max	% mass	8
Lubricity, corrected wear scar diameter @ 60°C , max	μm (microns)	460
Copper strip corrosion for 3 hrs @ 50°C	Rating	Class – 1
FAME Content, max	% v/v	7.0
Note: 1. Test methods and other provisions / details along with the requirements as given above shall be issued by Bureau of Indian Standards. 2. The Cetane number (CN), (min) shall be permitted upto 48 in North Eastern States till 01.04.2023		

4.4 Technical specifications of the Reference Fuel (E5)

Parameter	Unit	Limits ¹		Test method
		Minimum	Maximum	
Research octane number, RON ²		95.0	-	EN25164 / prEN ISO 5164
Motor octane number, MON ²		85.0	-	EN25163 /prEN ISO 5163
Density at 15 °C	kg/m ³	743.0	756.0	ENISO3675/EN ISO 12185
Vapour pressure (DVPE)	kPa	56.0	60.0	EN ISO13016-1(DVPE)
Water content	% m/m		0.015	ASTME 1064
Distillation:				
– evaporated at 70 °C	% v/v	24.0	44.0	EN ISO 3405
– evaporated at 100 °C	% v/v	48.0	60.0	EN ISO 3405
– evaporated at 150 °C	% v/v	82.0	94.0	EN ISO 3405
– final boiling point	°C	190	210	EN ISO 3405
Residue	% v/v	—	2.0	ENISO 3405
Hydrocarbon analysis:				
– Olefins	% v/v	3.0	13.0	ASTMD 1319
– Aromatics	% v/v	29.0	35.0	ASTMD 1319
– Benzene	% v/v	-	1.00	EN 12177
– saturates	% v/v	Report		ASTM1319
Carbon/hydrogen ratio		Report		
Carbon/oxygen ratio		Report		
Induction period ²	minutes	480	—	EN ISO 7536
Oxygen content ⁴	% m/m	3.3	3.7	EN 1601
Solvent washed gum (Existent gum content)	mg/ml	—	0.04	EN ISO 6246
Sulphur content ³	mg/kg	—	10	EN ISO 20846 / EN ISO 20884
Copper corrosion 3hrs, 50 °C		—	Class 1	EN ISO 2160
Lead content	mg/l	—	5	EN 237
Phosphorus content ⁵	mg/l	—	1.3	ASTM D 3231
Ethanol ⁴	% v/v	4.7	5.3	EN 10601/EN13132

Notes:

- 1 The values quoted in the specifications are 'true values'. In establishment of their limit values the terms of ISO 4259:2006 Petroleum products - Determination and application of precision data in relation to methods of test have been applied and in fixing a minimum value, a minimum difference of 2R above zero has been taken into account; in fixing a maximum and minimum value, the minimum difference is 4R (R = reproducibility).

Notwithstanding this measure, which is necessary for technical reasons, the manufacturer of fuels shall nevertheless aim at a zero value where the stipulated maximum value is 2R and at the mean value in the case of quotations of maximum and minimum limits. Should it be necessary to clarify whether a fuel meets the requirements of the specifications, the terms of ISO 4259 shall be applied.

- 2 The fuel may contain oxidation inhibitors and metal deactivators normally used to stabilize refinery petrol streams, but detergent/dispersive additives and solvent oils shall not be added.
- 3 The actual sulphur content of the fuel used for the type I test shall be reported.
- 4 Ethanol meeting the specification of prEN15376 is the only oxygenate that shall be intentionally added to the reference fuel.
- 5 There shall be no intentional addition to this reference fuel of compounds containing phosphorus, iron, manganese or lead.

4.5 Technical specifications of the reference Diesel Fuel (B7)

Parameter	Unit	Limits ¹		Test method
		Minimum	Maximum	
Cetane Index		46.0		EN ISO 4264
Cetane number ²		52.0	56.0	EN ISO 5165
Density at 15 °C	kg/m ³	833.0	837.0	EN ISO 12185
Distillation:				
- 50% point	°C	245.0	—	EN ISO 3405
- 95% point	°C	345.0	360.0	EN ISO 3405
- final boiling point	°C	—	370.0	EN ISO 3405
Flash point	°C	55	—	EN ISO 2719
Cloud point	°C	-	-10	EN 23015
Viscosity at 40 °C	mm ² /s	2.30	3.30	EN ISO 3104
Polycyclic aromatic hydrocarbons	% m/m	2.0	4.0	EN 12916
Sulphur content	mg/kg	—	10.0	EN ISO 20846 EN ISO 20884
Copper corrosion 3hrs, 50 °C		—	Class 1	EN ISO 2160
Conradson carbon residue (10 % DR)	% m/m	—	0.20	EN ISO 10370
Ash content	% m/m	—	0.010	EN ISO 6245
Total contamination	mg/kg	-	24	EN 12662
Water content	mg/kg	—	200	EN ISO 12937
Acid number	mg KOH/g	—	0.10	EN ISO 6618
Lubricity (HFRR wear scan diameter at 60 °C)	µm	—	400	EN ISO 12156
Oxidation stability @ 110 °C ³	h	20.0		EN 15751
FAME ⁴	% v/v	6.0	7.0	EN 14 78

Notes:

- 1 The values quoted in the specifications are 'true values'. In establishment of their limit values the terms of ISO 4259 Petroleum products – Determination and application of precision data in relation to methods of test have been applied and in fixing a minimum value, a minimum difference of 2R above zero has been taken into account; in fixing a maximum and minimum value, the minimum difference is 4R (R = reproducibility). Notwithstanding this measure, which is necessary for technical reasons, the manufacturer of fuels shall nevertheless aim at a zero value where the stipulated maximum value is 2R and at the mean value in the case of quotations of maximum and minimum limits. Should it be necessary to clarify whether a fuel meets the requirements of the specifications, the terms of ISO 4259 shall be applied.
- 2 The range for cetane number is not in accordance with the requirements of a minimum range of 4R. However, in the case of a dispute between fuel supplier and fuel user, the terms of ISO 4259 may be used to resolve such disputes provided replicate measurements, of sufficient number to archive the necessary precision, are made in preference to single determinations.
- 3 Even though oxidation stability is controlled, it is likely that shelf life will be limited. Advice shall be sought from the supplier as to storage conditions and life.
- 4 FAME content to meet the specification of EN 14214.

CHAPTER 5

EMISSIONS DATA REQUIRED AT TYPE-APPROVAL FOR ROADWORTHINESS PURPOSES

Measuring Carbon Monoxide Emissions at Idling Speeds

1.0 INTRODUCTION

1.1 This Chapter sets out the procedure for measuring gaseous pollutants emissions at idling speeds (normal and high) for positive-ignition engines installed in vehicles.

1.2 This Chapter does not apply to dual-fuel engines and vehicles.

2.0 GENERAL PROVISIONS

2.1 Emission data required for roadworthiness testing

2.1.1 This requirement applies to all vehicles powered by a positive ignition engine for which type approval is sought in accordance with this Part.

2.1.2 When tested in accordance with clause 3 of this Chapter at normal idling speed:

- (a) The carbon monoxide content by volume of the exhaust gases emitted shall be recorded; and
- (b) The engine speed during the test shall be recorded, including any tolerances.

2.1.3 When tested at "high idle" speed (i. e. $> 2,000 \text{ min}^{-1}$)

- (a) The carbon monoxide content by volume of the exhaust gases emitted shall be recorded;
- (b) The Lambda value shall be recorded; and the manufacturer shall confirm the accuracy of the recorded Lambda value as representative of typical production vehicles within 24 months of date of granting of type approval. An assessment shall be made on the basis of surveys and studies of production vehicles.
- (c) The engine speed during the test shall be recorded, including any tolerances.

The Lambda value shall be calculated using the simplified Brettschneider equation as follows:

Where:

$$\frac{[\text{CO}_2] + \frac{[\text{CO}]}{2} + [\text{O}_2] + \left(\frac{\text{Hcv}}{4} \cdot \frac{3.5}{3.5 + \frac{[\text{CO}]}{[\text{CO}_2]}} - \frac{\text{Ocv}}{2} \right) \cdot ([\text{CO}_2] + [\text{CO}])}{\left(1 + \frac{\text{Hcv}}{4} - \frac{\text{Ocv}}{2} \right) \cdot ([\text{CO}_2] + [\text{CO}] + \text{K1}[\text{HC}])}$$

[] = concentration in per cent volume,

K1 = conversion factor for Non-Dispersive Infrared (NDIR) measurement to Flame Ionisation Detector (FID) measurement (provided by manufacturer of measuring equipment),

Hcv = Atomic ratio of hydrogen to carbon:

- (a) for petrol (E5) 1.89;
- (b) for petrol (E10) 1.93;
- (c) for LPG 2.525;
- (d) for NG/biomethane 4.0;
- (e) for ethanol (E85) 2.74;
- (f) for ethanol (E75) 2.61.

Ocv = Atomic ratio of oxygen to carbon:

- (a) for petrol (E5) 0.016;
- (b) for petrol (E10) 0.032;
- (c) for LPG 0.0;
- (d) for NG/biomethane 0.0;
- (e) for ethanol (E85) 0.39;
- (f) for ethanol (E75) 0.329.

- 2.1.4 The engine oil temperature at the time of the test shall be measured and recorded.

3.0 TECHNICAL REQUIREMENTS

Conditions of measurement

- 3.1 The fuel shall be the reference fuel, specifications for which are given in Chapter 4 of this Part.
- 3.2 The engine shall be warmed up until all temperatures of cooling and lubrication means and the pressure of lubrication means have reached equilibrium.

3.2.1 Vehicles that are fuelled either with petrol or with LPG or NG / biomethane shall be tested with the reference fuel(s) used as specified in Chapter 4 of this Part.

3.3 In the case of vehicles with manually-operated or semi-automatic-shift gearboxes, the test shall be carried out with the gear lever in the "neutral" position and with the clutch engaged.

3.4 In the case of vehicles with automatic-shift gearboxes, the test shall be carried out with the gear selector in either the "neutral" or the "parking" position.

3.5 Components for adjusting the idling speed

3.5.1 Definition

For the purposes of this Part, "*components for adjusting the idling speed*" means controls for changing the idling conditions of the engine which may be easily operated by a mechanic using only the tools described in clause 3.5.1.1. of this Chapter. In particular, devices for calibrating fuel and air flows are not considered as adjustment components if their setting requires the removal of the set-stops, an operation which cannot normally be performed except by a professional mechanic

3.5.1.1 Tools which may be used to control components for adjusting the idling speed: screwdrivers (ordinary or cross-headed), spanners (ring, open-end or adjustable), pliers, allen keys.

3.5.2 Determination of measurement points

3.5.2.1 A measurement at the setting in accordance with the conditions fixed by the manufacturer is performed first;

3.5.2.2 For each adjustment component with a continuous variation, a sufficient number of characteristic positions shall be determined.

3.5.2.3 The measurement of the gaseous pollutants of exhaust gases described in Gazette Notification shall be carried out for all the possible positions of the adjustment components, but for components with a continuous variation only the positions defined in clause 3.5.2.2. of this Chapter shall be adopted

3.5.2.4 This test shall be considered satisfactory if one or both of the two following conditions is met:

None of the values measured in accordance with clause 3.5.2.3. of this Chapter exceed the limit values as specified in CMV Rule 115(2)(i);

The maximum content obtained by continuously varying one of the adjustment components while the other components are kept stable does not exceed the limit value, this condition being met for the various combinations of adjustment components other than the one which was varied continuously

- 3.5.2.5 The possible positions of the adjustment components shall be limited:
- On the one hand, by the larger of the following two values: the lowest idling speed which the engine can reach; the speed recommended by the manufacturer, minus 100 revolutions per minute;
- On the other hand, by the smallest of the following three values:
- The highest speed the engine can attain by activation of the idling speed components;
- The speed recommended by the manufacturer, plus 250 revolutions per minute;
- The cut-in speed of automatic clutches

- 3.5.2.6 In addition, settings incompatible with correct running of the engine shall not be adopted as measurement settings. In particular, when the engine is equipped with several carburetors all the carburetors shall have the same setting

4.0 SAMPLING OF GASES

- 4.1 The sampling probe shall be inserted into the exhaust pipe to a depth of at least 300 mm into the pipe connecting the exhaust with the sampling bag and as close as possible to the exhaust.
- 4.2 The concentration in CO (C_{CO}) and CO₂ (C_{CO2}) shall be determined from the measuring instrument readings or recordings, by use of appropriate calibration curves.
- 4.3 The corrected concentration for carbon monoxide regarding four-stroke engines is:

$$C_{CO \text{ corr}} = C_{CO} \frac{15}{C_{CO} + C_{CO2}}$$

- 4.4 The concentration in C_{CO} (see clause 4.2. of this Chapter) measured according to the formulae contained in clause 4.3. of this Chapter need not be corrected if the total of the concentrations measured ($C_{CO} + C_{CO2}$) is for four-stroke engines at least:
- (a) For gasoline 15%
 - (b) For LPG 13.5%
 - (c) For NG/biomethane 11.5%

CHAPTER 6**VERIFYING THE DURABILITY OF ENGINE SYSTEMS****1.0 INTRODUCTION**

1.1 This Chapter sets out the procedures for selecting engines to be tested over a service accumulation schedule for the purpose of determining deterioration factors. The deterioration factors shall be applied in accordance with the requirements of clause 3.6 of this Chapter to the emissions measured according to Chapter 3 of this Part.

1.2 This Chapter also sets out the emission and non-emission-related maintenance carried out on engines undergoing a service accumulation schedule. Such maintenance shall conform to the maintenance performed on in-service engines and shall be communicated to owners of new engines and vehicles.

2.0 SELECTION OF ENGINES FOR ESTABLISHING USEFUL LIFE DETERIORATION FACTORS

2.1 Engines shall be selected from the engine family defined in accordance with clause 7 of Chapter 1 of this Part for emission testing in order to establish useful life deterioration factors.

2.2 Engines from different engine families may be further combined into families based on the type of exhaust after-treatment system utilized. In order to place engines with different numbers of cylinders and different cylinder configuration but having the same technical specifications and installation for the exhaust after- treatment systems into the same engine-after treatment system family, the manufacturer shall provide data to the Test Agency that demonstrates that the emissions reduction performance of such engine systems is similar.

2.3 One engine representing the engine-after treatment system family as determined in accordance with clause 2.2, shall be selected by the engine manufacturer for testing over the service accumulation schedule defined in clause 3.2 of this Chapter, and shall be reported to the Test Agency before any testing commences.

2.3.1 If the Test Agency decides that the worst-case emissions of the engine-after treatment system family can be characterized better by another engine, then the Test Agency and the engine manufacturer shall select the test engine jointly.

3.0 ESTABLISHING USEFUL LIFE DETERIORATION FACTORS**3.1 General**

Deterioration factors applicable to an engine-after treatment system family are developed from the selected engines based on a service accumulation schedule that includes periodic testing for gaseous and particulate emissions over the WHTC and WHSC tests.

3.2 Service accumulation schedule

Service accumulation schedules may be carried out at the choice of the manufacturer by running a vehicle equipped with the selected engine over an in-service accumulation schedule or by running the selected engine over a dynamometer service accumulation schedule.

3.2.1 In-service and dynamometer service accumulation

3.2.1.1. The manufacturer shall determine the form and extent of the distance, the service accumulation and the ageing cycle for engines, consistent with good engineering practice.

3.2.1.2. The manufacturer shall determine the test points where gaseous and particulate emissions will be measured over the hot WHTC and WHSC tests. The minimum number of test points shall be three, one at the beginning, one approximately in the middle and one at the end of the service accumulation schedule.

3.2.1.3. The emission values at the start point and at the useful life end point calculated in accordance with clause 3.5.2 of this Chapter shall meet the limit values specified in the clause 5.3 of Chapter 1 of this Part but individual emission results from the test points may exceed those limit values.

3.2.1.4. At the request of the manufacturer and with the agreement of the Test Agency, only one test cycle (either the hot WHTC or WHSC test) needs to be run at each test point, with the other test cycle run only at the beginning and at the end of the service accumulation schedule.

3.2.1.5. Service accumulation schedules may be different for different engine-after treatment system families.

3.2.1.6. Service accumulation schedules may be shorter than the useful life period, but shall not be shorter than shown in the Table 1 in clause 3.2.1.8.

3.2.1.7. For engine dynamometer service accumulation, the manufacturer shall provide the applicable correlation between the service accumulation period (driving distance) and engine dynamometer hours, for example, fuel consumption correlation, vehicle speed versus engine revolutions correlation, etc.

3.2.1.8 Minimum service accumulation period

Table 1		
Minimum Service Accumulation Period		
Category of vehicle in which engine will be installed	Minimum service accumulation period	Useful life
Category N1 vehicles	160,000 km	
Category N2 vehicles	188,000km	

Category N3 vehicles with a maximum technically permissible mass not exceeding 16 tonnes	188,000 km	Useful life (As mentioned in Chapter 1 of this Part)
Category N3 vehicles with a maximum technically permissible mass exceeding 16 tonnes	233,000 km	
Category M1 vehicles	160,000 km	
Category M2 vehicles	160,000 km	
Category M3 vehicles with a maximum technically permissible mass not exceeding 7.5 tonnes	188,000 km	
Category M3 vehicles exceeding 7.5 tonnes	233,000 km	

- 3.2.1.9. Accelerated ageing is permitted by adjusting the service accumulation schedule on a fuel consumption basis. The adjustment shall be based on the ratio between the typical in-use fuel consumption and the fuel consumption on the ageing cycle, but the fuel consumption on the ageing cycle shall not exceed the typical in-use fuel consumption by more than 30 %.
- 3.2.1.10 The service accumulation schedule shall be fully described in the application for type-approval and reported to the Test Agency before the start of any testing.
- 3.2.2. If the Test Agency decides that additional measurements need to be carried out on the hot WHTC and WHSC tests between the points selected by the manufacturer it shall notify the manufacturer. The revised service accumulation schedule shall be prepared by the manufacturer and agreed by the Test Agency

3.3 Engine Testing

3.3.1 Engine system stabilization

- 3.3.1.1 For each engine-after treatment system family, the manufacturer shall determine the number of hours of vehicle or engine running after which the operation of the engine-after treatment system has stabilised. If requested by the Test Agency the manufacturer shall make available, the data and analysis used to make this determination. As an alternative, the manufacturer may elect to run the engine between 60 and 125 hours or the equivalent mileage on the ageing cycle to stabilise the engine-after treatment system.

- 3.3.1.2. The end of the stabilization period determined in clause 3.3.1.1 will be deemed the start of the service accumulation schedule.

3.3.2 Service accumulation period

- 3.3.2.1 After stabilization, the engine shall be run over the service accumulation schedule selected by the manufacturer, as described in clause 3.2 of this Chapter. At the periodic intervals in the service accumulation schedule determined by the manufacturer, and, where appropriate stipulated by the Test Agency according to clause 3.2.2 of this Chapter the engine shall be tested for gaseous and particulate emissions over the hot WHTC and WHSC tests. In accordance with clause 3.2.1.4 of this Chapter, if it has been agreed that only one test cycle (hot WHTC or WHSC) be run at each test point, the other test cycle (hot WHTC or WHSC) shall be run at the beginning and end of the service accumulation schedule.
- 3.3.2.2 During the service accumulation schedule, maintenance shall be carried out on the engine according to the requirements of clause 4 of this Chapter.
- 3.3.2.3 During the service accumulation schedule, unscheduled maintenance on the engine or vehicle may be performed, for example if the OBD system has specifically detected a problem that has resulted in the malfunction indicator (hereinafter 'MI') being activated.
- 3.3.2.4 The use of market fuels is allowed for conducting the service accumulation schedule. A reference fuel shall be used to carry out the emission test.

3.4 Reporting

- 3.4.1 The results of all emission tests (hot WHTC and WHSC) conducted during the service accumulation schedule shall be made available to the Test Agency. If any emission test is declared to be void, the manufacturer shall provide an explanation of why the test has been declared void. In such a case, another series of emission tests over the hot WHTC and WHSC tests shall be carried out within the following 100 hours of service accumulation.
- 3.4.2 The manufacturer shall retain records of all information concerning all the emission tests and maintenance carried out on the engine during the service accumulation schedule. This information shall be submitted to the Test Agency along with the results of the emission tests conducted over the service accumulation schedule.

3.5 Determination of Deterioration Factor

- 3.5.1. For each pollutant measured on the hot WHTC and WHSC tests at each test point during the service accumulation schedule, a 'best fit' linear regression analysis shall be made on the basis of all test results. The results of each test for each pollutant shall be expressed to the same number of decimal places as the limit value for that pollutant, as shown in the clause 5.3 of Chapter 1 of this Part, plus one additional decimal place. In accordance with clause 3.2.1.4 of this Chapter, if it has been agreed that only one test cycle (hot WHTC or WHSC) be run at each

test point and the other test cycle (hot WHTC or WHSC) run only at the beginning and at the end of the service accumulation schedule, the regression analysis shall be made only on the basis of the test results from the test cycle run at each test point.

At the request of the manufacturer and with the prior approval of the Test Agency a non-linear regression shall be permitted.

- 3.5.2. The emission values for each pollutant at the start of the service accumulation schedule and at the useful life end point that is applicable for the engine under test shall be calculated from the regression equation. If the service accumulation schedule is shorter than the useful life period, the emission values at the useful life end shall be determined by extrapolation of the regression equation as determined in clause 3.5.1.

- 3.5.3 The deterioration factor for each pollutant is defined as the ratio of the applied emission values at the useful life end point and at the start of the service accumulation schedule (multiplicative deterioration factor).

At the request of the manufacturer and with the prior approval of the Test Agency, an additive deterioration factor for each pollutant may be applied. The additive deterioration factor shall be considered as the difference between the calculated emission values at the useful life end point and at the start of the service accumulation schedule.

If the calculation results in a value of less than 1.00 for a multiplicative DF, or less than 0,00 for an additive DF, then the deterioration factor shall be 1,0 or 0,00, respectively.

An example for determination of deterioration factors by using linear regression is shown in Figure 1 below.

Mixing of multiplicative and additive deterioration factors within one set of pollutants shall not be permitted.

In accordance with clause 3.2.1.4 of this Chapter, if it has been agreed that only one test cycle (hot WHTC or WHSC) be run at each test point and the other test cycle (hot WHTC or WHSC) run only at the beginning and end of the service accumulation schedule, the deterioration factor calculated for the test cycle that has been run at each test point shall be applicable also for the other test cycle

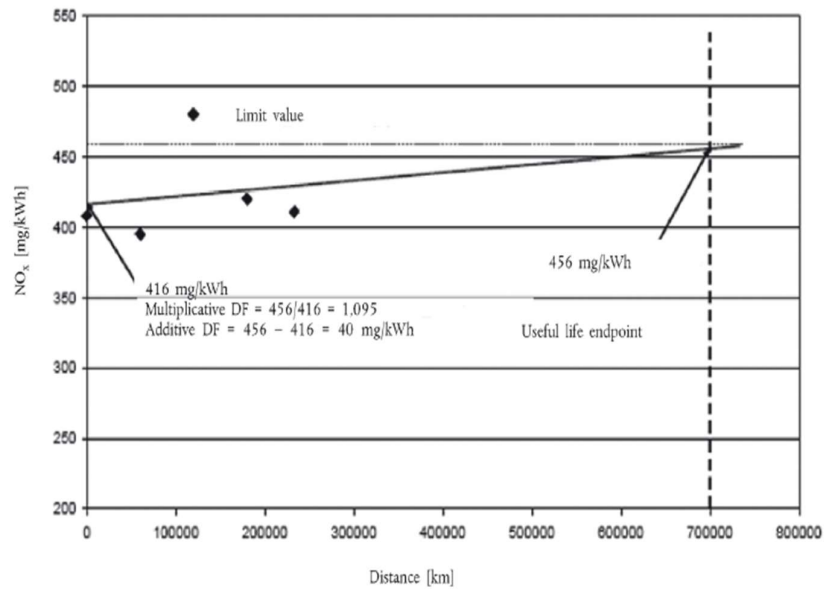


Figure 1

Example of Deterioration Factor Determination

3.6 Assigned Deterioration Factor

- 3.6.1 As an alternative to using a service accumulation schedule to determine deterioration factors, engine manufacturers may choose to use the following assigned multiplicative deterioration factors:

Table 2 Deterioration Factor								
Test cycle	CO	THC ¹	NMHC ²	CH ₄ ²	NOx	NH ₃	PM Mass	PM Number
WHTC	1.3	1.3	1.4	1.4	1.15	1.0	1.05	1.0
WHSC	1.3	1.3	1.4	1.4	1.15	1.0	1.05	1.0
Notes:								
1. Applies in case of a compression-ignition engine.								
2. Applies in case of a positive-ignition engine.								
Assigned additive deterioration factors are not given. It shall not be permitted to transform the assigned multiplicative deterioration factors into additive deterioration factors.								

3.7 Application of Deterioration Factor

- 3.7.1. The engines shall meet the respective emission limits for each pollutant, as given in the clause 5.3 of Chapter 1 of this Part, after application of the deterioration factors to the test result as measured in accordance with Chapter 3 (e_{gas} , e_{PM}) of this Part. Depending on the type of deterioration factor (DF), the following provisions shall apply:

- (a) Multiplicative: $(e_{\text{gas}} \text{ or } e_{\text{PM}}) \times \text{DF} \leq \text{emission limit}$
- (b) Additive: $(e_{\text{gas}} \text{ or } e_{\text{PM}}) + \text{DF} \leq \text{emission limit}$

- 3.7.2 The manufacturer may choose to carry across the DFs determined for an engine after treatment system family to an engine system that does not fall into the same engine-after treatment system family. In such cases, the manufacturer shall demonstrate to the Test Agency that the engine system for which the after treatment system family was originally tested and the engine system for which the DFs are being carried across have the same technical specifications and installation requirements on the vehicle and that the emissions of such engine or engine system are similar
- 3.7.3 The deterioration factors for each pollutant on the appropriate test cycle shall be recorded.

3.8 Checking of conformity of production

- 3.8.1. Conformity of production for emissions compliance shall be checked on the basis of the requirements of clause 8 of Chapter 1 of this Part.
- 3.8.2. The manufacturer may choose to measure the pollutant emissions before any exhaust after-treatment system at the same time as the type-approval test is being performed. In doing so, the manufacturer may develop an informal deterioration factor separately for the engine and the after treatment system that may be used by the manufacturer as an aid to end of production line auditing.
- 3.8.3. For the purposes of type-approval, only the deterioration factors according to clauses 3.5 or 3.6 of this Chapter shall be recorded.

4.0 MAINTENANCE

For the purpose of the service accumulation schedule, maintenance shall be performed in accordance with the manufacturer's manual for service and maintenance.

4.1 Emission-related scheduled maintenance

- 4.1.1 Emission-related scheduled maintenance for purposes of conducting a service accumulation schedule shall occur at the same distance or equivalent intervals to those that will be specified in the manufacturer's maintenance instructions to the owner of the engine or vehicle. This maintenance schedule may be updated as necessary throughout the service accumulation schedule provided that no maintenance operation is deleted from the maintenance schedule after the operation has been performed on the test engine.
- 4.1.2 The engine manufacturer shall specify for the service accumulation schedule the adjustment, cleaning and maintenance (where necessary) and scheduled exchange of the following items:
- (a) filters and coolers in the exhaust gas recirculation system;
 - (b) positive crankcase ventilation valve, if applicable;
 - (c) fuel injector tips (cleaning only);
 - (d) fuel injectors;
 - (e) turbocharger;

- (f) electronic engine control unit and its associated sensors and actuators;
- (g) particulate after treatment system (including related components);
- (h) deNOx system;
- (i) exhaust gas recirculation system, including all related control valves and tubing;
- (j) any other exhaust after-treatment system.

4.1.3 Critical emission-related scheduled maintenance shall only be performed if being performed in-use and being communicated to the owner of the vehicle.

4.2 Changes to scheduled maintenance

4.2.1 The manufacturer shall submit a request to the Test Agency for approval of any new scheduled maintenance that it wishes to perform during the service accumulation schedule and subsequently recommend to owners of engines or vehicles. The request shall be accompanied by data supporting the need for the new scheduled maintenance and the maintenance interval

4.3 Non emission related scheduled maintenance

4.3.1 Non-emission-related scheduled maintenance which is reasonable and technically necessary such as oil change, oil filter change, fuel filter change, air filter change, cooling system maintenance, idle speed adjustment, governor, engine bolt torque, valve lash, injector lash, timing, adjustment of the tension of any drive-belt, etc., may be performed on engines or vehicles selected for the service accumulation schedule at the least frequent intervals recommended by the manufacturer to the owner.

4.4 Repair

4.4.1 Repairs to the components of an engine selected for testing over a service accumulation schedule other than the engine emission control system or fuel system shall be performed only as a result of component failure or engine system malfunction.

4.4.2 If the engine itself, the emission control system or the fuel system fail during the service accumulation schedule, the service accumulation shall be considered void, and a new service accumulation shall be started with a new engine system.

CHAPTER 7

CONFORMITY OF IN-SERVICE ENGINES OR VEHICLES

1.0 INTRODUCTION

- 1.1. This Chapter sets out requirements for checking and demonstrating the conformity of in-service engines and vehicles.

2.0 PROCEDURE FOR IN-SERVICE CONFORMITY

- 2.1. The conformity of in-service vehicles or engines of an engine family shall be demonstrated by testing vehicles on the road operated over their normal driving patterns, conditions and payloads. The in-service conformity test shall be representative for vehicles operated on their real driving routes, with their normal load and with the usual professional driver of the vehicle. When the vehicle is operated by a driver other than the usual professional driver of the particular vehicle, this alternative driver shall be skilled and trained to operate vehicles of the category subject to be tested.
- 2.2. If the normal in-service conditions of a particular vehicle are considered to be incompatible with the proper execution of the tests, the manufacturer or the Test Agency may request that alternative driving routes and payloads are used.
- 2.3. The manufacturer shall demonstrate to the Test Agency that the chosen vehicle, driving patterns, conditions and payloads are representative for the engine family. The requirements as specified in clauses 4.1 and 4.5 of this Chapter shall be used to determine whether the driving patterns and payloads are acceptable for in-service conformity testing.
- 2.4. The manufacturer shall report the schedule and the sampling plan for conformity testing at the time of the initial type-approval of a new engine family.
- 2.5. Vehicles without a communication interface which permits the collection of the necessary ECU data as specified in clauses 9.4.2.1 and 9.4.2.2 of Chapter 1 of this Part, with missing data or with a non-standard data protocol shall be considered as non-compliant.
- 2.6. Vehicles where the collection of ECU data influences the vehicle emissions or performance shall be considered as non-compliant

3.0 ENGINE OR VEHICLE SELECTION

- 3.1. After the granting of type-approval for an engine family the manufacturer shall perform in-service testing on this engine family within 18 months from the date of first registration of a vehicle fitted with an engine from that family or from 1st April 2023 whichever is later. In case of multistage type-approval first registration means first registration of a completed vehicle.

The testing shall be repeated at least every two years for each engine family periodically on vehicles over their useful life period as specified in clause 5.4. of Chapter 1 of this Part.

At the request of the manufacturer the testing may stop five years after the end of production

- 3.1.1. With a minimum sample size of three engines the sampling procedure shall be set so that the probability of a lot passing a test with 20 % of the vehicles or engines defective is 0.90 (producer's risk = 10 %) while the probability of a lot being accepted with 60 % of the vehicles or engines defective is 0.10 (consumer's risk = 10 %).
- 3.1.2. The test statistic quantifying the cumulative number of nonconforming tests at the n th test shall be determined for the sample.
- 3.1.3. The pass or fail decision of the lot shall be made according to the following requirements.
- 3.1.3. The pass or fail decision of the lot shall be made according to the following requirements.
 - (a) If the test statistic is less than or equal to the pass decision number for the sample size given in Table 1 below, a pass decision is reached for the lot;
 - (b) If the test statistic is greater than or equal to the fail decision number for the sample size given in Table 1 below, a fail decision is reached for the lot;
 - (c) Otherwise, an additional engine is tested according to this Chapter and the calculation procedure is applied to the sample increased by one more unit.

In Table 1 below the pass and fail decision numbers are calculated by means of the International Standard ISO 8422/1991.

Table 1 Pass and Fail Decision Numbers of the Sampling Plan Minimum Sample Size: 3		
Cumulative number of engine tested (sample size)	Pass decision number	Fail decision number
3	-	3
4	0	4
5	0	4
6	1	4
7	1	4
8	2	4
9	2	4
10	3	4

The Test Agency shall approve the selected engines and vehicle configurations before the launch of the testing procedures. The selection shall be performed by presenting to the Test Agency the criteria used for the selection of the particular vehicles

- 3.2.1 The engines and vehicles selected shall represent the category and application. The engines and vehicles selected shall be registered vehicles and in use. The vehicle shall have be in service at least 25000 kms. For selection of in-service vehicles, following guidelines may be used.

N3 (< 16t), N2 (> 3.5t < 12t), M3 (< 7.5t) Categories								
Vehicle Type	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6		
Mileage (km)	25000 or more	25000 or more	75000 or more	125000 or more	175000 or more	225000 or more		
N3 > 16t and M3 > 7.5 t								
Sr No	Vehicle type	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7
1	City Buses, School Buses, Construction Tipper, Mining Tipper (mileage km)	25000 or more	50000 or more	80000 or more	110000 or more	140000 or more	170000 or more	300000 or more
2	All other vehicles (mileage km)	25000 or more	50000 or more	150000 or more	250000 or more	350000 or more	450000 or more	550000 or more

- 3.2.2 The vehicle shall not be older than the useful life period as specified in clause 5.4 of Chapter 1 of this Part.

- 3.2.3 If a vehicle which has covered the suggested kms above is not available for selection of in-service conformity, a vehicle which has run at least 25000 kms per year of age of the vehicle shall be selected.

- 3.3 Each vehicle tested shall have a maintenance record to show that the vehicle has been properly maintained and serviced in accordance with the manufacturer's recommendations.

- 3.4. The OBD system shall be checked for proper functioning of the engine. Any malfunction indications and the readiness code in the OBD memory shall be recorded and any required repairs shall be carried out.

Engines presenting a Class C malfunction shall not be forced to b repaired before testing. The Diagnostic Trouble Code (DTC) shall not be cleared.

Engines having one of the counters required by provisions of Chapter 10 of this Part not at “0” may not be tested. This shall be reported to the Test Agency.

- 3.5.** The engine or vehicle shall exhibit no indications of abuse (such as overloading, misfuelling, or other misuse), or other factors (such as tampering) that could affect emission performance. OBD system fault code and engine running hours’ information stored in the computer shall be taken into account.
- 3.6.** All emission control system components on the vehicle shall be in conformity with those stated in the applicable type-approval documents.
- 3.7.** In agreement with the Test Agency, the manufacturer may run in-service conformity testing comprising fewer engines or vehicles than the number given in clause 3.1. of this Chapter, if the number of engines manufactured with in an engine family is less than 250 units per year.

4.0 TEST CONDITIONS

4.1. Vehicle Payload

For the purpose of in- service conformity testing the payload may be reproduced and an artificial load may be used.

In the absence of statistics to demonstrate that the payload is representative for the vehicle, the vehicle payload shall be 50 - 60 per cent of the maximum vehicle payload.

The maximum payload is the difference between technically permissible maximum laden mass of the vehicle and the mass of the vehicle in running order.

4.2 Ambient Conditions

The test shall be conducted under ambient conditions meeting the following conditions:

Atmospheric pressure greater than or equal to 82.5 kPa,

Temperature greater than or equal to 273 K (0°C) and less than or equal to 42°C.

4.3 Engine Coolant Temperature

The engine coolant temperature shall be in accordance with clause A.1.2.6.1. of Appendix 1 of this Chapter.

4.4 The lubricating oil, fuel and reagent shall be within the specifications issued by the manufacturer.

4.4.1 Lubricating oil

Oil samples shall be taken

4.4.2 Fuel

The test fuel shall be market fuel covered by the relevant standards or reference fuel as specified in Chapter 4 of this Part. Fuel samples shall be taken.

- 4.4.2.1 If the manufacturer in accordance with clause 4 of Chapter 1 of this Part has declared the capability to meet the requirements of this Part on fuels declared in clause 4.6.2 of Chapter 1 of this Part, tests shall be conducted on at least one of the declared market fuels or blend between the declared market fuels and the market fuels covered by the relevant standards.

4.4.3 Reagent

For exhaust after treatment systems that use a reagent to reduce emissions, a sample of the reagent shall be taken. The reagent shall not be frozen.

4.5 Trip Requirements

The shares of operation shall be expressed as a percentage of the total trip duration.

The trip shall consist of urban driving followed by rural and motorway driving according to the shares specified in clauses 4.5.1. to 4.5.4. In the case another testing order is justified for practical reasons and after the agreement of the Test Agency another order of urban, rural and motorway operation may be used.

Inclusion of operating points into urban, rural and motorway phases shall be decided based on the vehicle speed bins as given below.

For the purpose of this clause, “approximately” shall mean the target value ± 5 per cent.

Urban operation (Phase I) is characterised by vehicle speeds between 0 and 40 km/h.

Rural operation (Phase II) is characterised by vehicle speeds between 40 and 60 km/h.

Motorway operation (Phase III) is characterised by vehicle speeds above 60 km/h.

- 4.5.1 For M1 and N1 vehicles the trip shall consist of approximately 34 per cent urban, 33 per cent rural and 33 per cent motorway operation.

- 4.5.2. For M2 and M3 vehicles (other than Type-I as defined in AIS-052) the trip shall consist of approximately 20 per cent urban, 35 per cent rural and 45 per cent motorway operation. M2 and M3 vehicles of Type I as defined in AIS-052 shall be tested in approximately 70 per cent urban and 30 per cent rural operation.

- 4.5.3. For N2 vehicles the trip shall consist of approximately 25 per cent urban, 35 per cent rural and followed by 40 per cent motorway operation.

- 4.5.4. For N3 vehicles the trip shall consist of approximately 20 per cent urban, 35 per cent rural and followed by 45 per cent motorway operation.
- 4.5.5 The following distribution of the characteristic trip values from the WHDC database may serve as additional guidance for the evaluation of the trip:
 - (a) Accelerating: 26.9 per cent of the time;
 - (b) Decelerating: 22.6 per cent of the time;
 - (c) Cruising: 38.1 per cent of the time;
 - (d) Stop (vehicle speed = 0): 12.4 per cent of the time.

4.6 Operational Requirements

- 4.6.1. The trip shall be selected in such a way that the testing is uninterrupted and the data continuously sampled to reach the minimum test duration defined in clause 4.6.5.
- 4.6.2. Emissions and other data sampling shall start prior to starting the engine. Any cold start emissions may be removed from the emissions evaluation, in accordance with clause A.1.2.6. of Appendix 1 of this Chapter.
- 4.6.3. It shall not be permitted to combine data of different trips or to modify or remove data from a trip.
- 4.6.4. If the engine stalls, it may be restarted, but the sampling shall not be interrupted
- 4.6.5. The minimum test duration shall be long enough to complete five times the work performed during the WHTC or produce five times the CO₂ reference mass in kg/cycle from the WHTC as applicable.
- 4.6.6. The electrical power to the PEMS system shall be supplied by an external power supply unit, and not from a source that draws its energy either directly or indirectly from the engine under test.
 - 4.6.6.1. As an alternative, the electrical power to the PEMS system may be supplied by the internal electrical system of the vehicle as long as the power demand for the test equipment does not increase the output from the engine by more than 1% of its maximum power and measures are taken to prevent excessive discharge of the battery when the engine is not running or idling.
 - 4.6.6.2. In case of a dispute the results of measurements performed with a PEMS system powered by an external power supply shall prevail over the results acquired according to the alternative method under 4.6.6.1.
- 4.6.7 The installation of the PEMS equipment shall not influence the vehicle emissions and/or performance.

- 4.6.8. It is recommended to operate the vehicles under normal daytime traffic conditions.
- 4.6.9. If the Test Agency is not satisfied with the data consistency check results according to clause A.1.3.2. of Appendix 1 of this Chapter, the Test Agency may consider the test to be void.
- 4.6.10. The same route shall be used for the tests of vehicles within the sample described in clauses 3.1.1. to 3.1.3 of this Chapter.

5.0 ECU DATA STREAM

5.1. Verification of the availability and conformity of the ECU data-stream information required for in-service testing.

- 5.1.1. The availability of the data stream information according to the requirements of clause 9.4.2. of Chapter 1 of this Part shall be demonstrated prior to the in-service test.
 - 5.1.1.1. If that information cannot be retrieved by the PEMS system in a proper manner, the availability of the information shall be demonstrated by using an external OBD scan-tool as described in Chapter 8B of this Part.
 - 5.1.1.1.1. In the case where this information can be retrieved by the scan-tool in a proper manner, the PEMS system is considered as failing and the test is void.
 - 5.1.1.1.2. In the case where that information cannot be retrieved in a proper manner from two vehicles with engines from the same engine family, while the scan-tool is working properly, the engine is considered as non-compliant.
- 5.1.2 **Torque Signal**
 - 5.1.2.1. The conformity of the torque signal calculated by the PEMS equipment from the ECU data-stream information required in clause 9.4.2.1. of Chapter 1 of this Part shall be verified at full load.
 - 5.1.2.1.1. The method used to check this conformity is described in Appendix 4 of this Chapter.
 - 5.1.2.2. The conformity of the ECU torque signal is considered to be sufficient if the calculated torque remains within the full load torque tolerance specified in clause 9.4.2.5 of Chapter 1 of this Part.
 - 5.1.2.3. If the calculated torque does not remain within the full load torque tolerance specified in clause 9.4.2.5 of Chapter 1 of this Part, the engine is considered to have failed the test.
 - 5.1.2.4. Dual-fuel engines and vehicles shall, in addition, comply with the requirements and exceptions related to the torque correction set out in Chapter 14 of this Part.

6.0 EMISSION EVALUATION

- 6.1. The test shall be conducted and the test results shall be calculated in accordance with the provisions of Appendix 1 of this Chapter.
- 6.2. The conformity factors shall be calculated and presented for both the CO₂ mass based method and the Work based method. The pass/fail decision shall be made on the basis of the results of the Work based method.
- 6.3. The 90% cumulative percentile of the exhaust emission conformity factors from each engine system tested, determined in accordance with the measurement and calculation procedures specified in Appendix 1 of this Chapter, shall not exceed any of the values set out in Table 2 below.

Table 2 Maximum Allowed Conformity Factors for In-Service Conformity Emission Testing	
Pollutant	Maximum allowed conformity factor ⁽³⁾
CO	XX
THC ⁽¹⁾	XX
NMHC ⁽²⁾	XX
CH ₄ ⁽²⁾	XX
NO _x	XX
PM mass	---
PM Number	---

Notes:

(1) For compression ignition engines

(2) For positive ignition engines

(3) Applicable with effect from 1st Apr 2023 as notified in notification G.S.R. 889(E) dated 16th September 2016 published by MoRTH

Note: The conformity factors to be decided based on data collection.

7.0 EVALUATION OF IN-SERVICE CONFORMITY RESULTS

- 7.1 On the basis of the in-service conformity report referred to in clause 10 of this Chapter, the Test Agency shall either:
- (a) Decide that the in-service conformity testing of an engine system family is satisfactory and not take any further action;
 - (b) Decide that the data provided is insufficient to reach a decision and request additional information and test data from the manufacturer;

- (c) Decide that the in-service conformity of an engine system family is unsatisfactory and proceed to the measures referred to in clause 9.3 of Chapter 1 of this Part and in clause 9 of this Chapter.

8.0 CONFORMITY OF VEHICLE TESTING

- 8.1. Confirmatory testing is done for the purpose of confirmation of the in-service emission functionality of an engine family.
- 8.2. Test Agencies may conduct confirmatory testing.
- 8.3. The confirmatory test shall be performed as vehicle testing as specified in clauses 2.1 and 2.2 of this Chapter. Representative vehicles shall be selected and used under normal conditions and be tested according to the procedures defined in this Chapter.
- 8.4. A test result may be regarded as non-satisfactory when, from tests of two or more vehicles representing the same engine family, for any regulated pollutant component, the limit value as determined according to clause 6 of this Chapter is exceeded significantly.

9.0 PLAN OF REMEDIAL MEASURES

- 9.1. The manufacturer shall submit a report to the Test Agency where the engines or vehicles subject to remedial action are registered or used when planning to conduct remedial action, and shall submit this report when deciding to take action. The report shall specify the details of the remedial action and describe the engine families to be included in the action. The manufacturer shall report regularly to the Test Agency after the start of the remedial action.
- 9.2. The manufacturer shall provide a copy of all communications related to the plan of remedial measures, and shall maintain a record of the recall campaign (if any), and supply regular status reports to the Test Agency.
- 9.3. The manufacturer shall assign a unique identifying name or number to the plan of remedial measures.
- 9.4. The manufacturer shall present a plan of remedial measures which shall consist of the information specified in clauses 9.4.1 to 9.4.11.
 - 9.4.1. A description of each engine system type included in the plan of remedial measures.
 - 9.4.2. A description of the specific modifications, alterations, repairs, corrections, adjustments, or other changes to be made to bring the engines into conformity including a brief summary of the data and technical studies which support the manufacturer's decision as to the particular measures to be taken to correct the non-conformity.
 - 9.4.3. A description of the method by which the manufacturer informs the engine or vehicle owners about the remedial measures.

- 9.4.4. A description of the proper maintenance or use, if any, which the manufacturer stipulates as a condition of eligibility for repair under the plan of remedial measures, and an explanation of the manufacturer's reasons for imposing any such condition. No maintenance or use conditions may be imposed unless it is demonstrably related to the non-conformity and the remedial measures.
- 9.4.5. A description of the procedure to be followed by engine or vehicle owners to obtain correction of the non-conformity. This description shall include a date after which the remedial measures may be taken, the estimated time for the workshop to perform the repairs and where they can be done. The repair shall be done expediently, within a reasonable time after delivery of the vehicle.
- 9.4.6. A copy of the information transmitted to the engine or vehicle owner.
- 9.4.7. A brief description of the system which the manufacturer uses to assure an adequate supply of components or systems for fulfilling the remedial action. It shall be indicated when there will be an adequate supply of components or systems to initiate the campaign.
- 9.4.8. A copy of all instructions to be sent to those persons who are to perform the repair.
- 9.4.9. A description of the impact of the proposed remedial measures on the emissions, fuel consumption, drivability, and safety of each engine or vehicle type, covered by the plan of remedial measures with data, technical studies, etc. which support these conclusions.
- 9.4.10. Any other information, reports or data the Test Agency may reasonably determine is necessary to evaluate the plan of remedial measures.
- 9.4.11. Where the plan of remedial measures includes a recall, a description of the method for recording the repair shall be submitted to the Test Agency. If a label is used, an example of it shall be submitted.
- 9.5. The manufacturer may be required to conduct reasonably designed and necessary tests on components and engines incorporating a proposed change, repair, or modification to demonstrate the effectiveness of the change, repair, or modification

10.0 REPORTING PROCEDURE

- 10.1. A technical report shall be submitted to the Test Agency for each engine family tested. The report shall show the activities and results of the in-service conformity testing. The report shall include at least the following:
 - 10.1.1. **General**
 - 10.1.1.1. Name and address of the manufacturer:

- 10.1.1.2. Address (es) of assembly plant(s):
- 10.1.1.3. The name, address, telephone and fax numbers and e-mail address of the manufacturer's representative:
- 10.1.1.4. Type and commercial description (mention any variants):
- 10.1.1.5. Engine family:
- 10.1.1.6. Parent engine:
- 10.1.1.7. Engine family members:
- 10.1.1.8. The vehicle identification number (VIN) codes applicable to the vehicles equipped with an engine that is part of the in-service conformity check.
- 10.1.1.9. Means and location of identification of type, if marked on the vehicle:
- 10.1.1.10. Category of vehicle:
- 10.1.1.11. Type of engine: petrol, ethanol (E85), diesel/NG /LPG /ethanol (ED95) (Delete as appropriate):
- 10.1.1.12. The numbers of the type-approvals applicable to the engine types within the in-service family, including, where applicable, the numbers of all extensions and field fixes/recalls (re-works):
- 10.1.1.13. Details of extensions, field fixes/recalls to those type-approvals for the engines covered within the manufacturer's information.
- 10.1.1.14. The engine build period covered within the manufacturer's information (e.g. 'vehicles or engines manufactured during the 2020 calendar year').
- 10.1.2. Engine / Vehicle selection
 - 10.1.2.1. Vehicle or engine location method
 - 10.1.2.2. Selection criteria for vehicles, engines, in-service families;
 - 10.1.2.3. Geographical areas within which the manufacturer has collected vehicles;
- 10.1.3. Equipment
 - 10.1.3.1. PEMS Equipment, brand and type
 - 10.1.3.2. PEMS calibration
 - 10.1.3.3. PEMS power supply
 - 10.1.3.4. Calculation software and version used (e.g. EMROAD 4.0)
- 10.1.4. Test data
 - 10.1.4.1. Date and time of test;

- 10.1.4.2. Location of test including details information about the test route;
- 10.1.4.3. Weather / ambient conditions (e.g. temperature, humidity, altitude);
- 10.1.4.4. Distances covered per vehicle on the test route;
- 10.1.4.5. Test fuel specifications characteristics
- 10.1.4.6. Reagent specification (if applicable)
- 10.1.4.7. Lubrication oil specification
- 10.1.4.8. Emission test results according to Appendix 1 of this Chapter
- 10.1.5. Engine information
 - 10.1.5.1. Engine fuel type (e.g. diesel, ethanol ED95, NG, LPG, petrol, E85)
 - 10.1.5.2. Engine combustion system (e.g. compressed ignition or positive ignition)
 - 10.1.5.3. Type-approval number
 - 10.1.5.4. Engine rebuilt
 - 10.1.5.5. Engine manufacturer
 - 10.1.5.6. Engine model
 - 10.1.5.7. Engine production year and month
 - 10.1.5.8. Engine identification number
 - 10.1.5.9. Engine displacement [litres]
 - 10.1.5.10. Number of cylinders
 - 10.1.5.11. Engine rated power: [kW @ rpm]
 - 10.1.5.12. Engine peak torque: [Nm @ rpm]
 - 10.1.5.13. Idle speed [rpm]
 - 10.1.5.14. Manufacturer supplied full-load torque curve available (yes/no)
 - 10.1.5.15. Manufacturer supplied full-load torque curve reference number
 - 10.1.5.16. DeNOx system (e.g. EGR, SCR)
 - 10.1.5.17. Type of catalytic converter
 - 10.1.5.18. Type of Particulate trap
 - 10.1.5.19. After treatment modified with respect to type-approval? (yes/no)
 - 10.1.5.20. Engine ECU information (Software calibration number)
- 10.1.6. Vehicle information

- 10.1.6.1. Vehicle owner
- 10.1.6.2. Vehicle type (e.g. M3, N3) and application (e.g. rigid or articulated truck, city bus)
- 10.1.6.3. Vehicle manufacturer
- 10.1.6.4. Vehicle Identification Number
- 10.1.6.5. Vehicle registration number and country of registration
- 10.1.6.6. Vehicle model
- 10.1.6.7. Vehicle production year and month
- 10.1.6.8. Transmission type (e.g. manual, automatic or other)
- 10.1.6.9. Number of forward gears
- 10.1.6.10. Odometer reading at test start [km]
- 10.1.6.11. Gross vehicle combination weight rating (GVW) [kg]
- 10.1.6.12. Tire size [Not mandatory]
- 10.1.6.13. Tail pipe diameter [mm] [Not mandatory]
- 10.1.6.14. Number of axles
- 10.1.6.15. Fuel tank(s) capacity [liters] [Not mandatory]
- 10.1.6.16. Number of fuel tanks [Not mandatory]
- 10.1.6.17. Reagent tank(s) capacity [litres] [Not mandatory]
- 10.1.6.18. Number of reagent tanks [Not mandatory]
- 10.1.7. Test route characteristics
 - 10.1.7.1. Odometer reading at test start [km]
 - 10.1.7.2. Duration [s]
 - 10.1.7.3. Average ambient conditions (as calculated from the instantaneous measured data)
 - 10.1.7.4. Ambient conditions sensor information (type and location of sensors)
 - 10.1.7.5. Vehicle speed information (for example cumulative speed distribution)
 - 10.1.7.6. Shares of the time of the trip characterised by urban, rural and motorway operation as described in clause 4.5 of this Chapter.

- 10.1.7.7. Shares of the time of the trip characterised by accelerating, decelerating, cruising and stop as described in clause 4.5.5 of this Chapter.
- 10.1.8. Instantaneous measured data
 - 10.1.8.1. THC concentration [ppm]
 - 10.1.8.2. CO concentration [ppm]
 - 10.1.8.3. NO_x concentration [ppm]
 - 10.1.8.4. CO₂ concentration [ppm]
 - 10.1.8.5. CH₄ concentration [ppm] for natural gas fuelled engines only
 - 10.1.8.6. Exhaust gas flow [kg/h]
 - 10.1.8.7. Exhaust temperature [°C]
 - 10.1.8.8. Ambient air temperature [°C]
 - 10.1.8.9. Ambient pressure [kPa]
 - 10.1.8.10. Ambient humidity [g/kg] [Not mandatory]
 - 10.1.8.11. Engine torque [Nm]
 - 10.1.8.12. Engine speed [rpm]
 - 10.1.8.13. Engine fuel flow [g/s]
 - 10.1.8.14. Engine coolant temperature [°C]
 - 10.1.8.15. Vehicle ground speed [km/h] from ECU and GPS
 - 10.1.8.16. Vehicle latitude [degree](Accuracy needs to be sufficient to enable the traceability of the test route)
 - 10.1.8.17. Vehicle longitude [degree]
- 10.1.9. Instantaneous calculated data
 - 10.1.9.1. THC mass [g/s]
 - 10.1.9.2. CO mass [g/s]
 - 10.1.9.3. NO_x mass [g/s]
 - 10.1.9.4. CO₂ mass [g/s]
 - 10.1.9.5. CH₄ mass [g/s] for P.I. engines only
 - 10.1.9.6. THC cumulated mass [g]
 - 10.1.9.7. CO cumulated mass [g]

10.1.9.8.	NOx cumulated mass [g]
10.1.9.9.	CO ₂ cumulated mass [g]
10.1.9.10.	CH ₄ cumulated mass [g] for natural gas fuelled engines only
10.1.9.11.	Calculated fuel rate [g/s]
10.1.9.12.	Engine power [kW]
10.1.9.13.	Engine work [kWh]
10.1.9.14.	Work window duration [s]
10.1.9.15.	Work window average engine power [%]
10.1.9.16.	Work window THC conformity factor [-]
10.1.9.17.	Work window CO conformity factor [-]
10.1.9.18.	Work window NOx conformity factor [-]
10.1.9.19.	Work window CH ₄ conformity factor [-]for natural gas fuelled engines only
10.1.9.20.	CO ₂ mass window duration [s]
10.1.9.21.	CO ₂ mass window THC conformity factor [-]
10.1.9.22.	CO ₂ mass window CO conformity factor [-]
10.1.9.23.	CO ₂ mass window NOx conformity factor [-]
10.1.9.24.	CO ₂ mass window CH ₄ conformity factor [-] for natural gas fuelled engines only
10.1.10.	Averaged and integrated data
10.1.10.1.	Average THC concentration [ppm] [Not mandatory]
10.1.10.2.	Average CO concentration [ppm] [Not mandatory]
10.1.10.3.	Average NOx concentration [ppm] [Not mandatory]
10.1.10.4.	Average CO ₂ concentration [ppm] [Not mandatory]
10.1.10.5.	Average CH ₄ concentration [ppm] for natural gas engines only [Not mandatory]
10.1.10.6.	Average Exhaust gas flow [kg/h] [Not mandatory]
10.1.10.7.	Average Exhaust temperature [°C] [Not mandatory]
10.1.10.8.	THC emissions [g]
10.1.10.9.	CO emissions [g]
10.1.10.10.	NOx emissions [g]

10.1.10.11	CO ₂ emissions [g]
10.1.10.12.	CH ₄ emissions [g] for gas engines only
10.1.11.	Pass-Fail results
10.1.11.1.	Minimum, maximum, and 90% cumulative percentile for:
10.1.11.2.	Work window THC conformity factor [-]
10.1.11.3.	Work window CO conformity factor [-]
10.1.11.4.	Work window NO _x conformity factor [-]
10.1.11.5.	Work window CH ₄ conformity factor [-]for natural gas fuelled engines only
10.1.11.6.	CO ₂ mass window THC conformity factor [-]
10.1.11.7.	CO ₂ mass window CO conformity factor [-]
10.1.11.8.	CO ₂ mass window NO _x conformity factor [-]
10.1.11.9.	CO ₂ mass window CH ₄ conformity factor [-]for natural gas fuelled engines only
10.1.11.10.	Work window: Minimum and maximum average window power [%]
10.1.11.11.	CO ₂ mass window: Minimum and maximum window duration [s]
10.1.11.12.	Work window: Percentage of valid windows
10.1.11.13.	CO ₂ mass window: Percentage of valid windows
10.1.12.	Test verifications
10.1.12.1.	THC analyser zero, span and audit results, pre and post test
10.1.12.2.	CO analyser zero, span and audit results, pre and post test
10.1.12.3.	NO _x analyser zero-span and audit results, pre and post test
10.1.12.4.	CO ₂ analyser zero, span and audit results, pre and post test
10.1.12.5	CH ₄ analyser zero, span and audit results, pre and post test for natural gas fuelled engines only
10.1.12.6	Data consistency check results, according to clause A.1.3.2. of Appendix 1 of this Chapter.
10.1.12.6.1	Results of the linear regression described in clause A.1.3.2.1. of Appendix 1 of this Chapter including the slope of the regression line, m, coefficient of determination, r^2 and the intercept, b, of the y-axis of the regression line.

- 10.1.12.6.2 Result of the consistency check of the ECU data in accordance with clause A.1.3.2.2. of Appendix 1 of this Chapter.
- 10.1.12.6.3 Result of the consistency check of the Brake-specific fuel consumption in accordance with paragraph A.1.3.2.3. of Appendix 1 of this Chapter, including the calculated Brake-specific fuel consumption and the ratio of the calculated Brake-specific fuel consumption from the PEMS measurement and the declared Brake-specific fuel consumption for the WHTC test.
- 10.1.12.6.4 Result of the consistency check of the odometer in accordance with clause A.1.3.2.4. of Appendix 1 of this Chapter.
- 10.1.12.6.5 Result of the consistency check of the ambient pressure in accordance with paragraph A.1.3.2.5. of Appendix 1 of this Chapter.
- 10.1.13. List of further attachments where these exist

CHAPTER 7 - APPENDIX 1

TEST PROCEDURE FOR VEHICLE EMISSIONS TESTING WITH PORTABLE EMISSIONS MEASUREMENT SYSTEMS

A.1.1 INTRODUCTION

This Appendix describes the procedure to determine gaseous emissions from on-vehicle on-road measurements using Portable Emissions Measurement Systems (here in after PEMS). The gaseous emissions to be measured from the exhaust of the engine include the following components: carbon monoxide, total hydrocarbons and nitrogen oxides for diesel engines with the addition of methane for gas engines.

For engines fuelled with gases and natural gas, the manufacturer, Test Agencies may choose to measure the total hydrocarbon (THC) emissions instead of measuring the non-methane hydrocarbon emission. In this case the emission limit for the total hydrocarbon emissions is the same as shown in clause 5.3 of Chapter 1 of this Part for non-methane hydrocarbon emissions. The applicable limit in the calculations of the conformity factors in A 1.4.2.3 and A1.4.3.2 of this Appendix shall in that case be the non-methane emission limit.

Additionally, carbon dioxide shall be measured to enable the calculation procedures described in clause A1.3 and A1.4 of this Appendix.

A.1.2 TEST PROCEDURE

A.1.2.1 General Requirements

The test shall be carried out with a PEMS comprised of :

- A.1.2.1.1. Gas analyzers to measure the concentrations of regulated gaseous pollutants in the exhaust gas;
- A.1.2.1.2 An exhaust mass flow meter based on the averaging Pitot or equivalent principle;
- A.1.2.1.3 A Global Positioning System (hereinafter "GPS");
- A.1.2.1.4 Sensors to measure the ambient temperature and pressure;
- A.1.2.1.5 A connection with the vehicle ECU;

A.1.2.2 TEST PARAMETERS

The parameters summarized in Table 1 below shall be measured and recorded.

Table 1
Test Parameters

Parameter	Unit	Source
THC concentration ⁽¹⁾	ppm	Analyser
CO concentration ⁽¹⁾	ppm	Analyser
NO _x concentration ⁽¹⁾	ppm	Analyser
CO ₂ concentration ⁽¹⁾	ppm	Analyser
CH ₄ concentration ⁽¹⁾⁽²⁾	ppm	Analyser
Exhaust gas flow	kg/h	Exhaust Flow Meter (hereinafter EFM)
Exhaust temperature	°K	EFM
Ambient temperature ⁽³⁾	°K	Sensor
Ambient pressure	kPa	Sensor
Engine torque ⁽⁴⁾	Nm	ECU or Sensor
Engine speed	rpm	ECU or Sensor
Engine fuel flow	g/s	ECU or Sensor
Engine coolant temperature	°K	ECU or Sensor
Engine intake air temperature ⁽³⁾	°K	Sensor
Vehicle ground speed	km/h	ECU and GPS
Vehicle latitude	degree	GPS
Vehicle longitude	degree	GPS

Notes:

⁽¹⁾ Measured or corrected to a wet basis

⁽²⁾ Gas engines only

⁽³⁾ Use the ambient temperature sensor or an intake air temperature sensor

⁽⁴⁾ The recorded value shall be either (a) the net brake engine torque according to clause A1.2.4.4 of this Appendix or (b) the net brake engine torque calculated from the torque values according to clause A.1.2.4.4 of this Appendix.

A.1.2.3 **Preparation of the vehicle**

The preparation of the vehicle shall include the following:

- (a) The check of the OBD system: any identified problems once solved shall be recorded and presented to the Test Agency.
- (b) The replacement of oil, fuel and reagent, if any.

A.1.2.4 **Installation of the Measuring Equipment**

A.1.2.4.1 **Main Unit**

Whenever possible, PEMS shall be installed in a location where it will be subject to minimal impact from the followings:

- (a) Ambient temperature changes;
- (b) Ambient pressure changes;
- (c) Electromagnetic radiation;
- (d) Mechanical shock and vibration;
- (e) Ambient hydrocarbons – if using a FID analyser that uses ambient air as FID burner air.

The installation shall follow the instructions issued by the PEMS manufacturer

A.1.2.4.2 **Exhaust Flow Meter**

The exhaust flow meter shall be attached to the vehicle's tailpipe. The EFM sensors shall be placed between two pieces of straight tube whose length should be at least 2 times the EFM diameter (upstream and downstream). It is recommended to place the EFM after the vehicle silencer, to limit the effect of exhaust gas pulsations upon the measurement signals.

A.1.2.4.3 **Global Positioning System.**

The antenna shall be mounted at the highest possible location, without risking interference with any obstructions encountered during on-road operation.

A.1.2.4.4 **Connection with the vehicle ECU**

A data logger shall be used to record the engine parameters listed in Table 1 of this Appendix. This data logger can make use of the Control Area Network (hereinafter CAN) bus of the vehicle to access the ECU data specified in Table 1 of Appendix 5 of Chapter 8B of this Part and broadcasted on the CAN according to standard protocols such as SAE J1939, J1708 or ISO 15765-4. It may calculate the net brake engine torque or perform unit conversions

A.1.2.4.5 **Sampling of gaseous emissions**

The sample line shall be heated according to the specifications of clause A.2.2.3. of Appendix 2 of this Chapter and properly insulated at the connection points (sample probe and back of the main unit), to avoid the presence of cold spots that could lead to a contamination of the sampling system by condensed hydrocarbons.

The sample probe shall be installed in the exhaust pipe in accordance with the requirements of clause 9.3.10 of Chapter 3 of this Part.

If the length of the sample line is changed, the system transport times shall be verified and if necessary corrected.

A.1.2.5 Pre-test procedures

A.1.2.5.1 Starting and stabilizing the PEMS instruments

The main units shall be warmed up and stabilized according to the instrument manufacturer specifications until pressures, temperatures and flows have reached their operating set points.

A.1.2.5.2 Cleaning the sampling system

To prevent system contamination, the sampling lines of the PEMS instruments shall be purged until sampling begins, according to the instrument manufacturer specifications.

A.1.2.5.3 Checking and calibrating the analysers

The zero and span calibration and the linearity checks of the analysers shall be performed using calibration gases meeting the requirements of clause 9.3.3 of Chapter 3 of this Part. A linearity check shall have been performed within three months before the actual test.

A.1.2.5.4 Cleaning the EFM

The EFM shall be purged at the pressure transducer connections in accordance with the instrument manufacturer specifications. This procedure shall remove condensation and diesel particulate matter from the pressure lines and the associated flow tube pressure measurement ports.

A.1.2.6 Emission Test Run

A.1.2.6.1 Test Start

Emissions sampling, measurement of the exhaust parameters and recording of the engine and ambient data shall start prior to starting the engine. The data evaluation shall start after the coolant temperature has reached 343K (70°C) for the first time or after the coolant temperature is stabilized within ± 2 K over a period of 5 minutes whichever comes first but no later than 20 minutes after engine start.

A.1.2.6.2 Test Run

Emission sampling, measurement of the exhaust parameters and recording of the engine and ambient data shall continue throughout the normal in-use operation of the engine. The engine may be stopped and started, but emissions sampling shall continue throughout the entire test.

Periodic checks of the PEMS gas analysers shall be conducted at least every two hours. The data recorded during the checks shall be flagged and shall not be used for the emission calculations.

A.1.2.6.3 End of Test Sequence

At the end of the test, sufficient time shall be given to the sampling systems to allow their response times to elapse. The engine may be shut down before or after sampling is stopped.

A.1.2.7 Verification of the Measurements

A.1.2.7.1 Checking of the analysers

The zero, span and linearity checks of the analysers as described in clause A.1.2.5.3 of this Appendix shall be performed using calibration gases meeting the requirements of clause 9.3.3 of Chapter 3 of this Part.

A.1.2.7.2 Zero Drift

Zero response is defined as the mean response, including noise, to a zero gas during a time interval of at least 30 seconds. The drift of the zero response shall be less than 2 per cent of full scale on the lowest range used.

A.1.2.7.3 Span Drift

Span response is defined as the mean response, including noise, to a span gas during a time interval of at least 30 seconds. The drift of the span response shall be less than 2 per cent of full scale on the lowest range used.

A.1.2.7.4 Drift verification

This shall apply only if, during the test, no zero drift correction was made.

As soon as practical but no later than 30 minutes after the test is complete the gaseous analyser ranges used shall be zeroed and spanned to check their drift compared to the pre-test results.

The following provisions shall apply for analyser drift:

- (a) If the difference between the pre-test and post-test results is less than 2 per cent as specified in clauses A.1.2.7.2. and A.1.2.7.3 of this Appendix., the measured concentrations may be used uncorrected or may be corrected for drift according to clause A.1.2.7.5 of this Appendix.;
- (b) If the difference between the pre-test and post-test results is equal to or greater than 2 per cent as specified in clauses A.1.2.7.2. and A.1.2.7.3 of this Appendix., the test shall be voided or the measured concentrations shall be corrected for drift according to clause A.1.2.7.5 of this Appendix.

A.1.2.7.5 Drift Correction

If drift correction is applied in accordance with clause A.1.2.7.4 of this Appendix, the corrected concentration value shall be calculated according to clause 8.6.1 of Chapter 3 of this Part.

The difference between the uncorrected and the corrected brake-specific emission values shall be within ± 6 per cent of the uncorrected brake-specific emission values. If the drift is greater than 6 per cent, the test shall be voided. If drift correction is applied, only the drift-corrected emission results shall be used when reporting emissions.

A.1.3 CALCULATION OF THE EMISSION

The final test result shall be rounded in one step to the number of places to the right of the decimal point indicated by the applicable emission standard plus one additional significant figure, in accordance with ASTM E 29-06b. No rounding of intermediate values leading to the final brake-specific emission result shall be allowed.

A.1.3.1 Time Alinement of Data

To minimize the biasing effect of the time, lag between the different signals on the calculation of mass emissions, the data relevant for emissions calculation shall be time aligned, as described in clauses A.1.3.1.1 to A.1.3.1.4 of this Appendix.

A.1.3.1.1 Gas Analysers Data

The data from the gas analysers shall be properly aligned using the procedure in clause 9.3.5. of Chapter 3 of this Part.

A.1.3.1.2 Gas analyzers and EFM data

The data from the gas analysers shall be properly aligned with the data of the EFM using the procedure in clause A.1.3.1.4 of this Appendix.

A.1.3.1.3 PEMS and Engine Data

The data from the PEMS (gas analysers and EFM) shall be properly aligned with the data from the engine ECU using the procedure in clause A.1.3.1.4 of this Appendix.

A.1.3.1.4 Procedure for improved time-alignment of the PEMS data

The test data listed in Table 1 of this Appendix are split into 3 different categories:

- 1: Gas analysers (THC, when applicable CH₄, CO, CO₂, NO_x concentrations);
- 2: Exhaust Flow Meter (Exhaust mass flow and exhaust temperature);
- 3: Engine (Torque, speed, temperatures, fuel rate, vehicle speed from ECU).

The time alignment of each category with the other categories shall be verified by finding the highest correlation coefficient between two series of parameters. All the parameters in a category shall be shifted to maximize the correlation factor. The following parameters shall be used to calculate the correlation coefficients:

To time-align:

- (a) Categories 1 and 2 (Analysers and EFM data) with category 3 (Engine data): the vehicle speed from the GPS and from the ECU.
- (b) Category 1 with category 2: the CO₂ concentration and the exhaust mass.
- (c) Category 2 with category 3: the CO₂ concentration and the engine fuel flow.

A.1.3.2 Data Consistency Checks

A.1.3.2.1 Analysers and EFM data

The consistency of the data (exhaust mass flow measured by the EFM and gas concentrations) shall be verified using a correlation between the measured fuel flow from the ECU and the fuel flow calculated using the formula in clause 8.4.1.6. of Chapter 3 of this Part. A linear regression shall be performed for the measured and calculated fuel rate values. The method of least squares shall be used, with the best fit equation having the form:

$$y = mx + b$$

Where:

Y is the calculated fuel flow [g/s]

m is the slope of the regression line

x is the measured fuel flow [g/s]

b is the y intercept of the regression line

The slope (m) and the coefficient of determination (r^2) shall be calculated for each regression line. It is recommended to perform this analysis in the range from 15 per cent of the maximum value to the maximum value and at a frequency greater or equal to 1 Hz. For a test to be considered valid, the following two criteria shall be evaluated:

Table 2 Tolerances	
Slope of the regression line, m	0.9 to 1.1 - Recommended
Coefficient of determination r^2	min. 0.90 - Mandatory

A.1.3.2.2 ECU Torque Data

The consistency of the ECU torque data shall be verified by comparing the maximum ECU torque values at different engine speeds with the corresponding values on the official engine full load torque curve according to clause 5. of this Chapter.

A.1.3.2.3 Brake-Specific Fuel Consumption

The Brake Specific Fuel Consumption (BSFC) shall be checked using:

- (a) The fuel consumption calculated from the emissions data (gas analyser concentrations and exhaust mass flow data), according to the formulae in clause 8.4.1.6. of Chapter 3 of this Part;
- (b) The work calculated using the data from the ECU (Engine torque and engine speed).

A.1.3.2.4 Odometer

The distance indicated by the vehicle odometer shall be checked against the GPS data and verified.

A.1.3.2.5 Ambient Pressure

The ambient pressure value shall be checked against the altitude indicated by the GPS data.

A.1.3.3 Dry-Wet Correction

If the concentration is measured on a dry basis, it shall be converted to a wet basis according to the formula in clause 8.1. of Chapter 3 of this Part.

A.1.3.4 NO_x correction for humidity and temperature

The NO_x concentrations measured by the PEMS shall not be corrected for ambient air temperature and humidity.

A.1.3.5 Calculation of the instantaneous gaseous emissions

The mass emissions shall be determined as described in clause 8.4.2.3. of Chapter 3 of this Part.

A.1.4 DETERMINATION OF EMISSIONS AND CONFORMITY FACTORS

A.1.4.1 Averaging Window Principle

The emissions shall be integrated using a moving averaging window method, based on the reference CO₂ mass or the reference work. The principle of the calculation is as follows: The mass emissions are not calculated for the complete data set, but for sub-sets of the complete data set, the length of these sub-sets being determined so as to match the engine CO₂ mass or work measured over the reference laboratory transient cycle. The moving average calculations are conducted with a time increment Δt equal to the data sampling period. These sub-sets used to average the emissions data are referred to as “averaging windows” in the following paragraphs:

Any portion of invalidated data shall not be considered for the calculation of the work or CO₂ mass and the emissions of the averaging window.

The following data shall be considered as invalidated data:

- (a) The periodic verification of the instruments and/or after the zero drift verifications;
- (b) The data outside the conditions specified in clauses 4.2. and 4.3. of this Chapter.

The mass emissions (mg/window) shall be determined as described in clause 8.4.2.3. of Chapter 3 of this Part.

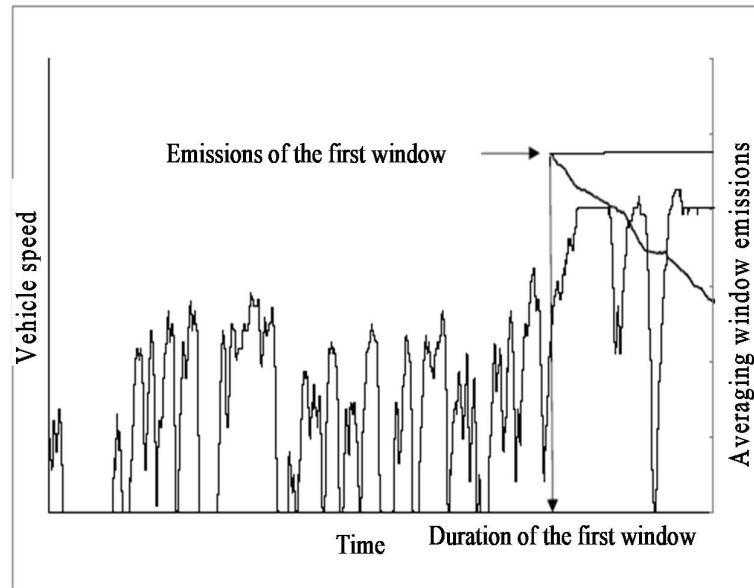


Figure 1
Vehicle Speed Versus Time and Vehicle Averaged Emissions,
Starting from the First Averaging Window, Versus Time.

A.1.4.2 Work Based Method

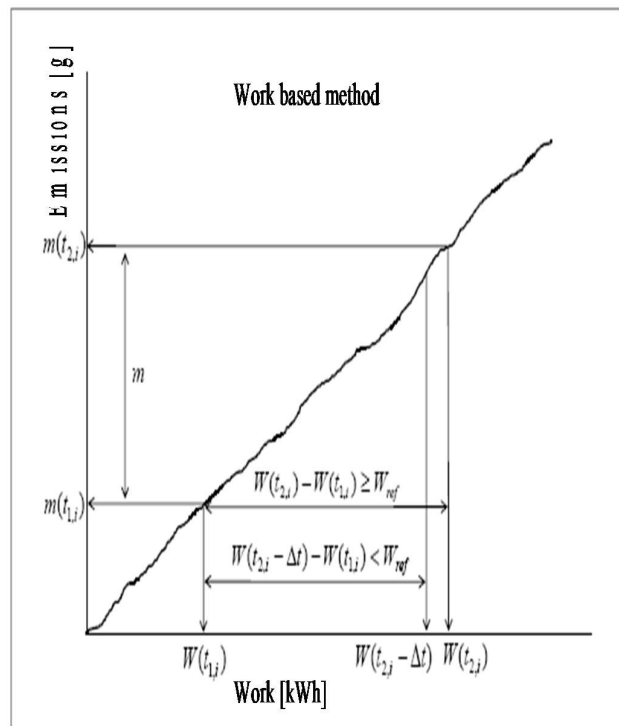


Figure 2.
Work Based Method

The duration ($t_{2i} - t_{1i}$) of the i^{th} averaging window is determined by:

$$W(t_{2,i}) - W(t_{1,i}) \geq W_{ref}$$

Where:

$W(t_{j,i})$ is the engine work measured between the start and time $t_{j,i}$, kWh;

W_{ref} is the engine work for the WHTC, kWh

$t_{2,i}$ shall be selected such that:

$$W(t_{2,i} - \Delta t) - W(t_{1,i}) < W_{ref} \leq W(t_{2,i}) - W(t_{1,i})$$

Where Δt is the data sampling period, equal to 1 second or less.

A.1.4.2.1 Calculation of The Specific Emissions

The specific emissions e_{gas} (mg/kWh) shall be calculated for each window and each pollutant in the following way:

$$e_{\text{gas}} = \frac{m}{W(t_{2,i}) - W(t_{1,i})}$$

Where:

m is the mass emission of the component, mg/window

$W(t_{2,i}) - W(t_{1,i})$ is the engine work during the i^{th} averaging window, kWh

A.1.4.2.2 Selection of Valid Windows

The valid windows are the windows whose average power exceeds the power threshold of 20% of the maximum engine power. The percentage of valid windows shall be equal or greater than 50 per cent.

A.1.4.2.2.1 If the percentage of valid windows is less than 50 per cent, the data evaluation shall be repeated using lower power thresholds. The power threshold shall be reduced in steps of 1 per cent until the percentage of valid windows is equal to or greater than 50 per cent.

A.1.4.2.2.2 In any case, the lower threshold shall not be lower than 15 per cent.

A.1.4.2.2.3 The test shall be void if the percentage of valid windows is less than 50 per cent at a power threshold of 15 per cent.

A.1.4.2.3 Calculation of the conformity factors

The conformity factors shall be calculated for each individual valid window and each individual pollutant in the following way:

$$CF = \frac{e}{L}$$

Where:

e is the brake-specific emission of the component, mg/kWh;

L is the applicable limit, mg/kWh.

A.1.4.3 CO₂ Mass Based Method

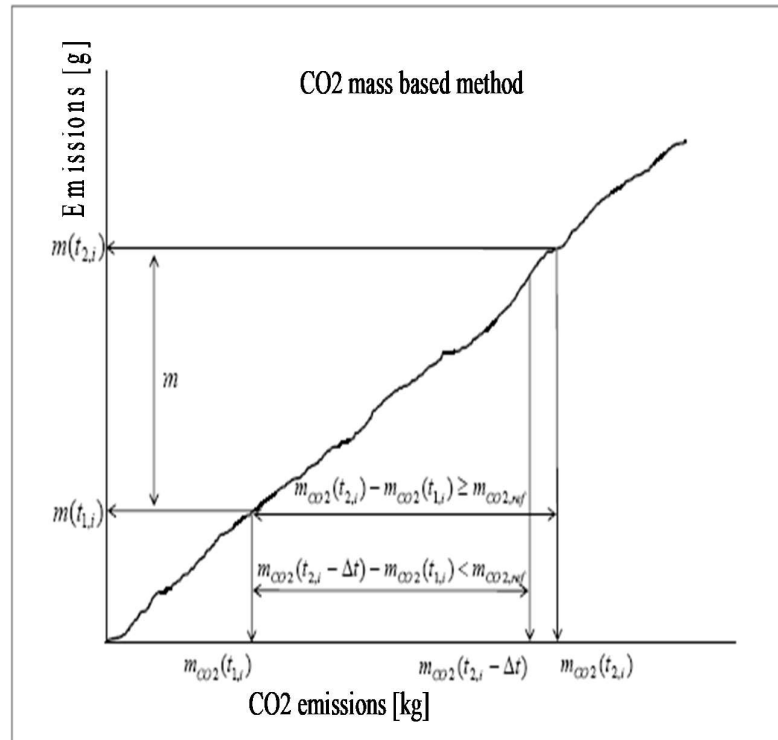


Figure 3
CO₂ Mass Based Method

The duration $(t_{2,i} - t_{1,i})$ of the i^{th} averaging window is determined by:

$$m_{CO2}(t_{2,i}) - m_{CO2}(t_{1,i}) \geq m_{CO2,ref}$$

Where:

$m_{CO2}(t_{j,i})$ is the CO₂ mass measured between the test start and time $t_{j,i}$, kg;

$m_{CO2,ref}$ is the CO₂ mass determined for the WHTC, kg;

$t_{2,i}$ shall be selected such as:

$$m_{CO_2}(t_{2,i} - \Delta t) - m_{CO_2}(t_{1,i}) < m_{CO_2,ref} \leq m_{CO_2}(t_{2,i}) - m_{CO_2}(t_{1,i})$$

Where Δt is the data sampling period, equal to 1 second or less.

The CO₂ masses are calculated in the windows by integrating the instantaneous emissions calculated according to the requirements introduced in clause A.1.3.5 of this Appendix.

A.1.4.3.1 Selection of valid windows

The valid windows shall be the windows whose duration does not exceed the maximum duration calculated from:

$$D_{\max} = 3600 \cdot \frac{W_{ref}}{0.2 \cdot P_{\max}}$$

D_{\max} is the maximum window duration, s;

P_{\max} is the maximum engine power, kW.

A.1.4.3.1.1 If the percentage of valid windows is less than 50% the data evaluation shall be using longer window durations. this is achieved by decreasing the value of 0.2 in the formula given in clause A.1.4.3.1 by steps of 0.01 until the percentage of valid windows is equal to greater than 50%.

A.1.4.3.1.2 In any case the lowered value in the above formula shall not be lower than 0.15

A.1.4.3.1.3 The test shall be void if the percentage of valid windows is less than 50% at a maximum window duration calculated in accordance with clauses 1.4.3.1 ,1.4.3.1.1 and 1.4.3.1.2 of this Appendix.

A.1.4.3.2 Calculation of the Conformity Factor

The conformity factors shall be calculated for each individual window and each individual pollutant in the following way:

$$CF = \frac{CF_I}{CF_C}$$

With $CF_I = \frac{m}{m_{CO_2}(t_{2,i}) - m_{CO_2}(t_{1,i})}$ (in service ratio) and

$$CF_C = \frac{m_L}{m_{CO_2,ref}} \quad \text{(Certification ratio)}$$

Where:

m	is the mass emission of the component, mg/window
$m_{CO_2}(t_{2,i}) - m_{CO_2}(t_{1,i})$	is the CO ₂ mass during the i th averaging window, kg;
$m_{CO_2,ref}$	is the engine CO ₂ mass determined for the WHTC, kg;
m_L	is the mass emission of the component corresponding to the applicable limit on the WHTC, mg.

CHAPTER 7 - APPENDIX 2**PORTABLE EMISSION MEASUREMENT EQUIPMENT****A.2.1 GENERAL**

The gaseous emissions shall be measured according to the procedure set out in Appendix 1 of this Chapter. The present Appendix describes the characteristics of the portable measurement equipment that shall be used to perform such tests.

A.2.2 MEASURING EQUIPMENT**A.2.2.1 Gas Analyser Specification**

The PEMS gas analysers specifications shall meet the requirements set out in clause 9.3.1. of Chapter 3 of this Part.

A.2.2.2 Gas Analyser Technology

The gases shall be analysed using the technologies specified in clause 9.3.2 of Chapter 3 of this Part.

The oxides of nitrogen analyser may also be of the Non-Dispersive Ultra Violet (NDUV) type.

A.2.2.3 Sampling of gaseous emissions

The sampling probes shall meet the requirements defined in clause A.2.1.2 and A.2.1.3 of Appendix 2 of Chapter 3 of this Part. The sampling line shall be heated to 190°C (+/-10°C).

A.2.2.4 Other Instruments

The measuring instruments shall satisfy the requirements given in Table 7 and clause 9.3.1 of Chapter 3 of this Part.

A.2.3 AUXILIARY EQUIPMENT**A.2.3.1 Exhaust Gas Flow Meter (EFM) tailpipe connection**

The installation of the EFM shall not increase the backpressure by more than the value recommended by the engine manufacturer, nor increase the length of the tailpipe by more than 1.2 m. As for the all the components of the PEMS equipment, the installation of the EFM shall comply with the locally applicable road safety standards and insurance requirements.

A.2.3.2 PEMS Location and Mounting Hardware

The PEMS equipment shall be installed as specified in clause A.1.2.4. of Appendix 1 of this Chapter.

A.2.3.3 Electrical power

The PEMS equipment shall be powered using the method described in clause 4.6.6. of this Chapter.

CHAPTER 7 - APPENDIX 3

CALIBRATION OF PORTABLE EMISSION MEASUREMENT EQUIPMENT

A.3.1. EQUIPMENT CALIBRATION AND VERIFICATION

A.3.1.1. Calibration gases

The PEMS gas analysers shall be calibrated using gases meeting the requirements as set out in clause 9.3.3 of Chapter 3 of this Part.

A.3.1.2. Leakage test

The PEMS leakage tests shall be conducted following the requirements defined in clause 9.3.4. of Chapter 3 of this Part.

A.3.1.3 Response time check of the analytical system

The response time check of the PEMS analytical system shall be conducted in accordance with the requirements set out in clause 9.3.5. of Chapter 3 of this Part.

CHAPTER 7 - APPENDIX 4
METHOD TO CHECK THE CONFORMITY OF
THE ECU TORQUE-SIGNAL

A.4.1. INTRODUCTION

This Appendix describes in a non-detailed manner the method used to check the conformity of the ECU torque-signal during ISC-PEMS testing.

The detailed applicable procedure is left to the engine manufacturer, subject to approval of the Test Agency.

A.4.2 THE "MAXIMUM TORQUE" METHOD

A.4.2.1 The "Maximum torque" method consists of demonstrating that a point on the reference maximum torque curve as a function of the engine speed has been reached during vehicle testing.

A.4.2.2 If a point on the reference maximum torque curve as a function of the engine speed has not been reached during the ISC PEMS emissions testing, the manufacturer is entitled to modify the load of the vehicle and/or the testing route as necessary in order to perform that demonstration after the ISC PEMS emissions test has been completed.

CHAPTER 8A ON-BOARD DIAGNOSTIC SYSTEMS (OBD)

1.0 INTRODUCTION

This Chapter sets out the functional aspects of on-board diagnostic (OBD) systems for the control of emissions from engine systems which are covered by this Part.

2.0 GENERAL REQUIREMENTS

2.1. The general requirements, including the specific requirements for electronic system security, shall be those set out in clause 4 of Chapter 8B of this Part and those described in clause 2 of this Chapter.

2.2. Requirements regarding operating sequences and driving cycles for hybrid vehicles and vehicles with stop-start systems

2.2.1 Operating Sequence

2.2.1.1 For vehicles that employ engine shut-off strategies that are commanded by the engine control system (for example hybrid bus with engine shut-off at idle) and that are followed by an engine cranking, the (engine shut-off – engine cranking) sequence shall be considered as part of the existing operating sequence.

2.2.1.2 The manufacturer shall provide the description of such strategies in the documentation considered in clauses 3.1.3. (a) and 3.1.3. (b) of Chapter 1 of this Part.

2.2.1.3 In the case of a hybrid vehicle, the operating sequence shall start at the time of the engine start or at the time when the vehicle starts moving, whichever occurs first.

2.2.2 Driving cycle

2.2.2.1 For vehicles that employ engine shut-off strategies that are commanded by the engine control system (for example hybrid bus with engine shut-off at idle) and that are followed by an engine cranking, the (engine shut-off – engine cranking) sequence shall be considered as part of the existing driving cycle

2.2.2.2 The manufacturer shall provide the description of such strategies in the documentation considered in clauses 3.1.3. (a) and 3.1.3. (b) of Chapter 1 of this Part.

2.2.2.3 In the case of a hybrid vehicle, the driving cycle shall start at the time of the engine start or at the time when the vehicle starts moving, whichever occurs first."

2.3. Additional Provisions Concerning Monitoring Requirements.

2.3.1. Malfunctioning Injectors

2.3.1.1. The manufacturer shall submit to the Test Agency an analysis of the long-term effects on the emission control system of malfunctioning fuel injectors (for example clogged or soiled injectors) even if the OBD Threshold Limits (OTLs) are not exceeded as a consequence of these malfunctions.

2.3.1.2. After the period set out in clause 4.10.7 of Chapter 1 of this Part the manufacturer shall submit to the Test Agency a plan of the monitoring techniques he intends to use in addition to those required by Appendix 3 of Chapter 8B of this Part in order to diagnose the effects considered in clause 2.3.1.1.

2.3.1.2.1 After the approval of this plan by the Test Agency, the manufacturer shall implement those techniques in the OBD system in order to get type approval.

2.3.2. Monitoring requirements concerning particulate after treatment devices

2.3.2.1 The performance of the particulate after treatment device including the filtration and continuous regeneration processes shall be monitored against the OBD threshold limit specified in clause 3.2.2 below.

2.3.2.2 In the case of a wall flow diesel particulate filter (DPF), the manufacturer may choose to apply the performance monitoring requirements set out in Appendix 8 of Chapter 8B of this Part instead of the requirements of clause 2.3.2.1, if he can demonstrate with technical documentation that in case of deterioration there is a positive correlation between the loss of filtration efficiency and the loss of pressure drop ("delta pressure") across the DPF under the operating conditions of the engine specified in the test described in Appendix 8 of Chapter 8B of this Part.

2.4. Alternative Approval

2.4.1. If requested by the manufacturer, for vehicles of categories M2 and N1, for vehicles of categories M1 and N2 with a technically permissible maximum laden mass not exceeding 7.5 tonnes, and for vehicles of category M3 of Type-I and Type-II (as defined in AIS-052) with a permissible mass not exceeding 7.5 tonnes, compliance with the requirements of Chapter 14 of AIS-137(Part 3) shall be considered equivalent to the compliance with this Chapter

2.4.1.1 If such alternative approval is used, the information related to OBD systems shall be as per AIS-137 (Part 3).

2.4.1.2 The equivalence set out in clauses 2.4.1 shall apply in the following manner

2.4.1.2.1 The requirements on NO_x control measures described in clauses 2.1.2.2.1. to 2.1.2.2.4. of Chapter 10 of this Part shall apply.

2.4.2 As an alternative to the requirements set out in clause 4. of Chapter 8B of this Part and those described in this Chapter, engine manufacturers whose annual production of engines within an engine type subject to this Part is less than 250 engines per year, may obtain type approval on the basis of the requirements of this Part when the emission control components of the engine-system are at least monitored for circuit continuity, and for rationality and plausibility of sensor outputs, and when the after-treatment system is at least monitored for total functional failure. Engine manufacturers whose annual production of engines within an engine type subject to this Part is less than 50 engines per year, may obtain type approval on the basis of the requirements of this Part when the emission control components of the engine system are at least monitored for circuit continuity, and for rationality and plausibility of sensor outputs ("component monitoring").

A manufacturer shall not be permitted to use the alternative provisions specified in this clause for more than 250 engines per year.

2.4.3 The Test Agencies shall inform the other Test Agencies of the circumstances of each type approval granted under clause 2.4.1 and clause 2.4.2 of this Chapter.

2.5. Conformity of production

The OBD system is subject to the requirements for conformity of production specified in clause 8.6 of Chapter 1 of this Part.

If the Test Agency decides that verification of the conformity of production of the OBD system is required, the verification shall be conducted in accordance with the requirements specified in clause 8.6 of Chapter 1 of this Part.

3.0 PERFORMANCE REQUIREMENTS

3.1. The performance requirements shall be those set out in clause 5 of Chapter 8B of this Part.

3.2. OBD Threshold Limits

3.2.1. The OBD threshold limits (hereinafter OTLs) applicable to the OBD system are those specified in Gazette Notification GSR-889 (E) dated 16th September 2016 published by Ministry of Road Transport and Highways (MoRTH).

- 3.2.2. The vehicles shall be equipped with an On-Board Diagnostic system for emission control which shall have the capability of identifying the likely area of the malfunctions by means of fault codes stored in computer memory and communicating that information off-board, as per procedure described in this Part, when that failure results in an increase in emission above the limits as given in Table 1 or Table 2 below (as applicable) as notified in the Gazette Notification GSR-889(E) dated 16th September 2016 published by MoRTH. The implementation dates for BS-VI-OBD-I and BS-VI-OBD-II shall be as specified in Gazette Notification GSR-889(E) dated 16th September 2016 published by Ministry of Road Transport and Highways (MoRTH).

At the manufacturer's request type approval may be granted for compliance to BS-VI OBD-II requirements before its implementation.

Table 1
OBD Threshold Limits: (BS-VI OBD-I)

	Limit in mg/kWh		
	NOx	PM Mass	
Compression Ignition Engine	1500	Performance monitoring	
Positive Ignition Engine	1500	-----	

Table 2
OBD Threshold Limits: (BS-VI OBD-II)

	Limit in mg/kWh		
	NOx	PM Mass	CO
Compression Ignition Engine	1200	25	----
Positive Ignition Engine	1200	-----	7500

4.0 DEMONSTRATION REQUIREMENTS

- 4.1. The demonstration requirements and test procedures shall be those set out in clauses 6 and 7 of Chapter 8B of this Part.

5.0 DOCUMENTATION REQUIREMENTS

- 5.1. The documentation requirements shall be those set out in clause 8 of Chapter 8B of this Part.

6.0 IN USE PERFORMANCE REQUIREMENTS

The requirements of this clause shall apply to the OBD system monitors in accordance with the provisions of Chapter 8C of this Part. This requirement shall be applicable from the date 1st April 2023 as specified in Gazette Notification GSR 889(E) dated 16th September 2016.

6.1 Technical Requirements

6.1.1 The requirements of this clause shall apply to the OBD system monitors in accordance with the provisions of Chapter 8C of this Part. This requirement shall be applicable from the date 1st April 2023 as specified in Gazette Notification GSR 889 (E) dated 16th September 2016.

6.1.2 In particular, the in-use performance ratio (IUPR_m) of a specific monitor *m* of the OBD system shall be calculated by the following formula:

$$\text{IUPR}_m = \text{Numerator}_m / \text{Denominator}_m$$

where

‘Numerator_m’ means the numerator of a specific monitor *m* and is a counter indicating the number of times a vehicle has been operated in such a way that all monitoring conditions necessary for that specific monitor to detect a malfunction have been encountered;

and

‘Denominator_m’ means the denominator of a specific monitor *m* and is a counter indicating the number of vehicle driving cycles that are of relevance to that specific monitor [or, “in which events occur that are of relevance to that specific monitor.”].

6.1.3 The in-use performance ratio (IUPR_g) of a group *g* of monitors on board of a vehicle is calculated by the following formula:

$$\text{IUPR}_g = \text{Numerator}_g / \text{Denominator}_g$$

where

‘**Numerator_g**’ means the numerator of a group *g* of monitors and is the actual value (Numerator_m) of the specific monitor *m* that has the lowest in-use performance ratio as defined in clause 6.1.2 of this Chapter of all monitors within that group *g* of monitors on board of a particular vehicle;

‘**Denominator_g**’ means the denominator of a group *g* of monitors and is the actual value (Denominator_m) of the specific monitor *m* that has the lowest in-use performance ratio as defined in clause 6.1.2 of this Chapter of all monitors within that group *g* of monitors on board of a particular vehicle.

6.2. Minimum In-Use Performance Ratio

6.2.1. The in-use performance ratio IUPR_m of a monitor *m* of the OBD system as defined in clause 5 of Chapter 8C of this Part, shall be greater than or equal to the minimum in-use-performance ratio IUPR_m(min) applicable to the monitor *m* throughout the useful life of the engine as specified in clause 5.4 of Chapter 1 of this Part.

6.2.2. The value of minimum in-use-performance ratio IUPR (min) is 0.1 for all monitors.

6.2.3. The requirement of clause 6.2.1 of this Chapter is deemed to be fulfilled if for all groups of monitor's g the following conditions are met:

6.2.3.1. The average value of the values IUPR_g of all vehicles equipped with engines belonging to the OBD engine family under consideration is equal to or above IUPR (min), and

6.2.3.2. More than 50% of all engines considered in clause 6.2.3.1. of this Chapter have an IUPR_g equal to or above IUPR(min).

6.3 Documentation Requirements

6.3.1 The documentation associated with each monitored component or system and required by clause 8 of Chapter 8B of this Part shall include the following information concerning in-use performance data:

- (a) The criteria used for incrementing the numerator and the denominator;
- (b) Any criterion for disabling incrementation of the numerator or of the denominator.

6.3.1.1 Any criterion for disabling incrementation of the general denominator shall be added to the documentation referred to in clause 6.3.1. of this Chapter.

6.4. Statement of OBD in-use Performance compliance

6.4.1. In the application for type approval, the manufacturer shall provide a statement of OBD in-use Performance compliance in accordance with the format set out in Appendix 2 of this Chapter. In addition to this statement, compliance with the requirements of clause 6.1 of this Chapter shall be verified through the additional assessment rules specified in clause 6.5. of this Chapter.

6.4.2. This statement referred to in clause 6.4.1 of this Chapter shall be attached to the documentation related to the OBD engine-family required by clause 5 and 6.3 of this Chapter.

6.4.3. The manufacturer shall maintain records which contain all test data, engineering and manufacturing analyses, and other information which provides the basis for the OBD in-use performance compliance statement. The manufacturer shall make such information available to the Test Agency upon request.

6.4.4. During the phase-in period (from BSVI - OBD-I to BS-VI-OBD-II) set out in clause 4.10.7 of Chapter 1 of this Part, the manufacturer shall be exempted from providing the statement required by clause 6.4.1. of this Chapter.

6.5. Assessment of the in-use performance

6.5.1. The OBD in-use performance and compliance with clause 6.2.3 of this Chapter shall be demonstrated at least according to the procedure set out in Appendix 1 of this Chapter.

- 6.5.2. Test Agencies may pursue further in-use performance surveys to verify compliance with clause 6.2.3 of this Chapter.
- 6.5.2.1 To demonstrate non-compliance with the requirements of clause 6.2.3 of this Chapter, based on the provision of clause 6.5.2 of this Chapter, the Test Agencies must show for at least one of the requirements of clause 6.2.3 of this Chapter non-compliance with a statistical confidence level of 95%, based on a sample of at least 30 vehicles.
- 6.5.2.2 The manufacturer shall have the opportunity to establish compliance with the requirements of clause 6.2.3 of this Chapter, for which non-compliance was demonstrated according to clause 6.5.2.1 of this Chapter, by using a survey based on a sample of at least 30 vehicles, with a better statistical confidence than the test mentioned in clause 6.5.2.1.
- 6.5.2.3 For tests performed according to clauses 6.5.2.1 and 6.5.2.2 both Test Agencies and manufacturers must disclose relevant details, such as those relating to the selection of the vehicles, to the other party.
- 6.5.3 If non-compliance with the requirements of clause 6.2.3 of this Chapter is established according to clauses 6.5.1 or 6.5.2. of this Chapter, remedial measures in accordance with clause 9.3 of Chapter 1 of this Part shall be taken.

CHAPTER 8A - APPENDIX 1

ASSESSMENT OF THE IN-USE PERFORMANCE OF THE ON-BOARD DIAGNOSTIC SYSTEM

1.0 GENREAL

1.1 This Appendix sets out the procedure to be followed when demonstrating the OBD in-use performance with regard to the provisions set out in clause 6 of this Chapter.

2.0 PROCEDURE FOR DEMONSTRATING OBD IN-USE PERFORMANCE

2.1. The OBD in-use performance of an engine family shall be demonstrated by the manufacturer to the Test Agency that granted the type-approval for the vehicles or engines concerned. The demonstration shall require consideration of the OBD in-use performance of all OBD engine families within the engine family under consideration (Figure 1 below).

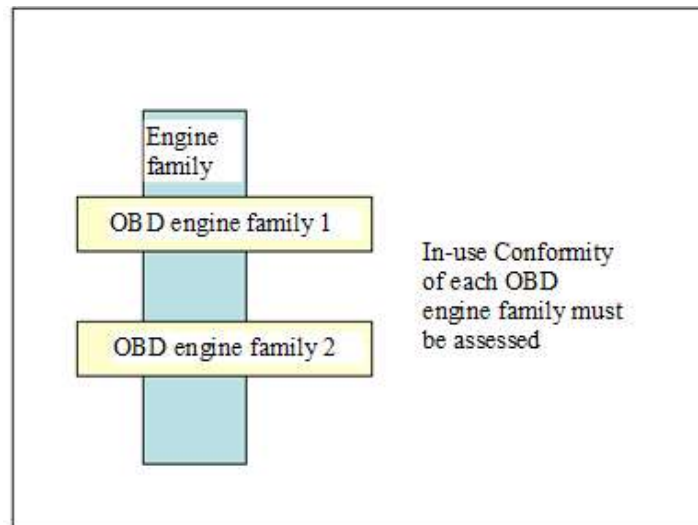


Figure 1

Two OBD Engine Families within one Engine Family

2.1.1. The demonstration of OBD in-use performance shall be organised and conducted by the manufacturer, in close cooperation with the Test Agency.

2.1.2. The manufacturer may use in the demonstration of conformity relevant elements that were used to demonstrate the conformity of an OBD engine family within another engine family provided that this earlier demonstration took place no more than two years before the current demonstration (Figure 2 of this Appendix).

2.1.2.1. A manufacturer may not, however, then use these elements in demonstrating conformity of a third or subsequent, engine family unless each of these demonstrations takes place within two years of the first use of the elements in a demonstration of conformity.

In-use Conformity of each OBD engine family must be assessed

Conformity of OBD engine family 1 may only be demonstrated once

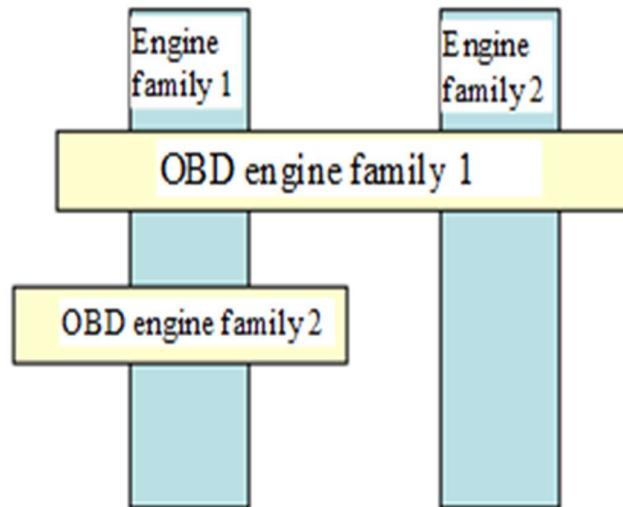


Figure 2

Previously Demonstrated Conformity of an OBD Engine Family

- 2.2. The demonstration of OBD in-use performance shall be performed at the same time and at the same frequency as the in-service conformity demonstration specified in Chapter 7 of this Part.
- 2.3. The manufacturer shall report the initial schedule and the sampling plan for conformity testing to the Test Agency at the time of the initial type approval of a new engine family.
- 2.4. Vehicle types without a communication interface which permits the collection of the necessary in-use performance data as specified in Chapter 8C of this Part, with missing data or with a non-standard data protocol shall be considered as non-compliant.
 - 2.4.1. Individual vehicles with mechanical or electrical faults which prevent the collection of the necessary in-use performance data as specified in Chapter 8C of this Part shall be excluded from the conformity testing survey and the vehicle type shall not be considered non-compliant unless insufficient vehicles that meet the sampling requirements can be found to permit the survey to be properly conducted.
- 2.5. Engine or vehicle types where the collection of in-use performance data influences the OBD monitoring performance shall be considered as non-compliant.

3.0 OBD IN-USE PERFORMANCE DATA

- 3.1.** The OBD in-use performance data to be considered for assessing the conformity of an OBD engine family shall be those recorded by the OBD system according to clause 6 of Chapter 8C of this Part, and made available according to clause 7 of that Chapter of this Part.

4.0 ENGINE OR VEHICLE SELECTION

4.1. Engine Selection

- 4.1.1.** In the case where an OBD engine-family is used in several engine families (Figure 2 of this Appendix), engines from each of these engine families shall be selected by the manufacturer for demonstrating the in-use performance of that OBD engine family.
- 4.1.2.** Any engine of a particular OBD-engine family may be included in the same demonstration even if the monitoring systems with which they are equipped are of different generations or at different modification states.

4.2. Vehicle Selection

4.2.1. Vehicle segments

- 4.2.1.1.** For the purpose of classifying the vehicles subject to demonstration, 6 vehicle segments shall be considered:
- (a) for vehicles of class N: long-haul vehicles, distribution vehicles, and others such as construction vehicles.
 - (b) for vehicles of class M: coaches and inter-city buses, city buses, and others such as M1 vehicles.
- 4.2.1.2.** Where possible, vehicles shall be selected from each segment in a survey.
- 4.2.1.3.** There shall be a minimum of 15 vehicles per segment.
- 4.2.1.4.** In the case where an OBD engine-family is used in several engine families (Figure 2 of this Appendix), the number of engines from each of these engine families within a vehicle segment shall be as representative as possible of their volume share, in terms of vehicles sold and in use, for that vehicle segment.

4.2.2. Vehicle qualification

- 4.2.2.1.** The engines selected shall be fitted to vehicles registered and used in India.
- 4.2.2.2.** Each vehicle selected shall have a maintenance record to show that the vehicle has been properly maintained and serviced in accordance with the manufacturer's recommendations.

- 4.2.2.3. The OBD system shall be checked for proper functioning. Any malfunction indications relevant to the OBD system itself that are stored in the OBD memory shall be recorded and the required repairs shall be carried out.
- 4.2.2.4. The engine and vehicle shall exhibit no indications of abuse such as overloading, misfueling, or other misuse, or other factors such as tampering that could affect the OBD performance. OBD system fault codes and information on operating hours stored in the computer memory shall be amongst the evidence taken into account in determining whether the vehicle has been subject to abuse or is otherwise ineligible for inclusion in a survey.
- 4.2.2.5. All emission control system and OBD components on the vehicle shall be as stated in the applicable type-approval documents.

5.0 IN-USE PERFORMANCE SURVEYS

5.1. Collection of in-use performance data

- 5.1.1. In accordance with the provisions of clause 6, the manufacturer shall retrieve the following information from the OBD system of each vehicle in the survey:
 - (a) The VIN (Vehicle Identification Number);
 - (b) The numerator_g and denominator_g for each group of monitors recorded by the system in accordance with the requirements of clause 6 of Chapter 8C of this Part;
 - (c) The general denominator;
 - (d) The value of the ignition cycle counter;
 - (e) The total engine running hours.
- 5.1.2. The results from the group of monitors under evaluation shall be disregarded if a minimum value of 25 for its denominator has not been reached.
- 5.2. **Assessment of the in-use performance**
 - 5.2.1. The actual performance ratio per group of monitors of an individual engine (IUPR_g) shall be calculated from the numerator_g and denominator_g retrieved from the OBD system of that vehicle.
 - 5.2.2. The assessment of the in-use performance of the OBD engine family in accordance with the requirements of clause 6.5.1 of this Chapter shall be made for each group of monitors within the OBD-engine family considered in a vehicle segment.
 - 5.2.3. For any segment of vehicles defined in clause 4.2.1 of this Appendix, the OBD in-use performance is considered as being demonstrated for the purposes of clause 6.5.1 of this Chapter if, and only if, for any group g of monitors the following conditions are met:

- (a) the average value of the IUPRg values of the considered sample is greater than 88 per cent of IUPR(min); and
- (b) More than 34 per cent of all engines in the considered sample have an IUPRg value of more or equal than IUPR(min).

6.0 REPORT TO THE TEST AGENCY

The manufacturer shall provide the Test Agency with a report on the in-use performance of the OBD engine family that contains the following information:

- 6.1.** The list of the engine families within the considered OBD engine family (Figure 1 of this Appendix).

6.2 The following information concerning the vehicles considered in the demonstration:

- (a) The total number of vehicles considered in the demonstration;
- (b) The number and the type of vehicle segments;
- (c) The VIN, and a short description (type-variant-version) of each vehicle

6.3 In-use performance information for each vehicle:

- (a) The numerator, denominator, and in-use performance ratio (IUPRg) for each group of monitors;
- (b) The general denominator, the value of the ignition cycle counter, the total engine running hours.

6.4 The results of the in-use performance statistics for each group of monitors:

- (a) The average value of the IUPRg values of the sample;
- (b) The number and the percentage of engines in the sample that have an IUPRg equal to or above IUPRm (min).

CHAPTER 8A - APPENDEX 2
MODELS OF AN OBD IN-USE PERFORMANCE COMPLIANCE
STATEMENT

"(Name of manufacturer) attests that the engines within this OBD engine family have been so designed and manufactured as to comply with all requirements of clauses 6.1 and 6.2 of this Chapter.

(Name of manufacturer) makes this statement in good faith, after having performed an appropriate engineering evaluation of the OBD in-use performance of the engines within the OBD engine family over the applicable range of operating and ambient conditions."

[date]

CHAPTER 8B

TECHNICAL REQUIREMENTS FOR ON-BOARD DIAGNOSTIC SYSTEMS

1.0 INTRODUCTION

This Chapter set out the technical requirements of an on-board diagnostic (OBD) system for the control of emission from engine systems.

2.0 RESERVED

3.0 DEFINITIONS

- 3.1. **"Alert system"** means a system on-board the vehicle which informs the driver of the vehicle or any other interested party that the OBD system has detected a malfunction.
- 3.2. **"Test Agency"** means the authority that grants the compliance approval of an OBD system considered by this Chapter. .
- 3.3. **"Calibration verification number"** means the number that is calculated and reported by the engine system to validate the calibration/software integrity.
- 3.4. **"Component monitoring"** means the monitoring of input components for electrical circuit failures and rationality failures and monitoring of output components for electrical circuit failures and functionality failures. It refers to components that are electrically connected to the controller(s) of the engine system.
- 3.5. **"Confirmed and active DTC"** means a DTC that is stored during the time the OBD system concludes that a malfunction exists.
- 3.6. **"Continuous-MI"** means the malfunction indicator showing a steady indication at all times while the key is in the on (run) position with the engine running (ignition on - engine on) or the vehicle starts moving, whichever occurs first, and extinguishing when the key is moved to off."
- 3.7. **"Deficiency"** means an OBD monitoring strategy or other OBD feature that does not meet all the detailed requirements of this Chapter.
- 3.8. **"Diagnostic trouble code (DTC)"** means a numeric or alphanumeric identifier which identifies or labels a malfunction.
- 3.9. **"Electrical circuit failure"** means a malfunction (e.g. open circuit or short circuit) that leads to the measured signal (i.e. voltages, currents, frequencies, etc.) being outside the range where the transfer function of the sensor is designed to operate.
- 3.10. **"Emission OBD family"** means a manufacturer's grouping of engine systems having common methods of monitoring/diagnosing emission-related malfunctions.

- 3.11 **"Emission Threshold Monitoring"** means monitoring of a malfunction that leads to an excess of the OTLs. It consists of:
- (a) Direct emissions measurement via a tailpipe emissions sensor(s) and a model to correlate the direct emissions to test-cycle specific emissions; and/or
 - (b) Indication of an emissions increase via correlation of computer input/output information to test-cycle specific emissions.
- 3.12 **"Engine System"** means the engine as it would be configured when tested for its exhaust emissions on a approval test-bed, including:
- (a) The engine's electronic management controller(s);
 - (b) The exhaust after treatment system(s);
 - (c) Any emission-related component of the engine or the exhaust system which supplies input to, or receives output from, the engine's electronic management controller(s); and
 - (d) The communication interface (hardware and messages) between the engine's electronic management controller(s) and any other power train or vehicle control unit if the exchanged information has an influence on the control of emissions.
- 3.13. **"Functionality failure"** means a malfunction where an output component does not respond to a computer command in the expected way.
- 3.14. **"Malfunction emission control strategy (MECS)"** means a strategy within the engine system that is activated as a result of an emission-related malfunction.
- 3.15. **"Malfunction indicator (MI)"** is an indicator which clearly informs the driver of the vehicle in the event of a malfunction. The MI is part of the alert system (see "continuous-MI", "on-demand-MI", and "short-MI").
- 3.16. **"Malfunction"** means a failure or deterioration of an engine system, including the OBD system, that may lead either to an increase in any of the regulated pollutants emitted by the engine system or to a reduction in the effectiveness of the OBD system.
- 3.17. **"MI status"** means the command status of the MI, being either continuous-MI, Short-MI, on-demand-MI, or off.
- 3.18. **"Monitoring"** (see "emission threshold monitoring", "performance monitoring", and "total functional failure monitoring")
- 3.19. **"OBD test-cycle"** means the cycle over which an engine system is operated on an engine test-bed to evaluate the response of an OBD system to the presence of a qualified deteriorated component.
- 3.20. **"OBD-parent engine system"** means an engine system that has been selected from an emission-OBD family for which most of its OBD elements of design are representative of that family.

- 3.21. **"On-board diagnostic system (OBD)"** means a system on-board a vehicle or engine which has the capability:
- (a) of detecting malfunctions, affecting the emission performance of the engine system;
 - (b) of indicating their occurrence by means of an alert system;
 - (c) of identifying the likely area of the malfunctions by means of information stored in computer memory and/or communicating that information off-board.
- 3.22. **"On-demand-MI"** means the malfunction indicator showing a steady indication in response to a manual demand from the driving position when the key is in the on (run) position with the engine off (ignition on - engine off).
- 3.23. **"Operating sequence"** means a sequence consisting of an engine start-up, an operating period, an engine shut-off, and the time until the next start-up, where a specific OBD monitor runs to completion and a malfunction would be detected if present.
- 3.24. **"Pending DTC"** means a DTC that is stored by the OBD system because a monitor has detected a situation where a malfunction may be present during the current or last completed operating sequence.
- 3.25. **"Performance monitoring"** means malfunction monitoring that consists of functionality checks and monitoring parameters that are not correlated to emission thresholds. Such monitoring is typically done on components or systems to verify that they are operating within the proper range (e.g. differential pressure in case of a DPF).
- 3.26. **"Potential DTC"** means a DTC that is stored by the OBD system because a monitor has detected a situation where a malfunction may be present but requires further evaluation to be confirmed. A potential DTC is a pending DTC which is not a confirmed and active DTC.
- 3.27. **"Previously active DTC"** means a formerly confirmed and active DTC that remains stored after the OBD system has concluded that the malfunction that caused the DTC is no longer present.
- 3.28. **"Qualified deteriorated component or system (QDC)"** means a component or system that has been intentionally deteriorated (e.g. accelerated aging) and/or manipulated in a controlled manner and which has been accepted by the Test Agencies according to the provisions set in this Chapter.
- 3.29. **"Rationality failure"** means a malfunction where the signal from an individual sensor or component is at variance with that expected when assessed against signals available from other sensors or components within the control system. Rationality failures include malfunctions that lead to the measured signal (i.e. voltages, currents, frequencies, etc.) being inside the range where the transfer function of the sensor is designed to operate.

- 3.30. **"Readiness"** means a status indicating whether a monitor or a group of monitors have run since the last erasing by an external request or command (for example through an OBD scan-tool).
- 3.31. **"Scan-tool"** means an external test equipment used for standardized off-board communication with the OBD system in accordance with the requirements of this Chapter.
- 3.32. **"Short-MI"** means the malfunction indicator showing a 15 second steady indication from the time the key is moved to on (run) position and the engine is started (ignition on - engine on) or the vehicle starts moving, and extinguishing after these 15 seconds or when the key is moved to off, whichever occurs first.
- 3.33. **"Software calibration identification"** means a series of alphanumeric characters that identifies the emission-related calibration / software version(s) installed in the engine system.
- 3.34. **"Total functional failure monitoring"** means monitoring a malfunction which is leading to a complete loss of the desired function of a system.
- 3.35. **"Warm-up cycle"** means sufficient engine operation such that the coolant temperature has risen by at least 22 K (22 °C / 40 °F) from engine starting and reaches a minimum temperature of 333 K (60 °C / 140 °F)⁽¹⁾.

⁽¹⁾ This definition does not imply that a temperature sensor is necessary to measure the coolant temperature.

3.36. **Abbreviations**

AES	Auxiliary Emission Strategy
CV	Crankcase Ventilation
DOC	Diesel Oxidation Catalyst
DPF	Diesel Particulate Filter or Particulate Trap including catalyzed DPFs and Continuously Regenerating Traps (CRT)
DTC	Diagnostic trouble code
EGR	Exhaust Gas Recirculation
HC	Hydrocarbon
LNT	Lean NO _x Trap (or NO _x absorber)
LPG	Liquefied Petroleum Gas
MECS	Malfunction Emission Control Strategy
NG	Natural Gas
NO _x	Oxides of Nitrogen
OTL	OBD Threshold Limit

PM	Particulate Matter
SCR	Selective Catalytic Reduction
SW	Screen Wipers
TFF	Total Functional Failure monitoring
VGT	Variable Geometry Turbocharger
VVT	Variable Valve Timing

4.0 GENERAL REQUIRMENTS

In the context of this Chapter, the OBD system shall have the capability of detecting malfunctions, of indicating their occurrence by means of a malfunction indicator, of identifying the likely area of the malfunctions by means of information stored in computer memory, and communicating that information off-board.

The OBD system shall be designed and constructed so as to enable it to identify types of malfunctions over the complete life of the vehicle/engine. In achieving this objective, the Test Agency will recognize that engines which have been used in excess of their regulatory useful life may show some deterioration in OBD system performance and sensitivity such that the OBD thresholds may be exceeded before the OBD system signals a malfunction to the driver of the vehicle.

The above paragraph does not extend the engine manufacturer's compliance liability for an engine beyond its regulated useful life (i.e. the time or distance period during which emission standards or emission limits continue to apply).

4.1 Application for approval of an OBD system.

4.1.1 Primary Approval

The manufacturer of an engine system may apply for the approval of its OBD system in one of the three following manners:

- (a) The manufacturer of an engine system applies for the approval of an individual OBD system by demonstrating that OBD system complies with all the provisions of this Chapter.
- (b) The manufacturer of an engine system applies for the approval of an emission-OBD family by demonstrating that the OBD-parent engine system of the family complies with all the provisions of this Chapter.
- (c) The manufacturer of an engine system applies for the approval of an OBD system by demonstrating that OBD system meets the criteria for belonging to an emission-OBD family that has already been certified.

4.1.2 **Extension /Modification of an Existing Certificate**

4.1.2.1 **Extension to include a New Engine System into an Emission-OBD Family**

At the request of the manufacturer and upon approval of the Test Agency, a new engine system may be included as a member of a certified emission-OBD family if all the engine systems within the so-extended emission-OBD family still have common methods of monitoring / diagnosing emission-related malfunctions.

If all OBD elements of design of the OBD-parent engine system are representative of those of the new engine system, then the OBD-parent engine system shall remain unchanged and the manufacturer shall modify the application document according to clause 8 of this Chapter.

If the new engine system contains elements of design that are not represented by the OBD-parent engine system but itself would represent the whole family, then the new engine system shall become the new OBD-parent engine system. In this case the new OBD elements of design shall be demonstrated to comply with the provisions of this Chapter, and the documentation package shall be modified according to clause 8. of this Chapter.

4.1.2.2 **Extension to Address a Design Change that affects the OBD System**

At the request of the manufacturer and upon approval of the Test Agency, an extension of an existing certificate may be granted in the case of a design change of the OBD system if the manufacturer demonstrates that the design changes comply with the provisions of this Chapter.

The documentation package shall be modified according to clause 8. of this Chapter.

If the existing certificate applies to an emission-OBD family, the manufacturer shall justify to the Test Agency that the methods of monitoring/diagnosing emission-related malfunctions are still common within the family and that the OBD-parent engine system remains representative of the family.

4.1.2.3 **Certificate Modification to Address A Malfunction Reclassification.**

This clause applies when, following a request by the Test Agency that granted the approval, or at its own initiative, the manufacturer applies for a modification of an existing certificate in order to reclassify one or several malfunctions.

The compliance of the new classification shall then be demonstrated according to the provisions of this Chapter and the documentation package shall be modified according to clause 8 of this Chapter.

4.2 Monitoring Requirements

All emission-related components and systems included in an engine system shall be monitored by the OBD system in accordance with the requirements set in Appendix 3 of this Chapter and in the case of dual fuel engines or vehicles in clause 7 of Chapter 14 of this Part. However, the OBD system is not required to use a unique monitor to detect each malfunction referred to in Appendix 3 of this Chapter and in the case of dual fuel engines or vehicles in clause 7 of Chapter 14 of this Part.

The OBD system shall also monitor its own components.

The items of Appendix 3 of this Chapter list the systems or components required to be monitored by the OBD system and describes the types of monitoring expected for each of these components or systems (i.e. emission threshold monitoring, performance monitoring, total functional failure monitoring, or component monitoring).

The manufacturer can decide to monitor additional systems and components.

4.2.1 Selection of the Monitoring Technique

Test Agencies may approve a manufacturer's use of another type of monitoring technique than the one mentioned in Appendix 3 of this Chapter or in the case of dual fuel engines or vehicles in clause 7 of Chapter 14 of this Part. The chosen type of monitoring shall be shown by the manufacturer, to be robust, timely and efficient (i.e. through technical considerations, test results, previous agreements, etc.).

In case a system and/or component is not covered by Appendix 3 of this Chapter or in the case of dual fuel engines or vehicles in clause 7 of Chapter 14 of this Part the manufacturer shall submit for approval to the Test Agency an approach to monitoring. The Test Agency will approve the chosen type of monitoring and monitoring technique (i.e. emission threshold monitoring, performance monitoring, total functional failure monitoring, or component monitoring) if it has been shown by the manufacturer, by reference to those detailed in Appendix 3 of this Chapter or in the case of dual fuel engines or vehicles in clause 7 of Chapter 14 of this Part to be robust, timely and efficient (i.e. through either technical considerations, test results, previous agreements, etc.).

4.2.1.1 Correlation to Actual Emissions

In the case of emission threshold monitoring, a correlation to test-cycle specific emissions shall be required. This correlation would typically be demonstrated on a test engine in a laboratory setting.

In all other monitoring cases (i.e. performance monitoring, total functional failure monitoring, or component monitoring), no correlation to actual emissions is necessary. However, the Test Agency may request test data to verify the classification of the

malfunction effects as described in clause 6.2. of this Chapter.

Examples:

An electrical malfunction may not require a correlation because this is a yes/no malfunction. A DPF malfunction monitored via delta pressure may not require a correlation because it anticipates a malfunction.

If the manufacturer demonstrates, according to the demonstration requirements of this Chapter, that emissions would not exceed the OBD threshold limits upon total failure or removal of a component or system, a performance monitoring of this component or system shall be accepted.

When a tailpipe emission sensor is used for monitoring the emissions of a specific pollutant all other monitors may be exempted from further correlation to the actual emissions of that pollutant. Nevertheless, such exemption shall not preclude the need to include these monitors, using other monitoring techniques, as part of the OBD system as the monitors are still needed for the purpose of malfunction isolation.

A malfunction shall always be classified according to clause 4.5. of this Chapter based on its impact on emissions, regardless of the type of monitoring used to detect the malfunction.

4.2.2 **Component monitoring (input/output components/systems)**

In the case of input components that belong to the engine system, the OBD system shall at a minimum detect electrical circuit failures and, where feasible, rationality failures.

The rationality failure diagnostics shall then verify that a sensor output is neither inappropriately high nor inappropriately low (i.e. there shall be "two-sided" diagnostics).

To the extent feasible, and with the agreement of the Test Agency, the OBD system shall detect separately, rationality failures (e.g. inappropriately high and inappropriately low), and electrical circuit failures (e.g. out-of-range high and out-of-range low). Additionally, unique DTCs for each distinct malfunction (e.g. out-of-range low, out-of-range high and rationality failure) shall be stored.

In the case of output components that belong to the engine system, the OBD system shall at a minimum detect electrical circuit failures, and, where feasible, if the proper functional response to computer commands does not occur.

To the extent feasible, and with the agreement of the Test Agency, the OBD system shall detect separately functionality failures, electrical circuit failures (e.g. out-of-range high and out-of-range low) and store unique DTCs for each distinct malfunction (e.g. out-of-range low, out-of-range high, functionality failure).

The OBD system shall also perform rationality monitoring on the information coming from or provided to components that do not belong to the engine system when this information compromises the emission control system and/or the engine system for proper performance.

4.2.2.1 **Exception to Component Monitoring**

Monitoring of electrical circuit failures, and to the extent feasible, functionality, and rationality failures of the engine system shall not be required if all the following conditions are met:

- (a) The failure results in an emission increase of any pollutant of less than 50 per cent of the regulated emission limit, and
- (b) The failure does not cause any emission to exceed the regulated emission limit ⁽¹⁾, and
- (c) The failure does not affect a component or system enabling the proper performance of the OBD system, and
- (d) The failure does not substantially delay or affect the ability of the emission control system to operate as originally designed (for example a breakdown of the reagent heating system under cold conditions cannot be considered as an exception).

Determination of the emissions impact shall be performed on a stabilized engine system in an engine dynamometer test cell, according to the demonstration procedures of this Chapter.

When such a demonstration would not be conclusive regarding criterion (d), the manufacturer shall submit to the Test Agency appropriate design elements such as good engineering practice, technical considerations, simulations, test results, etc.

- (1) The measured value shall be considered taking into account the relevant precision tolerance of the test cell system and the increased variability in the test results due to the malfunction.

4.2.3 **Monitoring Frequency**

Monitors shall run continuously, at any time where the monitoring conditions are fulfilled, or once per operating sequence (e.g. for monitors that lead to an increase of emission when it runs).

At the request of the manufacturer, the Test Agency may approve monitors that do not run continuously. In that case the manufacturer shall clearly inform the Test Agency and describe the conditions under which the monitor runs and justify the proposal by appropriate design elements (such as good engineering practice).

The monitors shall run during the applicable OBD test-cycle as specified in clause 7.2.2. of this Chapter.

A monitor shall be regarded as running continuously, if it runs at a rate not less than twice per second and concludes the presence or the absence of the failure relevant to that monitor within 15 seconds. If a computer input or output component is sampled less frequently than one sample per second for engine control purpose, a monitor shall also be regarded as running continuously, if the system concludes the presence or the absence of the failure relevant to that monitor each time sampling occurs.

For components or systems monitored continuously, it is not required to activate an output component/system for the sole purpose of monitoring that output component/system.

4.3 Requirements for Recording OBD Information

When a malfunction has been detected but is not yet confirmed, the possible malfunction shall be considered as a "Potential DTC" and accordingly a "Pending DTC" status shall be recorded. A "Potential DTC" shall not lead to an activation of the alert system according to clause 4.6. of this Chapter.

Within the first operating sequence, a malfunction may be directly considered "confirmed and active" without having been considered a "potential DTC". It shall be given the "Pending DTC" and a "confirmed and active DTC" status.

In case a malfunction with the previously active status occurs again, that malfunction may at the choice of manufacturer be directly given the "Pending DTC" and "confirmed and active DTC" status without having been given the "potential DTC" status. If that malfunction is given the potential status, it shall also keep the previously active status during the time it is not yet confirmed or active.

The monitoring system shall conclude whether a malfunction is present before the end of the next operating sequence following its first detection. At this time, a "confirmed and active" DTC shall be stored and the alert system be activated according to clause 4.6. of this Chapter.

In case of a recoverable MECS (i.e. the operation automatically returns to normal and the MECS is de-activated at the next engine ON), a "confirmed and active" DTC need not be stored unless the MECS is again activated before the end of the next operating sequence. In case of a non-recoverable MECS, a "confirmed and active" DTC shall be stored as soon as the MECS is activated.

In some specific cases where monitors need more than two operating sequences to accurately detect and confirm a malfunction (e.g. monitors using statistical models or with respect to fluid consumption on the vehicle), the Test Agency may permit the use of more than two operating sequences for monitoring provided the manufacturer justifies the need for the longer period (e.g. by technical rationale, experimental results, in house experience, etc.).

When a confirmed and active malfunction is no longer detected by the system during a complete operating sequence, it shall be given the previously active status by the start of the next operating sequence and keep that status until the OBD information associated with this malfunction is erased by a scan tool or erased from the computer memory according to clause 4.4. of this Chapter.

Note: The requirements prescribed in this clause are illustrated in Appendix 2 of this Chapter.

4.4 Requirements for erasing OBD information

DTC and the applicable information (inclusive the associated freeze frame) shall not be erased by the OBD system itself from the computer memory until that DTC has been in the previously active status for at least 40 warm-up cycles or 200 engine operating hours, whichever occurs first. The OBD system shall erase all the DTCs and the applicable information (inclusive the associated freeze frame) upon request of a scan tool or a maintenance tool.

4.5 Requirements for malfunction classification

Malfunction classification specifies the class to which a malfunction is assigned when such a malfunction is detected, according to the requirements of clause 4.2. of this Chapter.

A malfunction shall be assigned to one class for the actual life of the vehicle unless the Test Agency that granted the certificate or the manufacturer determines that reclassification of that malfunction is necessary.

If a malfunction would result in a different classification for different regulated pollutant emissions or for its impact on other monitoring capability, the malfunction shall be assigned to the class that takes precedence in the discriminatory display strategy (for example Class A takes precedence over Class B1).

If an MECS is activated as a result of the detection of a malfunction, this malfunction shall be classified based on either the emission impact of the activated MECS or its impact on other monitoring capability. The malfunction shall then be assigned to the class that takes precedence in the discriminatory display strategy.

4.5.1 Class A Malfunction

A malfunction shall be identified as Class A when the relevant OBD threshold limits (OTLs) are assumed to be exceeded.

It is accepted that the emissions may still remain below the OTLs when this class of malfunction occurs.

4.5.2 Class B1 Malfunction

A malfunction shall be identified as Class B1 where circumstances exist that have the potential to lead to emissions being above the OTLs but for which the exact influence on emission cannot be estimated and thus the actual emissions according to circumstances may be above or below the OTLs.

Examples of Class B1 malfunctions may include malfunctions detected by monitors that infer emission levels based on readings of sensors or restricted monitoring capability.

Class B1 malfunctions shall include malfunctions that restrict the ability of the OBD system to carry out monitoring of Class A or B1 malfunctions.

4.5.3 **Class B2 Malfunction**

A malfunction shall be identified as Class B2 when circumstances exist that are assumed to influence emissions but not to a level that exceeds the OTL.

Malfunctions that restrict the ability of the OBD system to carry out monitoring of Class B2 malfunctions shall be classified into Class B1 or B2.

4.5.4 **Class C Malfunction**

A malfunction shall be identified as Class C when circumstances exist that, if monitored, are assumed to influence emissions but to a level that would not exceed the regulated emission limits.

Malfunctions that restrict the ability of the OBD system to carry out monitoring of Class C malfunctions shall be classified into Class B1 or B2.

4.6 **Alert System**

The failure of a component of the alert system shall not cause the OBD system to stop functioning.

4.6.1 **MI Specification**

The malfunction indicator shall be perceptible by the driver from the driver's seat position under all lighting conditions. The malfunction indicator shall comprise a yellow or amber warning signal identified by the 0640 symbol in accordance with ISO Standard 7000:2004.

4.6.2 **MI Illumination Schemes**

Depending on the malfunction(s) detected by the OBD system, the MI shall be illuminated according to one of the activation modes described in the following Table:

	Activation mode 1	Activation mode 2	Activation mode 3	Activation mode 4
Conditions of activation	No malfunction	Class C malfunction	Class B malfunction and B1 counters < 200 h	Class A malfunction or B1 counter > 200 h
Key on engine on	No display	Discriminatory display strategy	Discriminatory display strategy	Discriminatory display strategy
Key on engine off	Harmonized display strategy	Harmonized display strategy	Harmonized display strategy	Harmonized display strategy

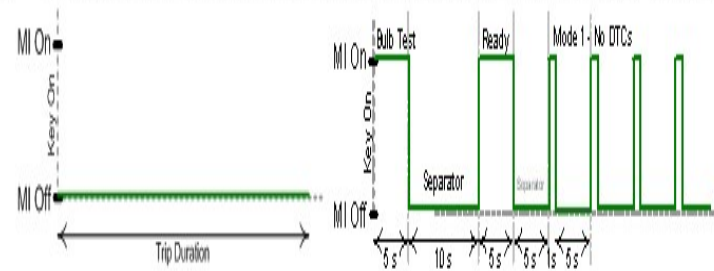
The display strategy requires the MI to be activated according to the class in which a malfunction has been classified. This strategy shall be locked by software coding that shall not be routinely available via the scan tool.

The MI activation strategy at key on, engine off is described in clause 4.6.4.

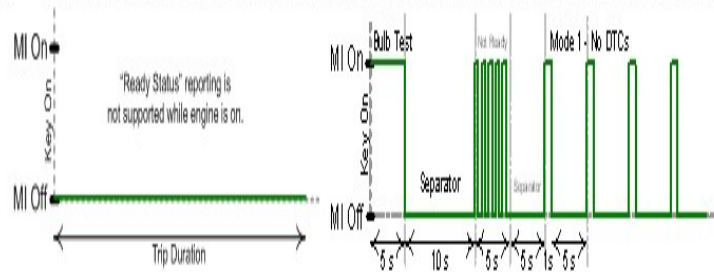
Figures B1 and B2 of this Chapter illustrate the prescribed activation strategies at key on, engine on or off..

ENGINE ON ENGINE OFF

a) MI (bulb) functioning, no malfunction to report, and the readiness of all monitored components "complete".



b) MI (bulb) functioning, no malfunction to report, and at least one component with readiness "not complete".



c) MI (bulb) non operational

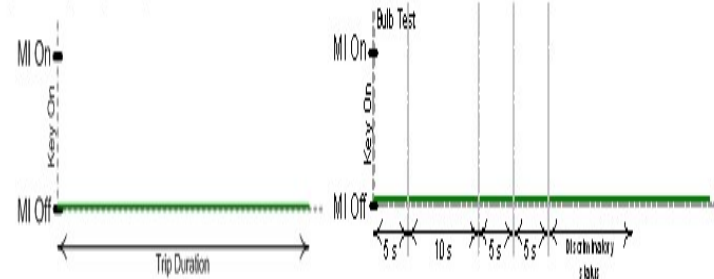


Figure B1
Bulb Test and Readiness Indication

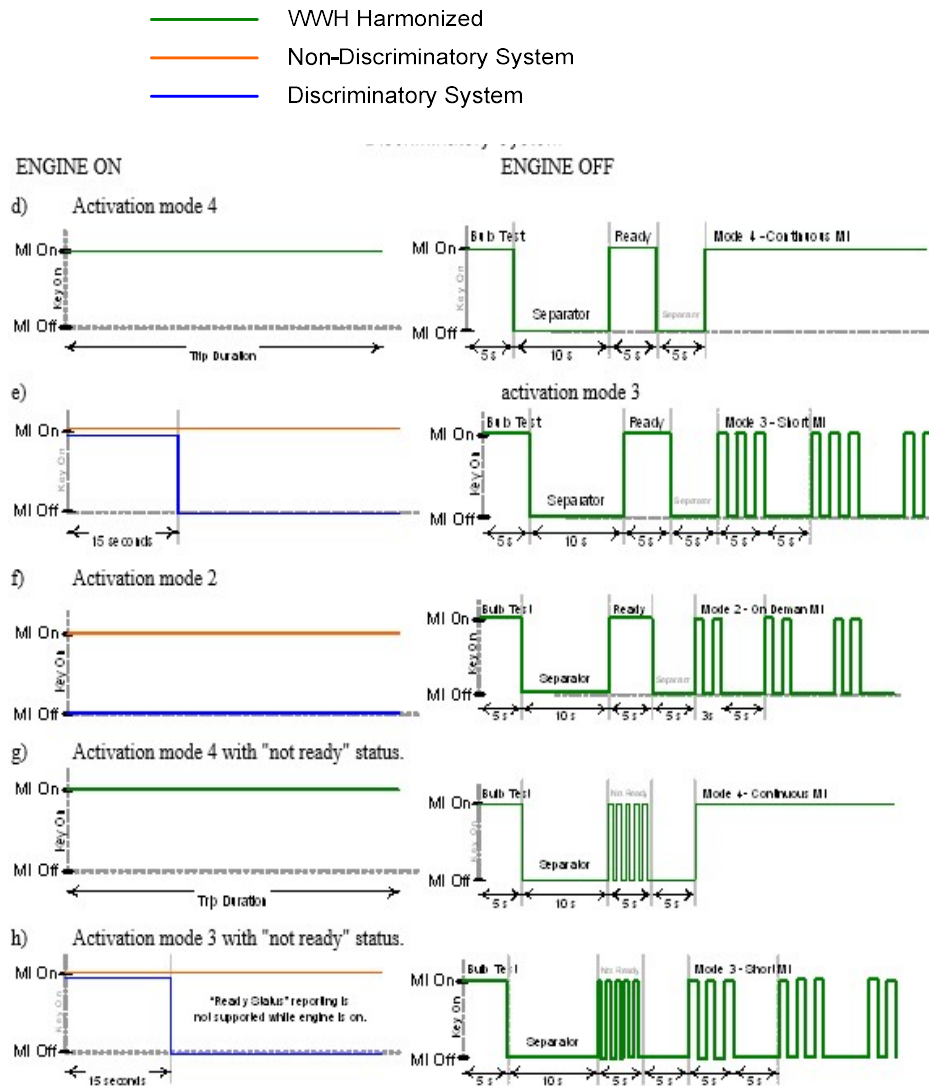


Figure B2

Malfunction Display Strategy: Only the Discriminatory Strategy is Applicable

4.6.3 MI Activation at "engine on"

When the key is placed in the on position and the engine is started (engine on), the MI shall be commanded off unless the provisions of clause 4.6.3.1. of this Chapter have been met.

4.6.3.1 MI Display Strategy

For the purpose of activating the MI, continuous-MI shall take precedence to short-MI and on-demand-MI. For the purpose of activating the MI, short-MI shall take precedence to on-demand-MI.

4.6.3.1.1 Class A malfunctions

The OBD system shall command a continuous-MI upon storage of a confirmed DTC associated with a Class A malfunction.

4.6.3.1.2 **Class B malfunctions**

The OBD system shall command a "short-MI" at the next key-on event following storage of a confirmed and active DTC associated with a Class B malfunction.

Whenever B1 counter reaches to 200h, the OBD system shall command a continuous-MI.

4.6.3.1.3 **Class C malfunctions**

The manufacturer may make available information on Class C malfunctions through the use of an on-demand-MI that shall be available until the engine is started.

4.6.3.1.4 **MI de-activation Scheme**

The "continuous-MI" shall switch to a "short-MI" if a single monitoring event occurs and the malfunction that originally activated the continuous-MI is not detected during the current operating sequence and a continuous-MI is not activated due to another malfunction.

The "short-MI" shall be deactivated if the malfunction is not detected during 3 subsequent sequential operating sequences following the operating sequence when the monitor has concluded the absence of the considered malfunction and the MI is not activated due to another Class A or B malfunction.

Figures 1, 4A and 4B in Appendix 2 of this Chapter illustrate respectively the short and continuous MI deactivation in different use-cases.

4.6.4 **MI activation at key-on/engine-off**

The MI activation at key-on/engine-off shall consist of two sequences separated by a 5 seconds MI off:

- (a) The first sequence is designed to provide an indication of the MI functionality and the readiness of the monitored components;
- (b) The second sequence is designed to provide an indication of the presence of a malfunction.

The first sequence starts from the first time the system is at key-on position and stops either at its normal completion or when the key is set to key-off position, whichever occurs first.

The second sequence is repeated until either the engine is started ⁽¹⁾, the vehicle starts moving, or the key is set to the key-off position, whichever occurs first

⁽¹⁾ An engine may be considered started during the cranking phase.

4.6.4.1. **MI functionality/readiness**

The MI shall show a steady indication for 5 seconds to indicate that the MI is functional.

The MI shall remain at the off position for 10 seconds.

The MI shall then remain at the on position for 5 seconds to indicate that the readiness for all monitored components is complete.

The MI shall blink once per second for 5 seconds to indicate that the readiness for one or more of the monitored components is not complete.

The MI shall then remain off for 5 seconds.

4.6.4.2. **Presence / absence of a malfunction**

Following the sequence described in clause 4.6.4.1, of this Chapter the MI shall indicate the presence of a malfunction by a series of flashes or a continuous illumination, depending on the applicable activation mode, as described in the following clauses, or absence of a malfunction by a series of single flashes. When applicable, each flash consists of a 1s MI-on followed by a 1s MI-off, and the series of flashes will be followed by a period of four seconds with the MI off.

Four activation modes are considered, where activation mode 4 shall take precedence over activation modes 1, 2 and 3, activation mode 3 shall take precedence over activation modes 1 and 2, and activation mode 2 shall take precedence over activation mode 1.

4.6.4.2.1 **Activation mode 1 - absence of malfunction**

The MI shall blink for one flash.

4.6.4.2.2 **Activation mode 2 - "On-demand-MI"**

The MI shall show blink for two flashes if the OBD system would command an on-demand-MI according to the discriminatory display strategy described in clause 4.6.3.1. of this Chapter.

4.6.4.2.3 **Activation mode 3 - "short-MI"**

The MI shall blink for three flashes if the OBD system would command a short-MI according to the discriminatory display strategy described in clause 4.6.3.1. of this Chapter.

4.6.4.2.4 **Activation mode 4 - "Continuous-MI"**

The MI shall remain continuously ON ("continuous-MI") if the OBD system would command a continuous-MI according to the discriminatory display strategy described in clause 4.6.3.1. of this Chapter.

4.6.5. Counters associated with malfunction**4.6.5.1 MI counters****4.6.5.1.1. Continuous-MI Counter**

The OBD system shall contain a continuous-MI counter to record the number of hours during which the engine has been operated while a continuous-MI is activated.

The continuous-MI counter shall count up to the maximum value provided in a 2-byte counter with 1-hour resolution and hold that value unless the conditions allowing the counter to be reset to zero are met.

The continuous-MI counter shall operate as follows:

- (a) If starting from zero, the continuous-MI counter shall begin counting as soon as a continuous-MI is activated;
- (b) The continuous-MI counter shall halt and hold its present value when the continuous-MI is no longer activated;
- (c) The continuous-MI counter shall continue counting from the point at which it had been held if a malfunction that results in a continuous-MI is detected within 3 operating sequences;
- (d) The continuous-MI counter shall start again counting from zero when a malfunction that results in a continuous-MI is detected after 3 operating sequences since the counter was last held;
- (e) The continuous-MI counter shall be reset to zero when:
 - a) No malfunction that results in a continuous-MI is detected during 40 warm up cycles or 200 engine operating hours since the counter was last held whichever occurs first; or
 - ii) The OBD scan tool commands the OBD System to clear OBD information

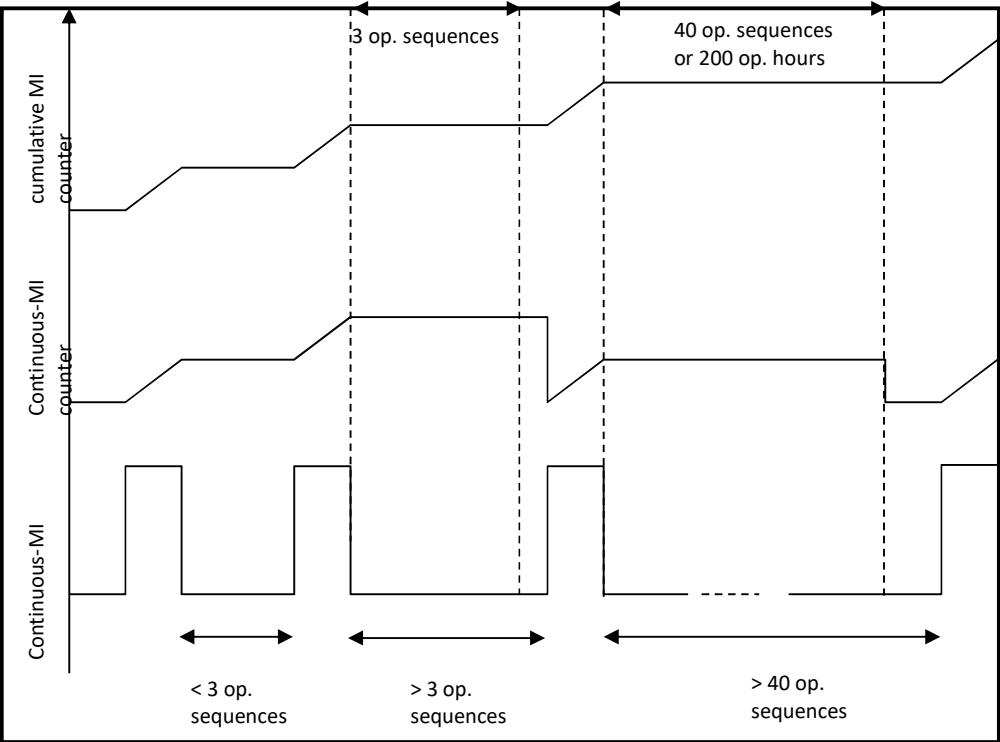


Figure C1
Illustration of the MI Counters Activation Principles

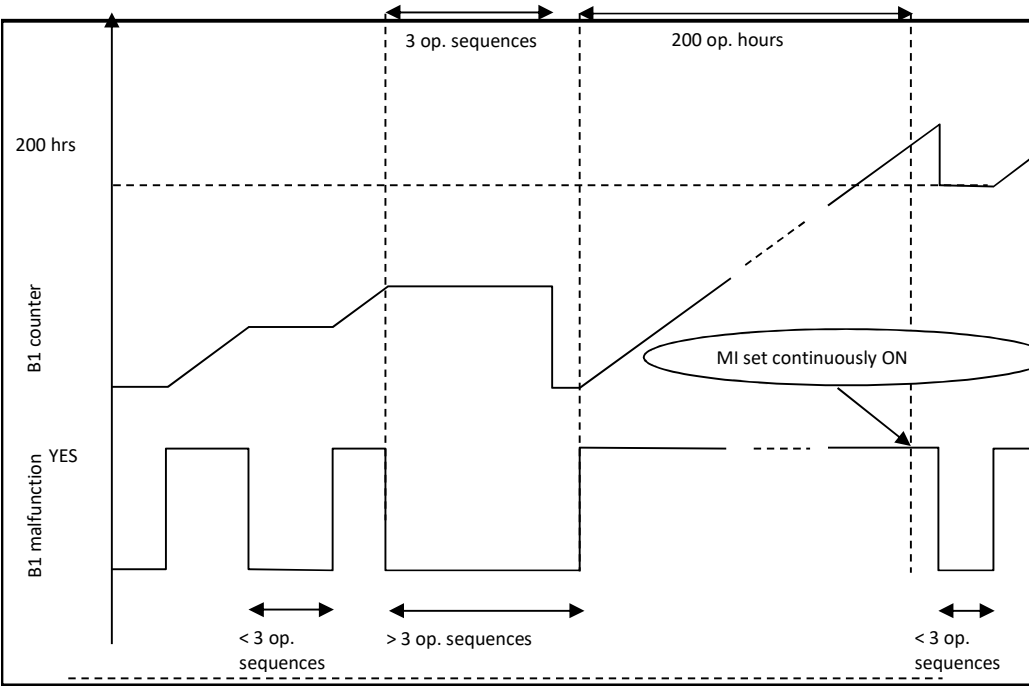


Figure C
Illustration of the B1 Counter Activation Principles

4.6.5.1.2 **Cumulative continuous-MI counter**

The OBD system shall contain a cumulative continuous-MI counter to record the cumulative number of hours during which the internal combustion engine has been operated over its life while a continuous-MI is activated.

The cumulative continuous-MI counter shall count up to the maximum value provided in a 2-byte counter with 1hour resolution and hold that value.

The cumulative continuous-MI counter shall not be reset to zero by the engine system, a scan tool or a disconnection of a battery.

The cumulative continuous-MI counter shall operate as follows:

- (a) The cumulative continuous-MI counter shall begin counting when the continuous-MI is activated.
- (b) The cumulative continuous-MI counter shall halt and hold its present value when the continuous-MI is no longer activated.
- (c) The cumulative continuous-MI counter shall continue counting from the point it had been held when a continuous-MI is activated.

Figure C1 of this Chapter illustrates the principle of the cumulative continuous-MI counter and Appendix 2 of this Chapter contains examples that illustrate the logic.

4.6.5.2 **Counters associated with Class B1 malfunctions**

4.6.5.2.1 **Single B1 -Counter**

The OBD system shall contain a B1 counter to record the number of hours during which the internal combustion engine has operated while a Class B1 malfunction is present.

The B1 counter shall operate as follows:

- (a) The B1 counter shall begin counting as soon as a Class B1 malfunction is detected and a confirmed and active DTC has been stored.
- (b) The B1 counter shall halt and hold its present value if no Class B1 malfunction is confirmed and active, or when all Class B1 malfunction have been erased by a scan tool.
- (c) The B1 counter shall continue counting from the point it had been held if a subsequent Class B1 malfunction is detected within 3 operating sequences.

In the case where the B1 counter has exceeded 200 engine running hours, the OBD system shall set the counter to 190 engine running hours when the OBD system has determined that a Class B1 malfunction is no longer confirmed and active, or when all Class B1

malfunctions have been erased by a scan tool. The B1 counter shall begin counting from 190 engine running hours if a subsequent Class B1 malfunction is present within 3 operating sequences.

The B1 counter shall be reset to zero when three consecutive operating sequences have occurred during which no Class B1 malfunctions have been detected.

(Note: The B1 counter does not indicate the number of engine running hours with a single Class B1 malfunction present.)

The B1 counter may accumulate the number of hours of 2 or more different Class B1 malfunctions, none of them having reached the time the counter indicates.

The B1 counter is only intended to determine when the continuous-MI shall be activated.

Figure C2 of this Chapter illustrates the principle of the B1 counter and Appendix 2 of this Chapter contains examples that illustrate the logic.

4.6.5.2.2 **Multiple B1-counters**

A manufacturer may use multiple B1 counters. In that case the system shall be capable of assigning a specific B1 counter to each class B1 malfunction.

The control of the specific B1 counter shall follow the same rules as the single B1 counter, where each specific B1 counter shall begin counting when the assigned Class B1 malfunction is detected.

4.7 **OBD Information**

4.7.1 **Recorded Information**

The information recorded by the OBD system shall be available upon off-board request in the following packages manner:

- (a) Information about the engine state;
- (b) Information about active emission-related malfunctions;
- (c) Information for repair.

4.7.1.1 **Information about the engine state**

This information will provide an enforcement agency⁽¹⁾ with the malfunction indicator status and associated data (e.g. continuous-MI counter, readiness).

The OBD system shall provide all information (according to the applicable standard set in Appendix 6) for the external roadside check test equipment to assimilate the data and provide an enforcement agent with the following information:

- (a) Discriminatory/non-discriminatory display strategy;
- (b) The VIN (vehicle identification number);
- (c) Presence of a continuous-MI;
- (d) The readiness of the OBD system;
- (e) The number of engine operating hours during which a continuous-MI was last activated (continuous-MI counter).

This information shall be read only access (i.e. no clearing).

- 1) A typical use of this information package may be to establish basic emission road worthiness of the engine system.

4.7.1.2 **Information about active emission-related malfunctions**

This information will provide any inspection station⁽²⁾ with a subset of engine related OBD data including the malfunction indicator status and associated data (MI counters), a list of active/confirmed malfunctions of classes A and B and associated data (e.g. B1-counter).

The OBD system shall provide all information (according to the applicable standard set in Appendix 6 of this Chapter) for the external inspection test equipment to assimilate the data and provide an inspector with the following information:

- (a) Type approval marking;
- (b) Discriminatory/ non-discriminatory display strategy;
- (c) The VIN (vehicle identification number);
- (d) The Malfunction Indicator status;
- (e) The Readiness of the OBD system;
- (f) Number of warm-up cycles and number of engine operating hours since recorded OBD information was last cleared;
- (g) The number of engine operating hours during which a continuous-MI was last activated (continuous-MI counter);
- (h) The cumulated operating hours with a continuous-MI (cumulative continuous-MI counter);
- (i) The value of the B1 counter with the highest number of engine operating hours;
- (j) The confirmed and active DTCs for Class A malfunctions;
- (k) The confirmed and active DTCs for Classes B (B1 and B2) malfunctions;
- (l) The confirmed and active DTCs for Class B1 malfunctions;
- (m) The software calibration identification(s);
- (n) The calibration verification number(s).

This information shall be read only access (i.e. no clearing).

⁽²⁾ A typical use of this information package may be to establish detailed understanding of the emission road worthiness of the engine system.

4.7.1.3 Information for Repair

This information will provide repair technicians with all OBD data specified in this Chapter (e.g. freeze frame information).

The OBD system shall provide all information (according to the applicable standard set in Appendix 6 of this Chapter) for the external repair test equipment to assimilate the data and provide a repair technician with the following information:

- (a) Type Approval Marking;
- (b) VIN (vehicle identification number);
- (c) Malfunction indicator status;
- (d) Readiness of the OBD system;
- (e) Number of warm-up cycles and number of engine operating hours since recorded OBD information was last cleared;
- (f) Monitor status (i.e. disabled for the rest of this drive cycle complete this drive cycle, or not complete this drive cycle) since last engine shut-off for each monitor used for readiness status;
- (g) Number of engine operating hours since the malfunction indicator has been activated (continuous MI counter);
- (h) Confirmed and active DTCs for Class A malfunctions;
- (i) Confirmed and active DTCs for Classes B (B1 and B2) malfunctions;
- (j) Cumulated operating hours with a continuous-MI (cumulative continuous-MI counter);
- (k) Value of the B1 counter with the highest number of engine operating hours;
- (l) Confirmed and active DTCs for Class B1 malfunctions and the number of engine operating hours from the B1-counter(s);
- (m) Confirmed and active DTCs for Class C malfunctions;
- (n) Pending DTCs and their associated class;
- (o) Previously active DTCs and their associated class;
- (p) Real-time information on OEM selected and supported sensor signals, internal and output signals (see clause 4.7.2 and Appendix 5 of this Chapter);
- (q) Freeze frame data requested by this Chapter (see clause 4.7.1.4. and Appendix 5 of this Chapter);
- (r) Software calibration identification(s)
- (s) Calibration verification number(s).

The OBD system shall clear all the recorded malfunctions of the engine system and related data (operating time information, freeze frame, etc.) in accordance with the provisions of this Chapter, when this request is provided via the external repair test equipment according to the applicable standard set in Appendix 6 of this Chapter.

4.7.1.4 **Freeze Frame Information**

At least one "freeze frame" of information shall be stored at the time that either a potential DTC or a confirmed and active DTC is stored at the decision of the manufacturer. The manufacturer is allowed to update the freeze frame information whenever the pending DTC is detected again.

The freeze frame shall provide the operating conditions of the vehicle at the time of malfunction detection and the DTC associated with the stored data. The freeze frame shall include the information as shown in Table 1 in Appendix 5 of this Chapter. The freeze frame shall also include all of the information in Tables 2 and 3 of Appendix 5 of this Chapter that are used for monitoring or control purposes in the specific control unit that stored the DTC.

Storage of freeze frame information associated with a Class A malfunction shall take precedence over information associated with a Class B1 malfunction which shall take precedence over information associated with a Class B2 malfunction and likewise for information associated with a Class C malfunction. The first malfunction detected shall take precedence over the most recent malfunction unless the most recent malfunction is of a higher class.

In case a device is monitored by the OBD system and is not covered by Appendix 5 of this Chapter the freeze frame information shall include elements of information for the sensors and actuators of this device in a way similar to those described in Appendix 5 of this Chapter. This shall be submitted for approval by the Test Agency at the time of approval.

4.7.1.5 **Readiness**

With the exceptions specified in clauses 4.7.1.5.1., 4.7.1.5.2. and 4.7.1.5.3. of this Chapter, a readiness shall only be set to "complete" when a monitor or a group of monitors addressed by this status have run and concluded the presence (that means stored a confirmed and active DTC) or the absence of the failure relevant to that monitor since the last erasing by request of an external OBD scan-tool. Readiness shall be set to "not complete" by erasing the fault code memory (see clause 4.7.4. of this Chapter) by an external request or command (for example through an OBD scan-tool).

Normal engine shutdown shall not cause the readiness to change.

- 4.7.1.5.1 The manufacturer may request, subject to approval by the Test Agency that the ready status for a monitor be set to indicate "complete" without the monitor having run and concluded the presence or the absence of the failure relevant to that monitor.

Such a request only be approved if during a multiple number of operating sequences (minimum 9 operating sequences or 72 operation hours):

- (a) Monitoring is temporarily disabled according to clause 5.2 of this Chapter due to the continued presence of extreme operating conditions (e.g. cold ambient temperatures, high altitudes); or
- (b) The system that is monitored is not in operation and the DTC associated to that system does not have the confirmed and active or the previously active status at the time when the readiness status becomes incomplete during a repair.

Any such request must specify the conditions for monitoring system disablement and the number of operating sequences that would pass without monitor completion before ready status would be indicated as "complete".

The extreme ambient or altitude conditions considered in the manufacturer's request shall never be less severe than the conditions specified by this Chapter for temporary disablement of the OBD system.

4.7.1.5.2 **Monitors subject to readiness**

Readiness shall be supported for each of the monitors or groups of monitors that are identified in this Chapter and that are required when and by referring to this Chapter, with the exception of items 11 and 12 of Appendix 3 of this Chapter.

4.7.1.5.3 **Readiness for continuous monitors**

Readiness of each of the monitors or groups of monitors that are identified in items 1, 7 and 10 of Appendix 3 of this Chapter, required when and by referring to this Chapter, and that are considered by this Chapter as running continuously, shall always indicate "complete".

4.7.2 **Data Stream Information**

The OBD system shall make available to a scan tool in real time the information shown in Tables 1 to 4 in Appendix 5 of this Chapter, upon request (actual signal values should be used in favour of surrogate values).

For the purpose of the calculated load and torque parameters, the OBD system shall report the most accurate values that are calculated within the applicable electronic control unit (e.g. the engine control computer).

Table 1 in Appendix 5 of this Chapter gives the list of mandatory OBD information relating to the engine load and speed.

Table 3 in Appendix 5 of this Chapter shows the other OBD information which must be included if used by the emission or OBD system to enable or disable any OBD monitors.

Table 4 in Appendix 5 of this Chapter shows the information which is required to be included if the engine is so equipped, senses or calculates the information⁽¹⁾ At the decision of the manufacturer, other freeze frame or data stream information may be included.

In case a device is monitored by the OBD system and is not covered by Appendix 5 of this Chapter (e.g. SCR), the data-stream information shall include elements of information for the sensors and actuators of this device in a way similar to those described in Appendix 5 of this Chapter. This shall be submitted for approval to the Test Agency at the time of approval.

- (1) It is not required to equip the engine for the sole purpose of providing the information data mentioned in Tables 3 and 4 of Appendix 5 of this Chapter.

4.7.3. Access to OBD information

Access to OBD information shall be provided only in accordance with the standards mentioned in Appendix 6 of this Chapter and the following sub-clauses ⁽¹⁾.

Access to the OBD information shall not be dependent on any access code or other device or method obtainable only from the manufacturer or its suppliers. Interpretation of the OBD information shall not require any unique decoding information, unless that information is publicly available.

A single access method (e.g. a single access point/node) to OBD information shall be supported to retrieve all OBD information. This method shall permit access to the complete OBD information required by this Chapter. This method shall also permit access to specific smaller information packages as defined in this Chapter (e.g. road worthiness information packages in case of emission related OBD)

Access to OBD information shall be provided using, at least one of the following series of standards mentioned in Appendix 6 of this Chapter:

- (a) ISO 27145 with ISO 15765-4 (CAN-based)
- (b) ISO 27145 with ISO 13400 (TCP/IP-based)
- (c) SAE J1939-73

Manufacturers shall use appropriate ISO or SAE-defined fault codes (for example, P0xxx, P2xxx) whenever possible. If such identification is not possible, the manufacturer may use diagnostic trouble codes according to the relevant clauses in ISO 27145 or SAE J1939. The fault codes must be fully accessible by standardized diagnostic equipment complying with the provisions of this Chapter.

The manufacturer shall provide the ISO or SAE standardization body through the appropriate ISO or SAE process with emission-related diagnostic data not specified by ISO 27145 or SAE J1939 but related to this Chapter.

Access to OBD information shall be possible by the means of a wired connection.

OBD data shall be provided by the OBD system upon request using scan tool that complies with the requirements of the applicable standards mentioned in Appendix 6 of this Chapter (communication with external tester).

- (1) The manufacturer is allowed to use an additional on-board diagnostic display, such as a dashboard mounted video display device, for providing access to OBD information. Such an additional device is not subject to the requirements of this Chapter.

4.7.3.1. CAN based wired communication

The communication speed on the wired data link of the OBD system shall be either 250 kbps or 500 kbps.

It is the manufacturer's responsibility to select the baud-rate and to design the OBD system according to the requirements specified in the standards mentioned in Appendix 6 of this Chapter, and referred to in this Chapter. The OBD system shall be tolerant against the automatic detection between these two baud-rates exercised by the external test equipment.

The connection interface between the vehicle and the external diagnostic test equipment (e.g. scan-tool) shall be standardized and shall meet all of the requirements of ISO 15031-3 Type A (12 VDC power supply), Type B (24 VDC power supply) or SAE J1939-13 (12 or 24 VDC power supply).

4.7.3.2 (Reserved for TCP/IP (Ethernet) based wired communication.)

4.7.3.3 Connector Location

The connector shall be located in the driver's side foot-well region of the vehicle interior in the area bound by the driver's side of the vehicle and the driver's side edge of the Centre console (or the vehicle centre line if the vehicle does not have a centre console) and at a location no higher than the bottom of the steering wheel when in the lowest adjustable position. The connector may not be located on or in the centre console (i.e. neither on the horizontal faces near the floor-mounted gear selector, parking brake lever, or cup holders nor on the vertical faces near the stereo/radio, climate system, or navigation system controls). The location of the connector shall be capable of being easily identified and accessed (e.g. to connect an off-board tool). For vehicles equipped with a driver's side door, the connector shall be capable of being easily identified and accessed by someone standing (or "crouched") outside the driver's side of the vehicle with the driver's side door open.

The Test Agency may approve upon request of the manufacturer an alternative location provided the installation position shall be easily accessible and protected from accidental damage during normal conditions of use, e.g. the location as described in ISO 15031 series of standards.

If the connector is covered or located in a specific equipment box, the cover or the compartment door must be removable by hand without the

use of any tools and be clearly labelled "OBD" to identify the location of the connector.

The manufacturer may equip vehicles with additional diagnostic connectors and data-links for manufacturer-specific purposes other than the required OBD functions. If the additional connector conforms to one of the standard diagnostic connectors allowed in Appendix 6 of this Chapter, only the connector required by this Chapter shall be clearly labelled "OBD" to distinguish it from other similar connectors.

4.7.4 **Erasing / resetting OBD information by a scan-tool**

On request of the scan tool, the following data shall be erased or reset to the value specified in this Chapter from the computer memory.

OBD information data	Erasable	Resettable ⁽¹⁾
Malfunction indicator status		X
Readiness of the OBD system		X
Number of engine operating hours since the malfunction indicator has been activated (continuous MI counter)	X	
All DTCs	X	
The value of the B1 counter with the highest number of engine operating hours		X
The number of engine operating hours from the B1-counter(s)		X
The freeze frame data requested by this Chapter	X	

(1) To the value specified in the appropriate section of this Chapter

OBD information shall not be erased by disconnection of the vehicle's battery(s).

4.8 **Electronic Security**

Any vehicle with an emission control unit must include features to deter modification, except as authorized by the manufacturer. The manufacturer shall authorize modifications if these modifications are necessary for the diagnosis, servicing, inspection, retrofitting or repair of the vehicle.

Any reprogrammable computer codes or operating parameters shall be resistant to tampering and afford a level of protection at least as good as the provisions in ISO 15031-7 (SAE J2186) or J1939-73 provided that the security exchange is conducted using the protocols and diagnostic connector as prescribed in this Chapter. Any removable calibration memory chips shall be potted, encased in a sealed container or protected by electronic algorithms and shall not be changeable without the use of specialized tools and procedures.

Computer-coded engine operating parameters shall not be changeable without the use of specialized tools and procedures (e.g. soldered or potted computer components or sealed (or soldered) computer enclosures).

Manufacturers shall take adequate steps to protect the maximum fuel delivery setting from tampering while a vehicle is in-service.

Manufacturers may apply to the Test Agency for an exemption from one of these requirements for those vehicles that are unlikely to require protection. The criteria that the Test Agency will evaluate in considering an exemption will include, but are not limited to, the current availability of performance chips, the high-performance capability of the vehicle and the projected sales volume of the vehicle.

Manufacturers using programmable computer code systems (e.g. electrical erasable programmable read-only memory, EEPROM) shall deter unauthorized reprogramming. Manufacturers shall include enhanced tamper-protection strategies and write protect features requiring electronic access to an off-site computer maintained by the manufacturer. Alternative methods giving an equivalent level of tamper protection may be approved by the Test Agency.

4.9 **Durability of the OBD System**

The OBD system shall be designed and constructed so as to enable it to identify types of malfunctions over the complete life of the vehicle or engine system.

Any additional provisions addressing the durability of OBD systems are contained in this Chapter.

An OBD system shall not be programmed or otherwise designed to partially or totally deactivate based on age and/or mileage of the vehicle during the actual life of the vehicle, nor shall the system contain any algorithm or strategy designed to reduce the effectiveness of the OBD system over time.

5.0 PERFORMANCE REQUIREMENTS

5.1 Thresholds

The OTLs for the applicable monitoring criteria defined in Appendix 3 of this Chapter are defined in Chapter 1 of this Part.

5.2 Temporary disablement of the OBD system

Test Agencies may approve that an OBD system be temporarily disabled under the conditions specified in the following sub-clauses.

At the time of type-approval, the manufacturer shall provide the Test Agency with the detailed description of each of the OBD system's temporary disablement strategies and the data and/or engineering evaluation demonstrating that monitoring during the applicable conditions would be unreliable or impractical.

In all cases, monitoring shall resume once the conditions justifying temporary disablement are no longer present.

5.2.1 Engine vehicle operational safety

Manufacturers may request approval to disable the affected OBD monitoring systems when operational safety strategies are activated.

The OBD monitoring system is not required to evaluate components during malfunction if such evaluation would result in a risk to the safe use of the vehicle.

5.2.2 Ambient temperature and altitude conditions

Manufacturers may request approval to disable OBD system monitors:

- (a) at ambient engine start temperatures below 273 K (0 degrees Celsius) in the case where the coolant temperature has not reached a minimum temperature of at least 333 K (60 degrees Celsius), or
- (b) at ambient temperatures below 273K (0 degrees Celsius) in the case of frozen reagent,) or
- (c) at ambient temperatures above 315 K (42 degrees Celsius
- (d) at elevations above 2,500 meters above sea level.
- (e) Below 400 m under sea level; or
- (f) With the exception of electrical circuit failures, at ambient temperatures below 266K (-7°C).

A manufacturer may further request approval that an OBD system monitor be temporarily disabled at other ambient temperatures and altitude conditions upon determining that the manufacturer has demonstrated with data and/or an engineering evaluation that misdiagnosis would occur at the ambient temperatures because of its effect on the component itself (e.g. component freezing, effect on the compatibility with sensor tolerances).

Note: Ambient conditions may be estimated by indirect methods. For example, ambient temperature conditions may be determined based on intake air temperature.

5.2.3 Low Fuel Level

Manufacturers may request approval to disable monitoring systems that are affected by low fuel level / pressure or running out of fuel (e.g. diagnosis of a malfunction of the fuelling system or misfiring) as follows:

	DIESEL	GAS	
		CNG	LPG
The low fuel level considered for such a disablement shall not exceed 100 litres or 20 per cent of the nominal capacity of the fuel tank, whichever is lower.	X		X
The low fuel pressure in the tank considered for such a disablement shall not exceed 20 per cent of the usable range of fuel tank pressure.		X	

5.2.4 Vehicle battery or system voltage levels

Manufacturers may request approval to disable monitoring systems that can be affected by vehicle battery or system voltage levels.

5.2.4.1 Low Voltage

For monitoring systems affected by low vehicle battery or system voltages, manufacturers may request approval to disable monitoring systems when the battery or system voltage is below 90 per cent of the nominal voltage (or 11.0 Volts for a 12 Volt battery, 22.0 Volts for a 24 Volt battery). Manufacturers may request approval to utilize a voltage threshold higher than this value to disable system monitoring.

The manufacturer shall demonstrate that monitoring at the voltages would be unreliable and that either operation of a vehicle below the disablement criteria for extended periods of time is unlikely or the OBD system monitors the battery or system voltage and will detect a malfunction at the voltage used to disable other monitors.

5.2.4.2 High Voltage

For emission related monitoring systems affected by high vehicle battery or system voltages, manufacturers may request approval to disable monitoring systems when the battery or system voltage exceeds a manufacturer-defined voltage.

The manufacturer shall demonstrate that monitoring above the manufacturer-defined voltage would be unreliable and that either the electrical charging system/alternator warning light is illuminated (or voltage gauge is in the "red zone") or the OBD system monitors the battery or system voltage and will detect a malfunction at the voltage used to disable other monitors.

5.2.5 Active PTO (power take off units)

The manufacturer may request approval to temporarily disable affected monitoring systems in vehicles equipped with a PTO unit, under the condition where that PTO unit is temporarily active.

5.2.6 Forced Regeneration

The manufacturer may request approval to disable the affected OBD monitoring systems during the forced regeneration of an emission control system downstream of the engine (e.g. a particulate filter).

5.2.7 Auxillary Emissions Strategy (AES)

The manufacturer may request approval to disable OBD system monitors during the operation of an AES, including MECS, under conditions not already covered in clause 5.2 of this Chapter. If the monitoring capability of a monitor is affected by the operation of an AES.

5.2.8 Re-fueling

After a refuelling, the manufacturer of a gaseous-fuelled vehicle may temporarily disable the OBD system when the system has to adapt to the recognition by the ECU of a change in the fuel quality and composition.

The OBD system shall be re-enabled as soon as the new fuel is recognized and the engine parameters are readjusted. This disablement shall be limited to a maximum of 10 minutes.

6.0 DEMONSTRATION REQUIREMENTS

The basic elements for demonstrating the compliance of an OBD system with the requirements of this Chapter are as follows:

- (a) Procedure for selecting the OBD-parent engine system. The OBD-parent engine system is selected by the manufacturer in agreement with the Test Agency
- (b) Procedure for demonstrating the classification of a malfunction. The manufacturer submits to the Test Agency the classification of each malfunction for that OBD-parent engine system and the necessary supporting data in order to justify each classification.
- (c) Procedure for qualifying a deteriorated component. The manufacturer shall provide, on request of the Test Agency, deteriorated components for OBD testing purposes. These components are qualified on the basis of supporting data provided by the manufacturer.
- (d) Procedure for selecting the reference fuel in case of a gas engine.

6.1 **Emission-OBD family**

The manufacturer is responsible for determining the composition of an emission-OBD family. Grouping engine systems within an emission-OBD family shall be based on good engineering judgment and be subject to approval by the Test Agency. Engines that do not belong to the same engine family may still belong to the same emission-OBD family

6.1.1 **Parameters defining an emission-OBD family**

An emission-OBD family is characterized by basic design parameters that shall be common to engine systems within the family.

In order that engine systems are considered to belong to the same OBD-engine family, the following list of basic parameters shall be similar:

- (a) Emission control systems
- (b) Methods of OBD monitoring
- (c) Criteria for performance and component monitoring
- (d) Monitoring parameters (e.g. frequency)

These similarities shall be demonstrated by the manufacturer by means of relevant engineering demonstration or other appropriate procedures and subject to the approval of the Test Agency.

The manufacturer may request approval by the Test Agency of minor differences in the methods of monitoring/diagnosing the engine emission control system due to engine system configuration variation, when these methods are considered similar by the manufacturer and:

- (a) They differ only to match specificities of the considered components (e.g. size, exhaust flow, etc.); or
- (b) Their similarities are based on good engineering judgement.

6.1.2 **OBD-Parent Engine System**

Compliance of an emission-OBD family with the requirements of this Chapter is achieved by demonstrating the compliance of the OBD-parent engine system of this family.

The selection of the OBD-parent engine system is made by the manufacturer and subject to the approval of the Test Agency.

Prior to testing the Test Agency may decide to request the manufacturer to select an additional engine for demonstration.

The manufacturer may also propose to the Test Agency to test additional engines to cover the complete emission-OBD family.

6.2 Procedures for demonstrating the malfunction classification

The manufacturer shall provide the documentation justifying the proper classification of each malfunction to the Test Agency. This documentation shall include a failure analysis (for example elements of a "failure mode and effect analysis") and may also include:

- (a) Simulation results;
- (b) Test results;
- (c) Reference to previously approved classification.

In the following paragraphs the requirements for demonstrating the correct classification are listed, including requirements for testing. The minimum number of tests is four and the maximum number of tests is four times the number of engine families considered within the emission OBD family. The Test Agency may decide to curtail the test at any time before this maximum number of failure tests has been reached.

In specific cases where the classification testing is not possible (for example, if an MECS is activated and the engine cannot run the applicable test, etc.), the malfunction may be classified based on technical justification. This exception shall be documented by the manufacturer and is subject to the agreement of the Test Agency.

6.2.1 Demonstration of classification into Class A

The classification by the manufacturer of a malfunction into Class A shall not be subject to a demonstration test.

If the Test Agency disagrees with a manufacturer's classification of a malfunction as Class A, the Test Agency requires the classification of the malfunction into Class B1, B2 or C, as appropriate.

In that case the approval document shall record that the malfunction classification has been assigned according to the request of the Test Agency.

6.2.2 Demonstration of classification into Class B1 (distinguishing between A and B1)

In order to justify the classification of a malfunction into Class B1 the documentation shall clearly demonstrate that, in some circumstances⁽¹⁾, the malfunction results in emissions that are lower than the OTLs.

In the case that the Test Agency requires an emission test for demonstrating the classification of a malfunction into Class B1 the manufacturer shall demonstrate that the emissions due to that particular malfunction are, in selected circumstances, below the OTLs:

- (a) The manufacturer selects the circumstances of the test in agreement with the Test Agency;

- (b) The manufacturer shall not be required to demonstrate that in other circumstances the emissions due to the malfunction are actually above the OTLs.

If the manufacturer fails to demonstrate the classification as Class B1, the malfunction is classified as Class A.

- ⁽¹⁾ Examples of circumstances that may influence if and when OTL are exceeded are the of the engine system or whether the test is conducted with a new or aged component.

6.2.3 **Demonstration of classification into Class B1 (distinguishing between B₂ and B1)**

If the Test Agency disagrees with a manufacturer's classification of a malfunction as Class B1 because it considers that the OTLs are not exceeded, the Test Agency requires the reclassification of that malfunction into Class B2 or C. In that case the approval documents shall record that the malfunction classification has been assigned according to the request of the Test Agency.

6.2.4 **Demonstration of classification into Class B2 (distinguishing between B2 and B1)**

In order to justify the classification of a malfunction into Class B2 the manufacturer shall demonstrate that emissions are lower than the OTLs.

In case the Test Agency disagrees with the classification of a malfunction as Class B2 because it considers that the OTLs are exceeded, the manufacturer may be required to demonstrate by testing that the emissions due to the malfunction are below the OTLs. If the test fails, then the Test Agency shall require the reclassification of that malfunction into A or B1 and the manufacturer shall subsequently demonstrate the appropriate classification and the documentation shall be updated.

6.2.5 **Demonstration of classification into Class B2 (distinguishing between B2 and C)**

If the Test Agency disagrees with a manufacturer's classification of a malfunction as Class B2 because it considers the regulated emission limits are not exceeded, the Test Agency requires the reclassification of that malfunction into Class C. In that case the approval documents shall record that the malfunction classification has been assigned according to the request of the Test Agency.

6.2.6 **Demonstration of classification into Class C**

In order to justify the classification of a malfunction into Class C the manufacturer shall demonstrate that emissions are lower than the regulated emission limits.

In case the Test Agency disagrees with the classification of a malfunction as Class C the manufacturer may be required to

demonstrate by testing that the emissions due to the malfunction are below the regulated emission limits.

If the test fails, then the Test Agency shall request the reclassification of that malfunction and the manufacturer shall subsequently demonstrate the appropriate reclassification and the documentation shall be updated.

6.3 Procedures for demonstrating the OBD performance

The manufacturer shall submit to the Test Agency a complete documentation package justifying the compliance of the OBD system as regards its monitoring capability, which may include:

- (a) Algorithms and decision charts
- (b) Tests and/or simulation results
- (c) Reference to previously approved monitoring systems, etc.

In the following paragraphs the requirements for demonstrating the OBD performance are listed, including requirements for testing. The number of tests shall be four times the number of engine families considered within the emission OBD family, but shall not be less than 8.

The monitors selected shall reflect the different types of monitors mentioned in clause 4.2. of this Chapter (i.e. emission threshold monitoring, performance monitoring, total functional failure monitoring, or component monitoring) in a well-balanced manner. The monitors selected shall also reflect the different items listed in Appendix 3 of this Chapter in a well-balanced manner.

6.3.1 Procedures for demonstrating the OBD performance by Testing

In addition to the supporting data referred to in clause 6.3. of this Chapter, the manufacturer shall demonstrate the proper monitoring of specific emission control systems or components by testing them on an engine test-bed according to the test procedures specified in clause 7.2. of this Chapter.

In that case, the manufacturer shall make available the qualified deteriorated components or the electrical device which would be used to simulate a malfunction.

The proper detection of the malfunction by the OBD system and its proper response to that detection (cf. MI indication, DTC storage, etc.) shall be demonstrated according to clause 7.2. of this Chapter.

6.3.2 Procedures for qualifying a deteriorated component (or system)

This clause applies to the cases where the malfunction selected for an OBD demonstration test is monitored against tailpipe emissions⁽¹⁾ (emission threshold monitoring - see clause 4.2. of this Chapter) and it is required that the manufacturer demonstrates, by an emission test, the qualification of that deteriorated component.

In very specific cases the qualification of deteriorated components or systems by testing may not be possible (for example, if an MECS is activated and the engine cannot run the applicable test, etc.). In such cases, the deteriorated component shall be qualified without testing. This exception shall be documented by the manufacturer and is subject to the agreement of the Test Agency.

(1) This clause will be extended to other monitors than emission threshold monitors at a later stage.

6.3.2.1 Procedure for qualifying a deteriorated component used to demonstrate the detection of classes A and B1 malfunctions.

6.3.2.1.1 Emission Threshold Monitoring

In the case the malfunction selected by the Test Agency results in tailpipe emissions that may exceed an OBD threshold limit, the manufacturer shall demonstrate by an emission test according to clause 7. of this Chapter that the deteriorated component or device does not result in the relevant emission exceeding its OTL by more than 20 per cent.

6.3.2.1.2 Performance Monitoring

At the request of the manufacturer and with the agreement of the Test Agency, in the case of performance monitoring, the OTL may be exceeded by more than 20 per cent. Such request shall be justified on a case by case basis.

In the case when the performance monitoring of an abnormality of the gaseous fuel consumption of a dual fuel engine or vehicle is required by Chapter 14 of this Part a deteriorated component is qualified without reference to the OTL.

6.3.2.1.3 Component Monitoring

In the case of component monitoring, a deteriorated component is qualified without reference to the OTL.

6.3.2.2 Qualification of deteriorated components used to demonstrate the detection of Class B2 malfunctions

In the case of Class B2 malfunctions, and upon request of the Test Agency, the manufacturer shall demonstrate by an emission test according to clause 7. of this Chapter that the deteriorated component or device does not lead the relevant emission to exceed its applicable OTL.

6.3.2.3 Qualification of deteriorated components used to demonstrate the detection of class C malfunctions.

In the case of Class C malfunctions, and upon request of the Test Agency, the manufacturer shall demonstrate by an emission test according to clause 7. of this Chapter that the deteriorated component or device does not lead the relevant emission to exceed its applicable regulated emission limit.

6.3.3 **Test Report**

The test report shall contain, at a minimum, the information set out in Appendix 4 of this Chapter.

6.4 **Approval of an OBD system containing deficiencies**

6.4.1 Test Agencies may approve upon request of a manufacturer an OBD system even though the system contains one or more deficiencies.

In considering the request, the Test Agency shall determine whether compliance with the requirements of this Chapter is feasible or unreasonable.

The Test Agency shall take into consideration data from the manufacturer that details such factors as, but not limited to, technical feasibility, lead time and production cycles including phase-in or phase-out of engines designs and programmed upgrades of computers, the extent to which the resultant OBD system will be effective in complying with the requirements of this Chapter and that the manufacturer has demonstrated an acceptable level of effort toward meeting the requirements of the Chapter.

The Test Agency will not accept any deficiency request that includes the complete lack of a required diagnostic monitor (i.e. a complete lack of the monitors required in Appendix 3 of this Chapter).

6.4.2 **Deficiency Period**

A deficiency is granted for a period of one year after the date of approval of the engine system.

If the manufacturer can adequately demonstrate to the Test Agency that substantial engine modifications and additional lead time would be necessary to correct the deficiency, then this deficiency can be granted again for an additional one year, provided that the total deficiency period does not exceed 3 years (i.e. 3 times one-year deficiency allowance is permitted).

The manufacturer cannot apply for a renewal of the deficiency period.

6.5 **Procedure for selecting the reference fuel in case of a gas engine**

Demonstration of the OBD performance and malfunction classification shall be performed by using one of the reference fuels mentioned in Chapter 4 of this Part on which the engine is designed to operate.

The selection of this reference fuel is done by the Test Agency, who shall provide sufficient time for the test laboratory to supply the selected reference fuel.

7.0 TEST PROCEDURES

7.1 Testing process

The demonstration by testing of the proper malfunction classification and the demonstration by testing of the proper monitoring performance of an OBD system are issues that shall be considered separately during the testing process. For example, a Class A malfunction will not require a classification test while it may be subject to an OBD performance test.

Where appropriate, the same test may be used to demonstrate the correct classification of a malfunction, the qualification of a deteriorated component provided by the manufacturer and the correct monitoring by the OBD system.

The engine system on which the OBD system is tested shall comply with the emission requirements of this Part.

7.1.1 Testing process for demonstrating the malfunction classification

When, according to clause 6.2. of this Chapter, the Test Agency requests the manufacturer to justify by testing the classification of a specific malfunction, the compliance demonstration will consist of a series of emission tests.

According to clause 6.2.2. of this Chapter, when testing is required by the Test Agency to justify the classification of a malfunction into Class B1 rather than in Class A, the manufacturer shall demonstrate that the emissions due to that particular malfunction are, in selected circumstances, below the OTLs:

- (a) The manufacturer selects these circumstances of test in agreement with the Test Agency
- (b) The manufacturer shall not be required to demonstrate that in other circumstances the emissions due to the malfunction are actually above the OTLs.

The emission test may be repeated upon request of the manufacturer up to three times.

If any of these tests leads to emissions below the considered OTL, then the malfunction classification into Class B1 shall be approved.

When testing is required by the Test Agency to justify the classification of a malfunction into Class B2 rather than in Class B1 or into Class C rather than in Class B2, the emission test shall not be repeated. If the emissions measured in the test are above the OTL or the emission limit, respectively, then the malfunction shall require a reclassification.

Note: According to clause 6.2.1. of this Chapter, this clause does not apply to malfunctions classified into Class A.

7.1.2 **Testing process for demonstrating the OBD performance**

When the Test Agency requests to test the OBD system performance according to clause 6.3. of this Chapter, the compliance demonstration shall consist of the following phases:

- (a) A malfunction is selected by the Test Agency and a corresponding deteriorated component or system shall be made available by the manufacturer;
- (b) When appropriate and if requested, the manufacturer shall demonstrate by an emission test that the deteriorated component is qualified for a monitoring demonstration;
- (c) The manufacturer shall demonstrate that the OBD system responds in a manner that complies with the provisions of this Chapter (i.e. MI indication, DTC storage, etc.) At the latest by the end of a series of OBD test-cycles.

7.1.2.1 **Qualification of the Deteriorated Component**

When the Test Agency requests the manufacturer to qualify a deteriorated component by testing according to clause 6.3.2. of this Chapter, this demonstration shall be made by performing an emissions test.

If it is determined that the installation of a deteriorated component or device on an engine system means that a comparison with the OBD threshold limits is not possible (e.g. because the statistical conditions for validating the applicable emission test cycle are not met), the malfunction of that component or device may be considered as qualified upon the agreement of the Test Agency based on technical rationale provided by the manufacturer.

In the case that the installation of a deteriorated component or device on an engine means that the full load curve (as determined with a correctly operating engine) cannot be attained during the test, the deteriorated component or device may be considered as qualified upon the agreement of the Test Agency based on technical rationale provided by the manufacturer.

7.1.2.2 **Malfunction Detection**

Each monitor selected by the Test Agency to be tested on an engine test-bed, shall respond to the introduction of a qualified deteriorated component in a manner that meets the requirements of this Chapter within two consecutive OBD test-cycles according to clause 7.2.2. of this Chapter.

When it has been specified in the monitoring description and agreed by the Test Agency that a specific monitor needs more than two operating sequences to complete its monitoring, the number of OBD test-cycles may be increased according to the manufacturer's request.

Each individual OBD test-cycle in the demonstration test shall be separated by an engine shut-off. The time until the next start-up shall take into consideration any monitoring that may occur after engine shut-off and any necessary condition that must exist for monitoring to occur at the next start up.

The test is considered complete as soon as the OBD system has responded in a manner that meets the requirements of this Chapter.

7.2 **Applicable Tests**

In the context of this Chapter:

- (a) The emission test-cycle is the test-cycle used for the measurement of the regulated emissions when qualifying a deteriorated component or system,
- (b) The OBD test-cycle is the test-cycle used to demonstrate the capacity of the OBD monitors to detect malfunctions.

7.2.1 **Emission Test Cycle**

The test-cycle considered in this Chapter for measuring emissions is the WHTC test-cycle as described in Chapter 3 of this Part.

7.2.2 **OBD Test Cycle**

The OBD test-cycle considered in this Chapter is the hot part of the WHTC cycle as described in Chapter 3 of this Part.

On request of the manufacturer and after approval of the Test Agency, an alternative OBD test-cycle can be used (e.g. the cold part of the WHTC cycle) for a specific monitor. The request shall contain documentation (technical considerations, simulation, test results, etc.) showing that:

- (a) The requested test-cycle appropriate to demonstrate monitoring occurs under real world driving conditions, and,
- (b) The hot part of the WHTC cycle appears as less appropriate for the considered monitoring (e.g. fluid consumption monitoring).

7.2.3 **Test Operating Conditions**

The conditions (i.e. temperature, altitude, fuel quality etc.) for conducting the tests referred to in clauses 7.2.1. and 7.2.2. of this Chapter shall be those required for operating the WHTC test cycle as described in Chapter 3 of this Part.

In the case of an emission test aimed at justifying the classification of a specific malfunction into Class B1, the test operating conditions may, per decision of the manufacturer, deviate from the ones in the clauses above according to clause 6.2.2 of this Chapter.

7.3 Demonstration Process for Performance Monitoring

The manufacturer may use the demonstration requirements as set out in Appendix 7 of this Chapter in case of performance monitoring.

Test Agencies may approve a manufacturer's use of a type of performance monitoring technique other than the one referred to in Appendix 7 of this Chapter. The chosen type of monitoring shall be demonstrated by the manufacturer by a robust technical case based upon the design characteristics, or by presentation of test results, or by reference to previous approvals, or by some other acceptable method, to be at least as robust, timely and efficient as the ones mentioned in Appendix 7 of this Chapter.

7.4 Test Reports

The test report shall contain, at a minimum, the information set out in Appendix 4 of this Chapter.

8.0 DOCUMENTATION REQUIREMENTS

8.1 Documentation for purpose of approval

The manufacturer shall provide a documentation package that includes a full description of the OBD system. The documentation package shall be made available in two parts:

- (a) A first part, which may be brief, provided that it exhibits evidence concerning the relationships between monitors, sensors/actuators, and operating conditions (i.e. describes all enable conditions for monitors to run and disable conditions that cause monitors not to run). The documentation shall describe the functional operation of the OBD, including the malfunction ranking within the hierarchical classification. This material shall be retained by the Test Agency. This information may be made available to interested parties upon request.
- (b) A second part containing any data, including details of qualified deteriorated components or systems and associated test results, which are used as evidence to support the decision process referred to above, and a listing of all input and output signals that are available to the engine system and monitored by the OBD system. This second part shall also outline each monitoring strategy and the decision process.

This second part shall remain strictly confidential. It may be kept by the Test Agency, or, at the discretion of the Test Agency, may be retained by the manufacturer but shall be made open for inspection by the Test Agency at the time of approval or at any time during the validity of the approval.

8.1.1 Documentation associated with each monitored component or system

The documentation package included in the second part shall contain but shall not be limited to the following information for each monitored component or system:

- (a) The malfunctions and associated DTC(s);
- (b) The monitoring method used for malfunction detection;
- (c) The parameters used and the conditions necessary for malfunction detection and when applicable the fault criteria limit (performance and component monitoring);
- (d) The criteria for storing a DTC;
- (e) The monitoring "time length" (i.e. the operation time/procedure necessary to complete the monitoring) and the monitoring "frequency" (e.g. continuous, once per trip, etc.).

8.1.2 Documentation associated with the malfunction classification

The documentation package included in the second part shall contain but shall not be limited to the following information for malfunction classification.

The malfunction classification of each DTC shall be documented. This classification may be different for different engine types (e.g. different engine ratings) within the same emission-OBD family.

This information shall include the technical justification required in clause 4.2. of this Chapter for classification into Class A, Class B1 or Class B2.

8.1.3 Documentation associated with the emission-OBD family

The documentation package included in the second part shall contain but shall not be limited to the following information for emission OBD-family:

A description of the emission-OBD family shall be provided. This description shall include a list and a description of the engine types within the family, the description of the OBD-parent engine system, and all elements that characterize the family according to clause 6.1.1. of this Chapter.

In the case where the emission-OBD family includes engines belonging to different engine families, a summary description of these engine families shall be provided.

In addition, the manufacturer shall provide a list of all electronic input, output and identification of the communication protocol utilized by each emission-OBD family.

8.2 **Documentation for installing in a vehicle an OBD equipped engine system**

The engine manufacturer shall include in the installation documents of its engine system the appropriate requirements that will ensure the vehicle, when used on the road or elsewhere as appropriate, will comply with the requirements of this Chapter. This documentation shall include but is not limited to:

- (a) The detailed technical requirements, including the provisions ensuring the compatibility with the OBD system of the engine system;
- (b) The verification procedure to be completed.

The existence and the adequacy of such installation requirements may be checked during the approval process of the engine system.

Note: In the case a vehicle manufacturer applies for a direct approval of the installation of the OBD system on the vehicle, this documentation is not required.

CHAPTER 8B - APPENDIX 1

APPROVAL OF INSTALLATION OF OBD SYSTEMS

This Appendix considers the case where the vehicle manufacturer requests approval of the installation on a vehicle of (an) OBD system(s) within an emission OBD family, that is (are) certified to the requirements of this Chapter.

In this case, and in addition to the general requirements of this Chapter, a demonstration of the correct installation is required. This demonstration shall be done on the basis of the appropriate element of design, results of verification tests, etc. and address the conformity of the following elements to the requirements of this Chapter:

- (a) The installation on-board the vehicle as regards its compatibility with the OBD system of the engine-system
- (b) The MI (pictogram, activation schemes, etc.);
- (c) The wired communication interface.

Correct MI illumination, information storage and on-board off-board OBD communication will be checked. But any check shall not force dismounting the engine system (e.g. an electric disconnection may be selected).

CHAPTER 8B - APPENDIX 2

MALFUNCTIONS ILLUSTRATION OF THE DTC STATUS - ILLUSTRATION OF THE MI AND COUNTERS ACTIVATION SCHEMES

This Appendix aims at illustrating the requirements set in clauses 4.3. and 4.6.5. of this Chapter.

It contains the following figures:

Figure 1: DTC status in case of a class B1 malfunction

Figure 2: DTC status in case of 2 consecutive different class B1 malfunction

Figure 3: DTC status in case of re-occurrence of a class B1 malfunction

Figure 4A: Class A malfunction -activation of the MI and MI counters

Figure 4B: Illustration of the continuous MI deactivation principle

Figure 5: Class B1 malfunction - activation of the B1 counter in 5 use cases.

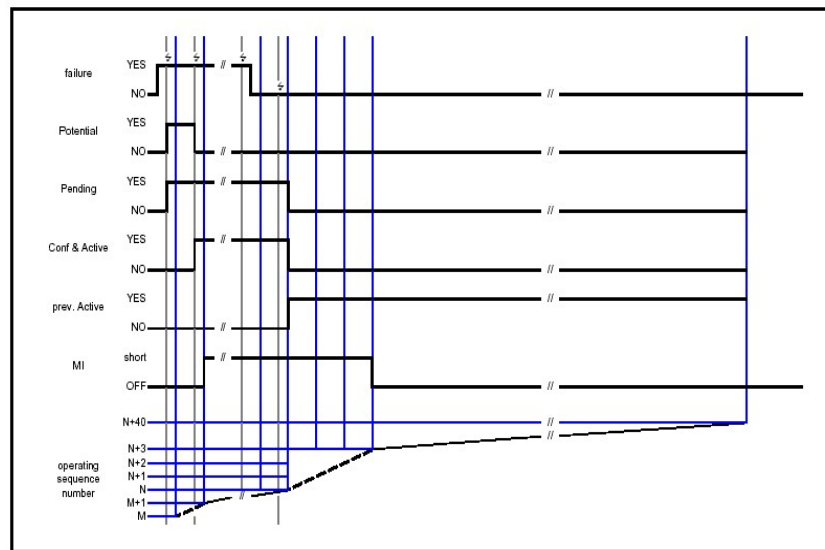


Figure 1
DTC Status in case of a Class B1 Malfunction

Notes:

⚡ Means the point a monitoring of the concerned malfunction occurs

N, M The Chapter requires the identification of "key" operating sequences during which some events occurs, and the counting of the subsequent operating sequences. For the purpose of illustrating this requirement, the "key" operating sequences have been given the values N and M.

e.g. M means the first operating sequence following the detection of a potential malfunction, and N means the operating sequence during which the MI is switched OFF.

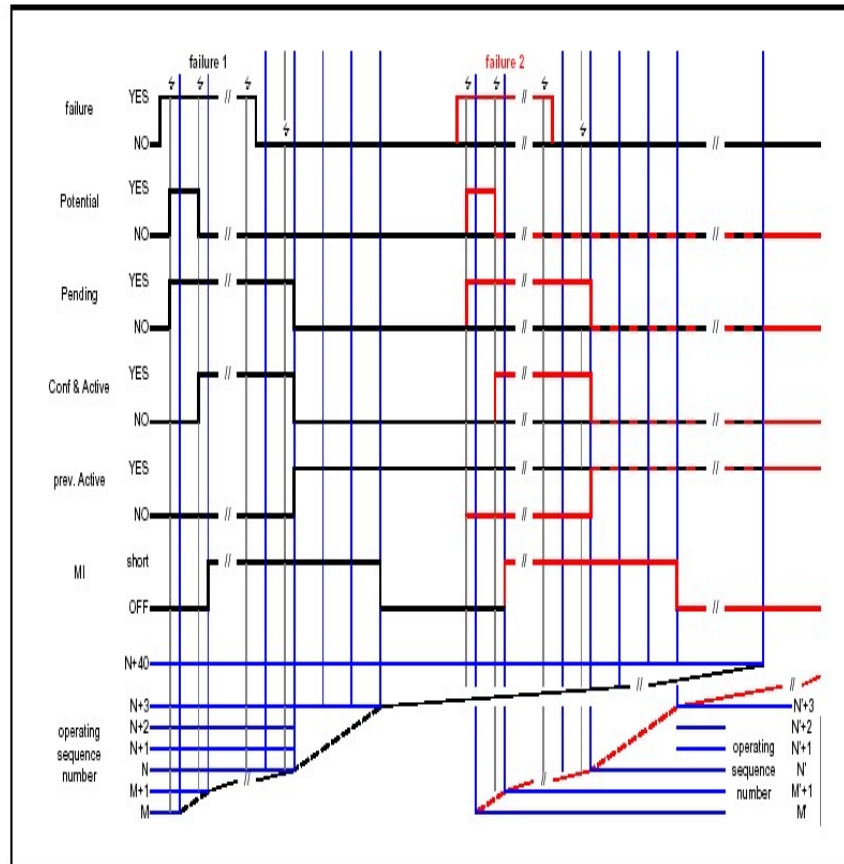


Figure 2
DTC Status in Case of
2 Consecutive Different Class B1 Malfunctions

Notes:

⚡ Means the point a monitoring of the concerned malfunction occurs

N, M,

N', M' The Chapter requires the identification of "key" operating sequences during which some events occurs, and the counting of the subsequent operating sequences. For the purpose of illustrating this requirement, the "key" operating sequences have been given the values N and M for the first malfunction, respectively N' and M' for the second one.

e.g. M means the first operating sequence following the detection of a potential malfunction, and N means the operating sequence during which the MI is switched OFF.

N + 40 the fortieth operating sequence after the first extinction of the MI or 200 engine operating hours, whichever the earliest.

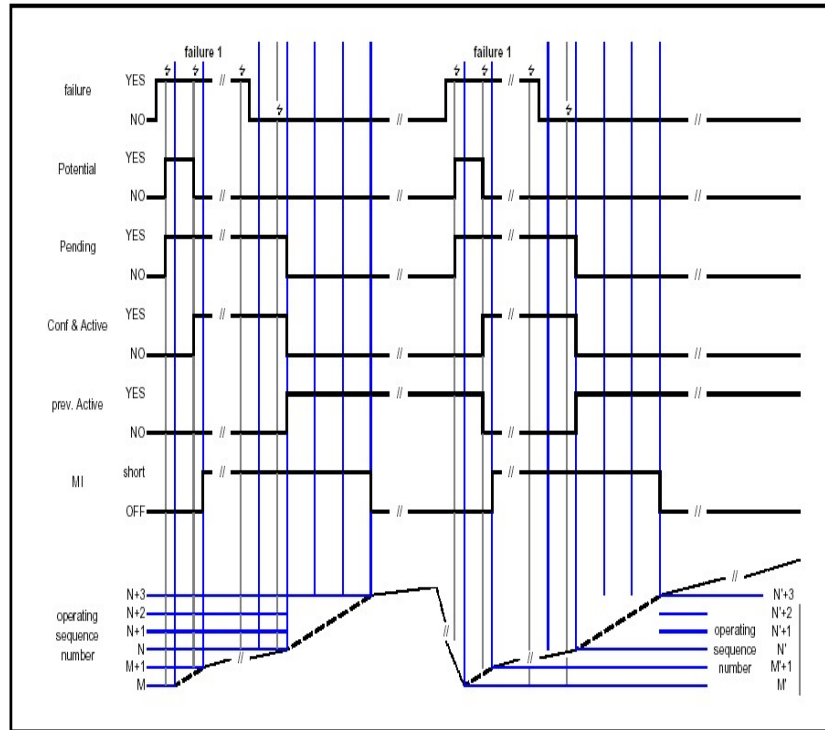


Figure 3
DTC Status in case of
the Re-Occurrence of a Class B1 Malfunction

Notes:

⚡ means the point a monitoring of the concerned malfunction occurs

N, M,

N', M' The Chapter requires the identification of "key" operating sequences during which some events occurs, and the counting of the subsequent operating sequences. For the purpose of illustrating this requirement, the "key" operating sequences have been given the values N and M for the first occurrence of a malfunction, respectively N' and M' for the second one.

e.g. M means the first operating sequence following the detection of a potential malfunction, and N means the operating sequence during which the MI is switched OFF.

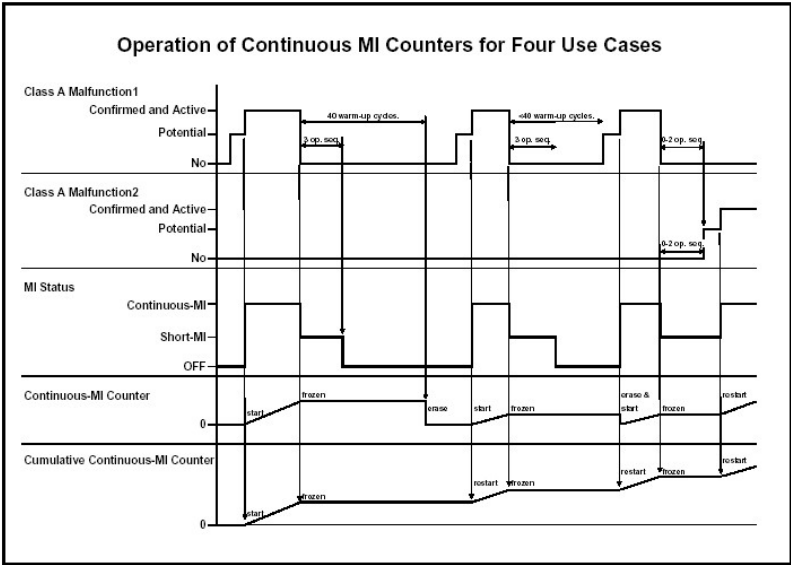


Figure 4A
Class A Malfunction - Activation of the MI and MI Counters

Note: Details related to the deactivation of the continuous MI are illustrated in Figure 4B below in the specific case where a potential state is present.

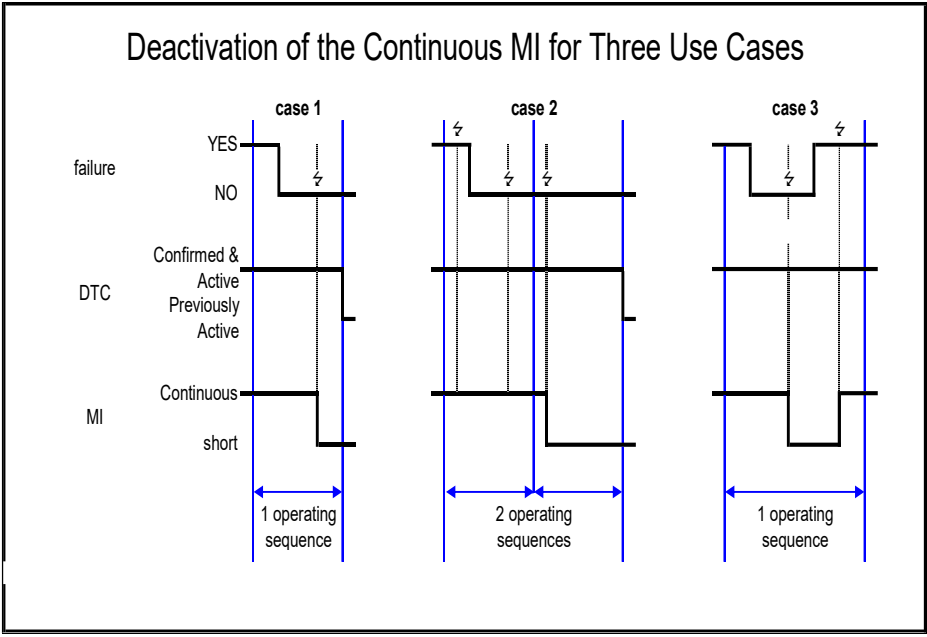


Figure 4B
Illustration of the Continuous MI Deactivation Principle

Notes:

⚡ means the point where monitoring of the concerned malfunction occurs.

M means the operating sequence when the monitor concludes for the first time that a confirmed and active failure is no longer present.

case 1 means the case where the monitor does not conclude the presence of failure during the operating sequence M.

case 2 means the case where the monitor has previously concluded, during the operating sequence M, the presence of the malfunction.

case 3 means the case where the monitor concludes during the operating sequence M the presence of the malfunction after having first concluded to its absence.

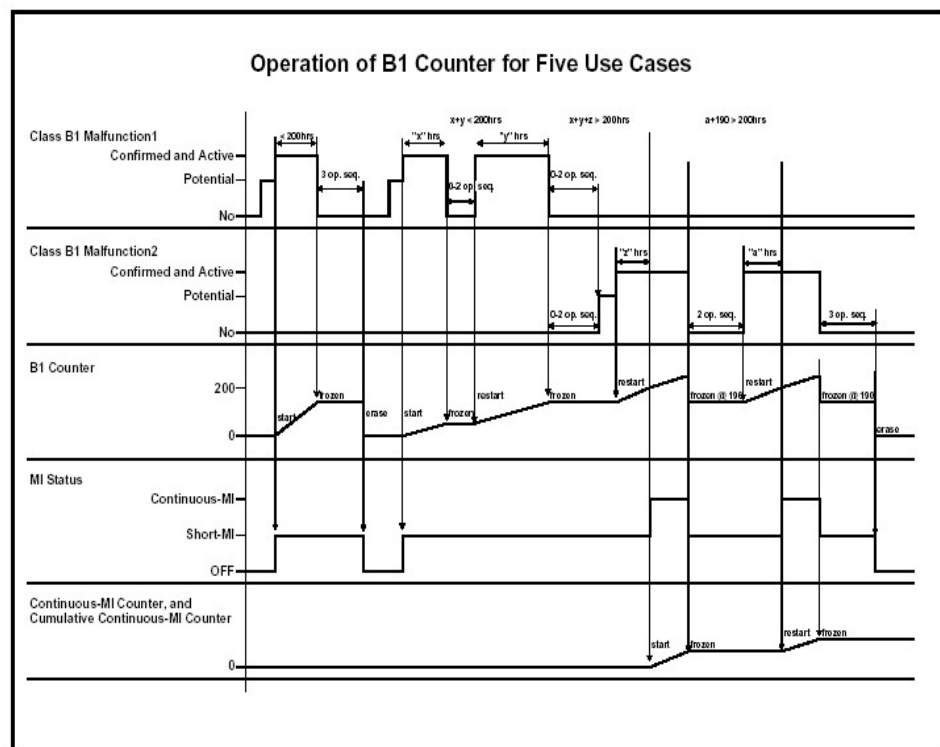


Figure 5
Class B1 Malfunction - Activation of the B1 Counter in 5 Use Cases

Note: In this example it is assumed that there is a single B1 counter

CHAPTER 8B - APPENDIX 3

MONITORING REQUIRMENTS

The items of this Appendix list the systems or components required to be monitored by the OBD system, according to clause 4.2 of this Chapter. Unless specified otherwise, the requirements apply to all engine types..

Appendix 3 - Item 1

Electric / Electronic Components Monitoring

Electric/electronic components used to control or monitor the emission control systems described in this appendix shall be subject to Component Monitoring according to the provisions of clause 4.2. of this Chapter. This includes, but is not limited to, pressure sensors, temperature sensors, exhaust gas sensors and oxygen sensors when present, knock sensors, in-exhaust fuel or reagent injector(s), in-exhaust burners or heating elements, glow plugs, intake air heaters.

Wherever a feedback control loop exists, the OBD system shall monitor the system's ability to maintain feedback control as designed (possible errors are for example. not entering feedback control within a manufacturer specified time interval, system fails to maintain feedback control, feedback control has used up all the adjustment capability allowed by the manufacturer and the system cannot achieve the target) - component monitoring.

In particular, in the case where the control of reagent injection is performed by means of a closed loop system, the monitoring requirements set out in this item shall apply, but the failures detected shall not be classified as Class C failures.

Note: These provisions apply to all electric-electronic components, even if they belong to any of the monitors described in the other items of this Appendix.

Appendix 3 - Item 2

DPF system

The OBD system shall monitor the following elements of the DPF system on engines so-equipped for proper operation:

- (a) DPF substrate: the presence of the DPF substrate - total functional failure monitoring
- (b) DPF performance: clogging of the DPF - total functional failure
- (c1) DPF filtering performance: the filtering and continuous regeneration process of the DPF. This requirement would apply to PM emissions only - emission threshold monitoring.

Note:

- (c1) is applicable to OBD stage II and c2 is applicable to OBD stage I
- (c2) DPF performance: filtering and regeneration processes (e.g. particulate accumulation during the filtering process and particulate removal during a forced regeneration process) - performance monitoring according to Appendix 8 of this Chapter.

The periodic regeneration shall be monitored against the ability of the device to perform as designed (for example to perform regeneration within a manufacturer-specified time interval, to perform regeneration upon demand, etc.). This will constitute one element of the component monitoring associated with the device.

Appendix 3 - Item 3

Selective catalytic reduction (SCR) monitoring

For the purpose of this Item, SCR means selective catalytic reduction or other lean NO_x catalyst device. The OBD system shall monitor the following elements of the SCR system on engines so-equipped for proper operation:

- (a) Active/intrusive reagent injection system: the system's ability to regulate reagent delivery properly, whether delivered via an in-exhaust injection or an in-cylinder injection - performance monitoring.
- (b) Active/intrusive reagent: the on-board availability of the reagent, the proper consumption of the reagent if a reagent other than fuel is used (e.g. urea) - performance monitoring.
- (c) Active/intrusive reagent: to the extent feasible the quality of the reagent if a reagent other than fuel is used (e.g. urea) - performance monitoring.
- (d) SCR catalyst conversion efficiency: the catalyst's SCR ability to convert NO_x emission threshold monitoring.

Appendix 3 - Item 4

Lean-NO_x trap /LNT, or NO_x adsorber)

The OBD system shall monitor the following elements of the LNT system on engines so-equipped for proper operation:

- (a) LNT capability: the LNT system's ability to adsorb/store and convert NO_x - performance monitoring.
- (b) LNT active/intrusive reagent injection system: the system's ability to regulate reagent delivery properly, whether delivered via an in-exhaust injection or an in-cylinder injection - performance monitoring.

Appendix 3 - Item 5**Oxidation catalysts (incl. diesel oxidation catalyst – DOC) monitoring**

This item applies to oxidation catalysts that are separate from other after treatment systems. Those that are included in the canning of an after treatment system are covered within the appropriate item of this Appendix.

The OBD system shall monitor the following elements of the oxidation catalysts on engines so-equipped for proper operation:

- (a) HC conversion efficiency: the oxidation catalysts ability to convert HC upstream of other after treatment devices - total functional failure monitoring.
- (b) HC conversion efficiency: the oxidation catalysts ability to convert HC downstream of other after treatment devices - total functional failure monitoring.

Appendix 3 - Item 6**Exhaust gas recirculation (EGR) system monitoring**

The OBD system shall monitor the following elements of the EGR system on engines so-equipped for proper operation:

	Diesel	Gas
(a1) EGR low/high flow: the EGR system's ability to maintain the commanded EGR flow rate, detecting both "flow rate too low" and "flow rate too high" conditions – emission threshold monitoring.	X	
(a2) EGR low/high flow: the EGR system's ability to maintain the commanded EGR flow rate, detecting both "flow rate too low" and "flow rate too high" conditions - performance monitoring.		X
(a3) EGR low flow: the EGR system's ability to maintain the commanded EGR flow rate, detecting "flow rate too low" conditions – total functional failure or performance monitoring as specified in this item.	X	X

(b) Slow response of the EGR actuator: the EGR system's ability to achieve the commanded flow rate within a manufacturer specified time interval following the command - performance monitoring.	X	X
(c1) EGR cooler under cooling performance: the EGR cooler system's ability to achieve the manufacturer's specified cooling performance - performance monitoring.	X	X
(c2) EGR cooler under cooling performance: the EGR cooler system's ability to achieve the manufacturer's specified cooling performance - total functional failure monitoring as specified in this item.	X	X

(a3) EGR low flow (total functional failure or performance monitoring)

In the case where the emissions would not exceed the OBD threshold limits even upon total failure of the EGR system's ability to maintain the commanded EGR flow rate (for example, because of the correct functioning of an SCR system downstream of the engine), then:

1. Where the control of the EGR flow rate is performed by means of a closed-loop system, the OBD system shall detect a malfunction when the EGR system cannot increase the EGR flow to achieve the demanded flow rate.

Such a malfunction shall not be classified as a class C failure.

2. Where the control of the EGR flow rate is performed by means of an open-loop system, the OBD system shall detect a malfunction when the system has no detectable amount of EGR flow when EGR flow is expected.

Such a malfunction shall not be classified as a class C failure.

(c2) EGR cooler under cooling performance (total functional failure monitoring)

In the case where total failure of the EGR cooler system's ability to achieve the manufacturer's specified cooling performance would not result in the monitoring system detecting a failure (because the resulting increase in emissions would not reach the OBD threshold limit for any pollutant), the OBD system shall detect a malfunction when the system has no detectable amount of EGR cooling.

Such a malfunction shall not be classified as a class C failure.

Appendix 3 - Item 7

Fuel System monitoring

The OBD system shall monitor the following elements of the fuel system on engines so-equipped for proper operation:

	DIESEL	GAS
(a) Fuel system pressure control: fuel system ability to achieve the commanded fuel pressure in closed loop control - performance monitoring.	X	
(b) Fuel system pressure control: fuel system ability to achieve the commanded fuel pressure in closed loop control in the case where the system is so constructed that the pressure can be controlled independently of other parameters - performance monitoring.	X	
(c) Fuel injection timing: fuel system ability to achieve the commanded fuel timing for at least one of the injection events when the engine is equipped with the appropriate sensors - performance monitoring.	X	
(d) Fuel injection quantity: fuel system ability to achieve the commanded fuel quantity by detecting errors from desired fuel quantity in at least one of the injection events when the engine is equipped with the appropriate sensors (e.g. pre-main or post-injection) – emission threshold monitoring	X	
(e) Fuel injection system: ability to maintain the desired air-fuel ratio (incl. but not limited to self-adaptation features) – performance monitoring.		X

Appendix 3 - Item 8**Air Handling and Turbocharger/Boost Pressure Control System**

The OBD system shall monitor the following elements of the Air Handling and Turbocharger/Boost Pressure Control System on engines so-equipped for proper operation.

	DIESEL	GAS
(a1) Turbo under/over boost: turbo boost system's ability to maintain the commanded boost pressure, detecting both "boost pressure too low" and "boost pressure too high" conditions – emission threshold monitoring.	X	
(a2) Turbo under/over boost: turbo boost system's ability to maintain the commanded boost pressure, detecting both "boost pressure too low" and "boost pressure too high" conditions – performance monitoring		X
(a3) Turbo under boost: turbo boost system's ability to maintain the commanded boost pressure, detecting "boost pressure too low" conditions – total functional failure or performance monitoring as specified in this item.	X	X
(b) Variable Geometry Turbo (VGT) slow response: VGT system's ability to achieve the commanded geometry within a manufacturer specified time-performance monitoring.	X	X
(c) Charge air cooling: Charge air cooling system efficiency - total functional failure.	X	X

(a3) Turbo under boost (total functional failure monitoring)

- 1 In the case where the emissions would not exceed the OBD threshold limits even upon total failure of the boost system's ability to maintain the demanded boost pressure and the control of the boost pressure is performed by means of a closed-loop system, the OBD system shall detect a malfunction when the boost system cannot increase the boost pressure to achieve the demanded boost pressure.

Such a malfunction shall not be classified as a Class C failure.

- 2 In the case where the emissions would not exceed the OBD threshold limits even upon total failure of the boost system's ability to maintain the demanded boost pressure and the control of the boost pressure is performed by means of an open-loop system, the OBD system shall detect a malfunction when the system has no detectable amount of boost pressure when boost pressure is expected.

Such a malfunction shall not be classified as a Class C failure.

Appendix 3 - Item 9

Variable Valve Timing (VVT) System

The OBD system shall monitor the following elements of the Variable Valve Timing (VVT) System on engines so-equipped for proper operation:

- (a) VVT target error: VVT system's ability to achieve the commanded valve timing - performance monitoring.
- (b) VVT slow response: VVT system's ability to achieve the commanded valve timing within a manufacturer specified time interval following the command-performance monitoring.

Appendix 3 - Item 10

Misfire Monitoring

	DIESEL	GAS
No prescriptions	X	
Misfire that may cause catalyst damage (e.g. by monitoring a certain percentage of misfiring in a certain period of time)-performance monitoring.		X

Appendix 3 - Item 11

Crankcase Ventilation System Monitoring

No prescriptions

Appendix 3 - Item 12

Engine Cooling System Monitoring

The OBD system shall monitor the following elements of the engine cooling system for proper operation

- (a) Engine coolant temperature (thermostat): Stuck open thermostat. Manufacturers need not monitor the thermostat if its failure will not disable any other OBD monitors - total functional failure.

Manufacturers need not monitor the engine coolant temperature or the engine coolant temperature sensor if the engine coolant temperature or the

engine coolant temperature sensor is not used to enable closed-loop/feedback control of any emissions control systems and/or will not disable any other monitor.

Manufacturers may suspend or delay the monitor for the time to reach close loop to enable temperature if the engine is subjected to conditions that could lead to false diagnosis (e.g. vehicle operation at idle for more than 50 to 75 per cent of the warm-up time).

Appendix 3 - Item 13

Exhaust Gas and Oxygen Sensors Monitoring

The OBD system shall monitor:

	DIESEL	GAS
(a) The electrical elements of the exhaust gas sensors on engines so-equipped for proper operation according to item 1 of this Appendix – component monitoring.	X	X
(b) Both the Primary and Secondary (fuel control) oxygen sensors. These sensors are considered as exhaust gas sensors to be monitored for proper operation according to item 1 of this Appendix – component monitoring.		X

Appendix 3 - Item 14

Idle Speed Control System Monitoring

The OBD system shall monitor the electrical elements of the idle speed control systems on engines so-equipped for proper operation according to item 1 to this Appendix.

Appendix 3 - Item 15

Three Way Catalyst

The OBD system shall monitor the three-way catalyst on engines so-equipped for proper operation:

(a) Three-way Catalyst Conversion efficiency: the catalyst ability to convert NOx and CO – performance monitoring	DIESEL	GAS
		X

CHAPTER 8B - APPENDIX 4**TECHNICAL COMPLIANCE REPORT**

This report is issued by the Test Agency, according to clauses 6.3.3. and 7.3. of this Chapter, after examination of an OBD system or an emission OBD family when that system or family complies with the requirements of this Appendix.

The exact reference (including its version number) of this Appendix shall be included in this report.

The exact reference (including its version number) to this Part. shall be included.

This report contains a cover page indicating the final compliance of the OBD system or emission OBD family and the following 5 items:

- Item 1 Information concerning the OBD system
- Item 2 Information concerning the conformity of the OBD system
- Item 3 Information concerning deficiencies
- Item 4 Information concerning demonstration tests of the OBD system
- Item 5 Test protocol

The content of the technical report, including its Items, shall, at a minimum, include the elements given in the following examples.

This report shall state that reproduction or publication in extracts of this report is not permitted without the written consent of the undersigned Test Agency.

Final Compliance Report

The documentation package and the herewith described OBD system / emission OBD family comply with the requirements of this Part.

Item 1 to the Technical Compliance Report (example)

Information concerning the OBD system

1 TYPE REQUESTED APPROVAL

Information concerning the OBD system.	YES/NO
Approval of an emission OBD family	YES/NO
Approval of an OBD system as member of a certified emission OBD family	YES/NO
Extension to include a new engine system into an emission OBD family	YES/NO
Extension to address a design change that affects the OBD system	YES/NO
Extension to address a malfunction reclassification	YES/NO

2 Information Concerning the OBD system.

Approval of an individual OBD system <ul style="list-style-type: none"> - type(s)⁽¹⁾ of the engine system family (where applicable, see clause 6.1. of this Chapter), or type(s)⁽¹⁾ of the single engine system(s) - OBD description (issued by the manufacturer): reference and date 	<p>....</p> <p>....</p>
Approval of an emission OBD family <ul style="list-style-type: none"> - List of the engine families concerned by the emission OBD family (when applicable, see clause 6.1. of this Chapter) - Type⁽¹⁾ of the parent engine system within the emission OBD family - List of the engine types⁽¹⁾ within the emission OBD family - OBD description (issued by the manufacturer): reference and date 	<p>....</p> <p>....</p> <p>....</p> <p>....</p>
Approval of an OBD system as member of a certified emission OBD family <ul style="list-style-type: none"> - List of the engine families concerned by the emission OBD family (when applicable, see clause 6.1. of this Chapter) - Type⁽¹⁾ of the parent engine system within the emission OBD family - List of the engine types⁽¹⁾ within the emission OBD family - Name of the engine system family concerned by the new OBD system (when applicable) - Type⁽¹⁾ of the engine system concerned by the new OBD system - Extended OBD description (issued by the manufacturer): reference and date 	<p>....</p> <p>....</p> <p>....</p> <p>....</p> <p>....</p> <p>....</p>

(1) As reported in the approval document

Extension to include a new engine system into an emission OBD family <ul style="list-style-type: none"> - List (extended if necessary) of the engine families concerned by the emission OBD family (when applicable, see clause 6.1. of this Chapter). 	<p>....</p> <p>....</p> <p>....</p>
--	-------------------------------------

<ul style="list-style-type: none"> - List (extended if necessary) of the engine types⁽¹⁾ within the emission OBD family - Actualized (new or unchanged) type⁽¹⁾ of the parent engine system within the emission OBD family - Extended OBD description (issued by the manufacturer): reference and date 	<p>....</p>
<p>Extension to address a design change that affects the OBD system</p> <ul style="list-style-type: none"> - List of the engine families (when applicable) concerned by the design change - List of the engine types⁽¹⁾ concerned by the design change - Actualized (when applicable, new or unchanged) type⁽¹⁾ of the parent engine system within the emission OBD family <p>Modified OBD description (issued by the manufacturer): reference and date</p>	<p>....</p> <p>....</p> <p>....</p> <p>....</p>
<p>Extension to address a malfunction reclassification</p> <ul style="list-style-type: none"> - List of the engine families (when applicable) concerned by the reclassification - List of the engine types⁽¹⁾ concerned by the reclassification <p>Modified OBD description (issued by the manufacturer): reference and date</p> <p>⁽¹⁾ As reported in the approval document</p>	<p>....</p> <p>....</p> <p>....</p>

Item 2 to the technical compliance report (example)

Information concerning the conformity of the OBD system

1. Documentation Package

<p>The elements provided by the manufacturer in the documentation package of the emission OBD family, is complete and complies with the requirements of clause 8. of this Chapter, on the following issues:</p>	
---	--

- Documentation associated with each monitored component or system	YES / NO
- Documentation associated with each DTC	YES/NO
- Documentation associated with the malfunction classification	YES /NO
- Documentation associated with the emission OBD family	YES / NO
The documentation required in clause 8.2. of this Chapter for installing an OBD system in a vehicle has been provided by the manufacturer in the documentation package, is complete, and complies with the requirements of this Chapter:	YES / NO
The installation of the engine system equipped with the OBD system complies with Appendix 1 of this Chapter	YES / NO

2 Content of the Documentation

Monitoring The monitors comply with the requirements of clause 4.2. of this Chapter:	YES / NO
Classification The malfunction classification complies with the requirements of clause 4.5. of this Chapter	YES / NO
MI activation scheme According to clause 4.6.3. of this Chapter, the MI-activation scheme is: The activation and the extinguishing of the malfunction indicator comply with the requirements of clause 4.6. of this Chapter:	Discriminatory / Non-discriminatory YES / NO
DTCs recording & erasing The recording and erasing of DTCs comply with the requirements of clauses 4.3. and 4.4. of this Chapter:	YES / NO
Disablement of the OBD system The strategies described in the documentation package for a momentary disconnection or disablement of the OBD system comply with the requirements of clause 5.2. of this Chapter	YES / NO
Electronic system security The measures described by the manufacturer for electronic system security comply with the requirements of clause 4.8. of this Chapter:	YES / NO

**Item 3 to the Technical Compliance Report (example)
Information Concerning Deficiencies**

Number of deficiencies of OBD system	(ex: 4 deficiencies)
The deficiencies comply with the requirements of clause 6.4. of this Chapter	YES / NO
Deficiency No. 1	
- Object of the deficiency	e.g. measuring of the urea concentration (SCR) within defined tolerances
- Period of the deficiency	e.g. one year / six months after the date of approval
(Description of deficiencies 2 to n-1)	
Deficiency No. n	
- Object of the deficiency	e.g. measuring of NH ₃ concentration behind SCR system
- Period of the deficiency	e.g. one year / six months after the date of approval

Item 4 to the Technical Compliance Report (example)

Demonstration tests of the OBD system

1.	Test result of the OBD system	
	Results of the tests The OBD system described in the above complying documentation package has been tested with success according to clause 6 of this Chapter for demonstrating the compliance of monitors and of malfunction classifications as listed in item 5:	YES/NO
	Details to the conducted demonstration tests are given in item 5.	
1.1	OBD System Tested on the Engine Test Bed	
	Engine <ul style="list-style-type: none"> - Engine name (manufacturer and commercial names): - Engine type (as reported in the approval document): - Engine number (serial number): 	
	Control units concerned by this Chapter (incl. engine ECUs) <ul style="list-style-type: none"> - Main functionality: - Identification number (software and calibration): 	
	Diagnostic tool (scan tool used during testing) <ul style="list-style-type: none"> - Manufacturer: - Type: - Software / version 	
	Test information <ul style="list-style-type: none"> - Ambient testing conditions (temperature, humidity, pressure): - Place of test (incl. altitude): - Reference fuel: - Engine lubricating oil: - Date of test: 	

2	Demonstration tests of the installation of the OBD system	
	In addition to the demonstration of the OBD system / emission OBD family, the installation of the OBD system / of the OBD systems within the emission OBD family has been tested on a vehicle, according to the provisions of Appendix 1 of this Chapter	YES/NO
2.1	Test result of the installation of the OBD system	
	Results of the test If the installation of the OBD system has been tested on a vehicle, the installation of the OBD system has been tested with success according to Appendix 1 of this Chapter.	YES/NO
2.2	Tested installation	
	If the installation of the OBD system has been tested on a vehicle:	
	Tested vehicle <ul style="list-style-type: none"> - Vehicle name (manufacturer and commercial names): - Vehicle type: - Vehicle Identification Number (VIN):
	Diagnostic tool (scan tool used for testing) <ul style="list-style-type: none"> - Manufacturer: - Type: - Software / version:
	Test information <ul style="list-style-type: none"> - Place and date:

Item 5 to the technical compliance report (example)

Test protocol

OBD System Demonstration Test																
- General -		- Demonstration of the Failure Classification -							- Demonstration of the OBD Performance -							
		- Test -		- Emission Level -		- Classification -			- Qualification of the Deteriorated Component -				- MI Activation -			
Failure Mode	Fault Code	Tested according to point	Test Cycle	above OTL	below OTL	below EL + X	Manufacturer proposed Classification	Final Classification (1)	Tested according to point	Test Cycle	qualified	Tested according to point	Test Cycle	Continuous MI after ... cycle	short MI after ... cycle	On-demand MI after ... cycle
SCR System Dosing Valve	P 2...	not tested		-	-	-	A	A	6.3.2.1	WHTC	yes	6.3.1	WHTC	2nd		
EGR Valve Electrical	P 1...	not tested					A	B1	6.3.2.1	WHTC	yes	6.3.1	WHTC		1st	
EGR Valve Mechanical	P 1...	not tested					B1	B1	6.3.2.1	WHTC	yes	6.3.1	WHTC		2nd	
EGR Valve Mechanical	P 1...	6.2.2	WHTC		X		B1	B1	not tested		yes					
EGR Valve Mechanical	P 1...	6.2.2	WHTC		X		B1	B1	6.3.2.1	WHTC	yes	6.3.1	WHTC		2nd	
Air Temp. Sensor Electrical	P 1...	Not tested					B2	B2	6.3.2.2	WHTC	yes	6.3.1	WHTC		1st	
Oil Temp. Sensor Electrical	P 1...	6.2.6	ETC			X	C	C	not tested		yes					

Remarks: 1) Upon request of the certification authority the failure may be re-classified into a class different from the one proposed by the manufacturer.

Only the failures that have been tested either for classification or for performance and the failures that have been reclassified at the verification authority request are listed in this sheet

A malfunction may be tested either for its classification, or for its performance, or for both.
Example given of the EGR mechanical value gives the way each of these 3 cases are considered in the table

CHAPTER 8B - APPENDIX 5**FREEZE FRAME AND DATA STREAM INFORMATION**

The following Tables list the pieces of information that are considered in clauses 4.7.1.4. and 4.7.2. of this Chapter.

Table 1**Mandatory Requirements**

	Freeze frame	Data stream
Calculated load (engine torque as a percentage of maximum torque available at the current engine speed)	x	x
Engine speed	x	x
Engine coolant temperature (or equivalent)	x	x
Barometric pressure (directly measured or estimated)	x	x
Reference maximum engine torque		X
Net brake engine torque (as percentage of reference max. engine torque), or actual engine torque/indicated torque (as percentage of reference max. engine torque, e.g. calculated from commanded injection fuel quantity)		X
Friction torque (as percentage of reference max. engine torque)		X
Engine fuel flow		X

Table 2**Optional Engine Speed and Load Information.**

	Freeze frame	Data stream
Driver's demand engine torque (as a percentage of maximum engine torque)	x	x
Actual engine torque (calculated as a percentage of maximum engine torque, e.g. calculated from commanded injection fuel quantity)	x	x
Reference maximum engine torque as a function of engine speed		x
Time elapsed since engine start	x	x

Table 3

**Optional Information, if Used by the Emission or
the OBD System to Enable or Disable any OBD Information**

	Freeze frame	Data stream
Fuel level (e.g. percentage of the nominal capacity of the fuel tank) or tank fuel pressure (e.g. percentage of the usable range of fuel tank pressure), as appropriate	<i>x</i>	<i>x</i>
Engine oil temperature	<i>x</i>	<i>x</i>
Vehicle speed	<i>x</i>	<i>x</i>
Status of the fuel quality adaptation (active / not active) in case of gas engines		<i>x</i>
Engine control computer system voltage (for the main control chip)	<i>x</i>	<i>x</i>

Table 4

**Optional Information, If the Engine is so Equipped, Senses or
Calculates the Information**

	Freeze frame	Data stream
Absolute throttle position / intake air throttle position (position of valve used to regulate intake air)	x	x
Diesel fuel control system status in case of a close loop system (e.g. in case of a fuel pressure close loop system)	x	x
Fuel rail pressure	x	x
Injection control pressure (i.e. pressure of the fluid controlling fuel injection)	x	x
Representative fuel injection timing (beginning of first main injection)	x	x
Commanded fuel rail pressure,	x	x
Commanded injection control pressure (i.e. pressure of the fluid controlling fuel injection)	x	x
Intake air temperature	x	x
Ambient air temperature	x	x
Turbocharger inlet / outlet air temperature (compressor and turbine)	x	x

Turbocharger inlet / outlet pressure (compressor and turbine)	x	x
Charge air temperature (post intercooler if fitted)	x	x
Actual boost pressure	x	x
Air flow rate from mass air flow sensor	x	x
Commanded EGR valve duty cycle/position, (provided EGR is so controlled)	x	x
Actual EGR valve duty cycle/position	x	x
PTO status (active or not active)	x	x
Accelerator pedal position	x	x
Redundant absolute pedal position	x	if sensed
Instantaneous fuel consumption	x	x
Commanded/target boost pressure (if boost pressure used to control turbo operation)	x	x
DPF inlet pressure	x	x
DPF outlet pressure	x	x
DPF delta pressure	x	x
Engine-out exhaust pressure	x	x
DPF inlet temperature	x	x
DPF outlet temperature	x	x
Engine-out exhaust gas temperature	x	x
Turbocharger/turbine speed	x	x
Variable geometry turbo position	x	x
Commanded variable geometry turbo position	x	x
Wastegate valve position	x	x
Air/fuel ratio sensor output		x
Oxygen sensor output		x
Secondary Oxygen sensor output (when fitted)		x
NOx sensor output		x

CHAPTER 8B - APPENDIX 6

REFERENCE STANDARD DOCUMENTS

This Appendix contains the references to the industry standards that are to be used in accordance to the provisions in this Chapter to provide the serial communications interface to the vehicle/engine. There are two allowed solutions identified:

- (a) ISO 27145 with either ISO 15765-4 (CAN based) or with ISO 13400 (TCP/IP based),
- (b) SAE J1939-73.

In addition, there are other ISO or SAE standards that are applicable in accordance with the provisions of this Chapter.

Reference by this Chapter to ISO 27145 means reference to:

- (a) ISO 27145-1 -Road vehicles — Implementation of WWH-OBD communication requirements — Part 1 — General Information and use case definitions
- (b) ISO 27145-2-Road vehicles — Implementation of WWH-OBD communication requirements — Part 2 — Common emissions-related data dictionary;
- (c) ISO 27145-3-Road vehicles — Implementation of WWH-OBD communication requirements — Part 3 — Common message dictionary;
- (d) ISO 27145-4-Road vehicles — Implementation of WWH-OBD communication requirements — Part 4 — Connection between vehicle and test equipment.

Reference by this Chapter to J1939-73 means reference to:

J1939-73 "APPLICATION LAYER - DIAGNOSTICS", dated on year 2011.

Reference by this Chapter to ISO 13400 means reference to:

- (a) FDIS 13400-1: 2011 Road vehicles — Diagnostic communication over Internet Protocol (DoIP) - Part 1: General information and use case definition;
- (b) FDIS 13400-3: 2011 Road vehicles — Diagnostic communication over Internet Protocol (DoIP) - Part 2: Network and transport layer requirements and services;
- (c) FDIS 13400-3: 2011 Road vehicles — Diagnostic communication over Internet Protocol (DoIP) — Part 3: IEEE 802.3 based wired vehicle interface;
- (d) [not yet finalized] 13400-4: 2011 Road vehicles — Diagnostic communication over Internet Protocol (DoIP) — Part 4: Ethernet-based high-speed data link connector.

CHAPTER 8B - APPENDIX 7

PERFORMANCE MONITORING

1.0 GENERAL

- 1.1. This Appendix sets out provisions relating to the demonstration process applicable in some cases of performance monitoring.

2.0 DEMONSTRATION OF PERFORMANCE MONITORING

- 2.1. Approval of the failure classification

- 2.1.1. As specified in clause 4.2.1.1 of this Chapter, in the case of performance monitoring no correlation to actual emissions is necessary. However, the Test Agency may request test data in order to verify the classification of the malfunction effects as described in clause 6.2. of this Chapter.

2.2. Approval of the performance monitoring selected by the manufacturer

- 2.2.1. In arriving at an approval decision on the choice of the performance monitoring selected by the manufacturer, the Test Agency shall consider technical information provided by the manufacturer.

- 2.2.2. The performance threshold selected by the manufacturer for the monitor under consideration shall be determined on the parent engine of the OBD engine family during a qualification test performed as follows:

- 2.2.2.1. The qualification test is performed in the same way as specified in clause 6.3.2. of this Chapter.

- 2.2.2.2. The decrease of performance of the component under consideration is measured and subsequently serves as the performance threshold for the parent engine of the OBD engine family.

- 2.2.3. The performance monitoring criteria approved for the parent engine will be considered to be applicable to all other members of the OBD engine family without further demonstration.

- 2.2.4. Upon agreement between the manufacturer and the Test Agency, adaption of the performance threshold to different members of the OBD family in order to cover different design parameters (for example EGR cooler size) shall be possible. Such agreement shall be based on technical elements showing its pertinence.

- 2.2.4.1. At the request of the Test Agency, a second member of the OBD engine family may be subjected to the approval process described in clause 2.2.2. of this Appendix.

2.3. **Qualification of a deteriorated component**

2.3.1. For the purpose of demonstrating the OBD performance of the selected monitor of an OBD engine family, a deteriorated component shall be qualified on the parent engine of the OBD engine family in accordance with clause 6.3.2. of this Chapter.

2.3.2. In case of a second engine tested in accordance with clause 2.2.4.1 of this Appendix, the deteriorated component shall be qualified on that second engine in accordance with clause 6.3.2 of this Chapter.

2.4. **Demonstration of the OBD performance**

2.4.1. The demonstration of the OBD performance shall be conducted according to the requirements of clause 7.1.2. of this Chapter using the qualified deteriorated component that is qualified for use with the parent engine.

CHAPTER 8B - APPENDIX 8
DEMONSTRATION REQUIREMENTS IN CASE OF
PERFORMANCE MONITORING OF A WALL-FLOW
DIESEL PARTICULATE FILTER

1.0 GENERAL

- 1.1. This Appendix specifies the OBD demonstration process applicable in the case where the filtering process of a wall-flow diesel particulate filter (DPF) is subject to performance monitoring.
- 1.1.1. A deteriorated wall-flow DPF can be created, for example, by drilling holes into the DPF substrate or by grinding the end caps of the DPF substrate.

2.0 QUALIFICATION TEST

2.1. Principle

- 2.1.1. A deteriorated wall-flow DPF is considered as a "Qualified Deteriorated Component" if, under the operating conditions of the engine specified for the purpose of that test, the pressure drop ("delta pressure") across that deteriorated wall-flow DPF exceeds or is no less than 60% of the pressure drop measured across a clean and non-deteriorated wall-flow DPF of the same type.
- 2.1.1.1. The manufacturer shall demonstrate that this clean and non-deteriorated wall-flow DPF leads to the same back-pressure as the deteriorated one before its deterioration.
- 2.1.2. Upon request of the manufacturer, the Test Agency may accept per derogation a pressure drop threshold of 50% instead of 60%. In order to apply for that derogation, the manufacturer shall justify his request by sound technical arguments, such as the spread in new filter quality, etc.

2.2. Qualification Process

- 2.2.1. For qualifying a deteriorated wall-flow DPF, the engine equipped with that wall-flow DPF shall be operated under stabilized steady-state conditions, set at the speed and load values specified for mode 9 in the WHSC test cycle specified in Chapter 3 of this Part. (55% normalized speed and 50% normalized torque).
- 2.2.2. To qualify a deteriorated wall-flow DPF as a "Qualified Deteriorated Component", the manufacturer shall demonstrate that the pressure drop across that deteriorated wall-flow DPF, measured when the engine system is operated under the conditions specified in clause 2.2.1. of this Appendix, is no less than the percentage of the pressure drop across a clean and non-deteriorated DPF under the same conditions which is applicable in accordance with clauses 2.1.1 and 2.1.2 of this Appendix.

2.3. Demonstration of the OBD performance

- 2.3.1. The demonstration of the OBD performance shall be conducted in accordance with the requirements of clause 7.1.2 of this Chapter with the qualified deteriorated wall-flow DPF mounted on the parent engine system

CHAPTER 8C

**TECHNICAL REQUIREMENTS FOR ASSESSING THE
IN-USE PERFORMANCE OF
ON-BOARD DIAGNOSTIC SYSTEMS (OBD)**

1.0 APPLICABILITY

In its current version, this Chapter is only applicable to road-vehicles equipped with a diesel engine

2.0 RESERVED**3.0 DEFINITIONS****3.1 "In-Use performance ratio"**

The in-use performance ratio (IUPR) of a specific monitor m of the OBD system is:

$$\text{IUPR}_m = \text{Numerator}_m / \text{Denominator}_m$$

3.2. "Numerator"

The numerator of a specific monitor m (Numerator_m) is a counter indicating the number of times a vehicle has been operated such that all monitoring conditions necessary for that specific monitor to detect a malfunction have been encountered.

3.3 "Denominator"

The denominator of a specific monitor m (Denominator_m) is a counter indicating the number of vehicle driving events, taking into account conditions specific to that specific monitor.

3.4 "General Denominator"

The general denominator is a counter indicating the number of times a vehicle has been operated, taking into account general conditions.

3.5 Abbreviations

IUPR In-Use Performance Ratio

IUPR_m In-Use Performance Ratio of a specific monitor m

4.0 GENERAL REQUIREMENTS

The OBD system shall have the capability of tracking and recording in-use performance data (clause 6. of this Chapter) of the OBD monitors specified in this paragraph, of storing these data in computer memory and communicating them off-board upon request (clause 7. of this Chapter).

The in-use performance data of a monitor consists of the numerator and denominator enabling the calculation of the IUPR.

4.1 IUPR Monitors

4.1.1 Group of Monitors

Manufacturers shall implement software algorithms in the OBD system to individually track and report in-use performance data of the groups of monitors mentioned in Appendix 1 of this Chapter.

Manufacturers are not required to implement software algorithms in the OBD system to individually track and report in-use performance data of monitors running continuously as defined in clause 4.2.3. of Chapter 8B of this Part if these monitors are already part of one of the groups of monitors mentioned in Appendix 1 of this Chapter.

In-use performance data of monitors associated to different exhaust lines or engine banks within a group of monitors shall be tracked and recorded separately as specified in clause 6 and reported as specified in clause 7. of this Chapter.

4.1.2 Multiple monitors

For each group of monitors which are required to be reported by clause 4.1.1. of this Chapter, the OBD system shall separately track in-use performance data, as specified in clause 6. of this Chapter, for each of the specific monitors belonging to that group.

4.2 Limitation of the use of in-use performance data

In-use performance data of a single vehicle are used for the statistical evaluation of the in-use performance of the OBD system of a larger group of vehicles.

Contrary to other OBD data, in-use performance data cannot be used to draw conclusions concerning the road-worthiness of an individual vehicle.

5.0 REQUIREMENTS FOR CALCULATING IN-USE PERFORMANCE RATIOS

5.1 Calculation of the In-Use Performance Ratio

For each monitor m considered in the present Chapter, the in-use performance ratio is calculated with the following formula:

$$IUPR_m = \text{Numerator}_m / \text{Denominator}_m$$

where the Numerator_m and Denominator_m are incremented according to the specifications of this clause

5.1.1 Requirements for the ratio when calculated and stored by system

Each $IUPR_m$ ratio shall have a minimum value of zero and a maximum value of 7.99527 with a resolution of 0.000122⁽¹⁾.

A ratio for a specific component shall be considered to be zero whenever the corresponding numerator is equal to zero and the corresponding denominator is not zero.

A ratio for a specific component shall be considered to be the maximum value of 7.99527 if the corresponding denominator is zero or if the actual value of the numerator divided by the denominator exceeds the maximum value of 7.99527

- (1) This value corresponds to a maximum hexadecimal value of 0xFFFF with a resolution of 0x1.

5.2 Requirements for Incrementing the Numerator

The numerator shall not be incremented more than once per driving cycle.

The numerator for a specific monitor shall be incremented within 10 seconds if and only if the following criteria are satisfied on a single driving cycle:

- (a) Every monitoring condition necessary for the monitor of the specific component to detect a malfunction and store a potential DTC has been satisfied, including enable criteria, presence or absence of related DTCs, sufficient length of monitoring time, and diagnostic executive priority assignments (e.g., diagnostic "A" shall execute prior to diagnostic "B").

Note: For the purpose of incrementing the numerator of a specific monitor, it may not be sufficient to satisfy all the monitoring conditions necessary for that monitor to determine the absence of a malfunction.

- (b) For monitors that require multiple stages or events in a single driving cycle to detect a malfunction, every monitoring condition necessary for all events to have been completed shall be satisfied.
- (c) For monitors which are used for failure identification and that run only after a potential DTC has been stored, the numerator and denominator may be the same as those of the monitor detecting the original malfunction.
- (d) For monitors that require an intrusive operation to further investigate the presence of a malfunction, the manufacturer may submit to the Test Agency an alternative way to increment the numerator. This alternative should be equivalent to that which would, had a malfunction been present, have permitted to increment the numerator.

For monitors that run or complete during engine-off operation, the numerator shall be incremented within 10 seconds after the monitor has completed during engine-off operation or during the first 10 seconds of engine start on the subsequent driving cycle.

5.3 Requirements for Incrementing the Denominator

5.3.1 General incrementing rules

The denominator shall be incremented once per driving cycle, if during this driving cycle:

- (a) The general denominator is incremented as specified in clause 5.4. of this Chapter, and
- (b) The denominator is not disabled according to clause 5.6. of this Chapter, and
- (c) When applicable, the specific additional incrementing rules specified in clause 5.3.2. of this Chapter are met.

5.3.2 Additional Monitor Specific Incrementing Rules

5.3.2.1 Specific denominator for evaporative system (Reserved)

5.3.2.2 Specific denominator for secondary air systems (Reserved)

5.3.2.3 Specific denominator for components / systems that operate at engine start-up only

In addition to the requirements of paragraph 5.3.1. (a) and (b), the denominator(s) for monitors of components or systems that operate only at engine start-up shall be incremented if the component or strategy is commanded "on" for a time greater than or equal to 10 seconds.

For purposes of determining this commanded "on" time, the OBD system may not include time during intrusive operation of any of the components or strategies later in the same driving cycle solely for the purposes of monitoring.

5.3.2.4 Specific denominator for components or systems that are not continuously commanded to function

In addition to the requirements of clause 5.3.1. (a) and (b), the denominator(s) for monitors of components or systems that are not continuously commanded to function (e.g. Variable Valve Timing systems - VVT- or EGR valves), shall be incremented if that component or system is commanded to function (e.g., commanded "on", "open", "closed", "locked") on two or more occasions during the driving cycle, or for a cumulative time greater than or equal to 10 seconds, whichever occurs first.

5.3.2.5 **Specific denominator for DPF**

In addition to the requirements of clause 5.3.1. (a) and (b), in at least one driving cycle the denominator(s) for DPF shall be incremented if at least 800 cumulative kilometers of vehicle operation or alternatively at least 750 minutes of engine run time have been experienced since the last time the denominator was incremented.

5.3.2.6 **Specific Denominator for Oxidation Catalysts**

In addition to the requirements of clause 5.3.1 (a) and (b), in at least one driving cycle the denominator(s) for monitors of oxidation catalyst used for the purpose of DPF active regeneration shall be incremented if a regeneration event is commanded for a time greater than or equal to 10 seconds.

5.3.2.7 **Specific denominator for hybrids (reserved)**

5.4 **Requirements for incrementing the general denominator**

The general denominator shall be incremented within 10 seconds, if and only if, all the following criteria are satisfied on a single driving cycle:

- (a) Cumulative time since start of driving cycle is greater than or equal to 600 seconds while remaining:
 - (i) At an elevation of less than 2,500 meters above sea level, and
 - (ii) At an ambient temperature of greater than or equal to 273 K (0°C), and Temperature boundary conditions will be reviewed based on data collection.
 - (iii) At an ambient temperature of lower than or equal to 315 K (42°C).
- (b) Cumulative engine operation at or above 1150 min⁻¹ for greater than or equal to 300 seconds while under the conditions specified in the above subparagraph (a); as alternatives left to the manufacturer an engine operation at or above 15 per cent calculated load or a vehicle operation at or above 40 km/h may be used in lieu of the 1150 min⁻¹ criterion.
- (c) Continuous vehicle operation at idle (e.g., accelerator pedal released by driver and either vehicle speed less than or equal to 1.6 km/h or engine speed less than or equal to 200 min⁻¹ above normal warmed-up idle) for greater than or equal to 30 seconds while under the conditions specified in the above sub-paragraph (a).

5.5. **Requirements for incrementing the ignition cycle counter**

The ignition cycle counter shall be incremented once and only once per engine start.

5.6. **Incrementing disablement of the numerators, of the denominators and of the general denominator**

- 5.6.1 Within 10 seconds of a malfunction being detected (i.e. a potential or a confirmed and active DTC is stored), which disables a monitor, the OBD system shall disable further incrementing of the corresponding numerator and denominator for each monitor that is disabled.

When the malfunction is no longer detected (e.g. the potential DTC is erased through self-clearing or through a scan-tool command), incrementing of all corresponding numerators and denominators shall resume within 10 seconds.

- 5.6.2 Within 10 seconds of the start of operation of a Power Take-Off unit (PTO) that disables a monitor as permitted in clause 5.2.5. of Chapter 8B of this Part, the OBD system shall disable further incrementing of the corresponding numerator and denominator for each monitor that is disabled.

When the PTO operation ends, incrementing of all corresponding numerators and denominators shall resume within 10 seconds.

- 5.6.3. In the case of a malfunction (i.e. a potential or confirmed and active DTC has been stored) preventing determination of whether the criteria for the Denominator_m of a monitor m mentioned in clause 5.3. of this Chapter are satisfied⁽¹⁾, the OBD system shall disable further incrementing the Numerator_m and Denominator_m within 10 seconds.

Incrementing the Numerator_m and Denominator_m shall resume within 10 seconds when the malfunction is no longer present (e.g., pending code erased through self-clearing or by a scan tool command).

⁽¹⁾ e.g. vehicle speed / engine speed / calculated load, ambient temperature, elevation, idle operation, or time of operation.

- 5.6.4. In the case of a malfunction (i.e. a potential or confirmed and active DTC has been stored) preventing determination of whether the criteria for the General denominator mentioned in clause 5.4. of this Chapter are satisfied, the OBD system shall disable further incrementing the general denominator within 10 seconds.

Incrementing the general denominator shall resume within 10 seconds when the malfunction is no longer present (e.g., pending code erased through self-clearing or by a scan tool command).

The general denominator may not be disabled from incrementing for any other condition.

6.0 REQUIREMENTS FOR TRACKING AND RECORDING IN-USE PERFORMANCE DATA

For each group of monitors listed in Appendix 1 of this Chapter, the OBD system shall separately track numerators and denominators for each of the specific monitors listed in Appendix 3 of Chapter 8B of this Part and belonging to that group.

It shall report only the corresponding numerator and denominator for the specific monitor that has the lowest numerical ratio.

If two or more specific monitors have identical ratios, the corresponding numerator and denominator for the specific monitor that has the highest denominator shall be reported for the specific group of monitors.

In order to determine without bias the lowest ratio of a group, only the monitors specifically mentioned in that group shall be taken into consideration (e.g. a NOx sensor when used to perform one of the monitors listed in Chapter 8B, Appendix 3, item 3 "SCR" will be taken into consideration into the "exhaust gas sensor" group of monitors and not in the "SCR" group of monitors)

The OBD system shall also track and report the general denominator and the ignition cycle counter.

Note: According to clause 4.1.1. of this Chapter, manufacturers are not required to implement software algorithms in the OBD system to individually track and report numerators and denominators of monitors running continuously.

7.0 REQUIREMENTS FOR STORING AND COMMUNICATING IN-USE PERFORMANCE DATA

Communication of the in-use performance data is a new use-case and is not included in the three existing use-cases which are dedicated to the presence of possible malfunctions.

7.1 Information about in-use performance data

The information about in-use performance data recorded by the OBD system shall be available upon off-board request according to clause 7.2. of this Chapter.

This information will provide Test Agencies with in use performance data.

The OBD system shall provide all information (according to the applicable standard set in Appendix 6 of Chapter 8B of this Part) for the external IUPR test equipment to assimilate the data and provide an inspector with the following information:

- (a) The VIN (vehicle identification number),
- (b) The numerator and denominator for each group of monitors recorded by the system according to clause 6. of this Chapter,
- (c) The general denominator,
- (d) The value of the ignition cycle counter,
- (e) The total engine running hours,
- (f) Confirmed and active DTCs for Class A malfunctions,
- (g) Confirmed and active DTCs for Class B (B1 and B2) malfunctions

This information shall be available through "read-only" access (i.e. no clearing).

7.2 Access to in-use performance data

Access to in-use performance data shall be provided only in accordance with the standards mentioned in Appendix 6 of Chapter 8B and the following sub-clauses ⁽¹⁾.

Access to the in-use performance data shall not be dependent on any access code or other device or method obtainable only from the manufacturer or its suppliers. Interpretation of the in-use performance data shall not require any unique decoding information, unless that information is publicly available.

The access method (i.e. the access point/node) to in-use performance data shall be the same as the one used to retrieve all OBD information. This method shall permit access to the complete in-use performance data required by this Chapter.

- (1) The manufacturer is allowed to use an additional on-board diagnostic display, such as a dashboard mounted video display device, for providing access to in-use performance data. Such an additional device is not subject to the requirements of this Chapter.

7.3 Reinitializing in-use performance data

7.3.1 Reset to Zero

Each number shall be reset to zero only when a non-volatile random access memory (NVRAM) reset occurs (e.g., reprogramming event). Numbers may not be reset to zero under any other circumstances including when a scan tool command to clear fault codes is received.

7.3.2 Reset in case of memory overflow

If either the numerator or denominator for a specific monitor reaches $65,535 \pm 2$, both numbers shall be divided by two before either is incremented again to avoid overflow problems.

If the ignition cycle counter reaches the maximum value of $65,535 \pm 2$, the ignition cycle counter may rollover and increment to zero on the next ignition cycle to avoid overflow problems.

If the general denominator reaches the maximum value of $65,535 \pm 2$, the general denominator may rollover and increment to zero on the next driving cycle that meets the general denominator definition to avoid overflow problems.

CHAPTER 8C - APPENDIX 1

GROUPS OF MONITERS

The groups of monitors considered in this Chapter are the following:

A. **Oxidation catalysts**

The monitors specific to that group are those listed in item 5 of Appendix 3 of Chapter 8B of this Part.

B. **Selective Catalytical Reduction Systems (SCR)**

The monitors specific to that group are those listed in item 3 of Appendix 3 of Chapter 8B of this Part.

C. **Exhaust gas and oxygen sensors**

The monitors specific to that group are those listed in item 13 of Appendix 3 of Chapter 8B of this Part.

D. **EGR systems and VVT**

The monitors specific to that group are those listed in items 6 and 9 and of Appendix 3 of Chapter 8B of this Part.

E. **DPF systems**

The monitors specific to that group are those listed in item 2 of Appendix 3 of Chapter 8B of this Part.

F. **Boost Pressure Control System**

The monitors specific to that group are those listed in item 8 of Appendix 3 of Chapter 8B of this Part.

G. **NO_x Adsorber**

The monitors specific to that group are those listed in item 4 of Appendix 3 of Chapter 8B of this Part.

H. **Three-way Catalyst**

The monitors specific to that group are those listed in item 15 of Appendix 3 of Chapter 8B of this Part.

I. **Evaporative Systems (reserved)**

J. **Secondary Air system (reserved)**

A specific monitor shall belong only to one of these groups

CHAPTER 9

TECHNICAL REQUIREMENTS ON OFF-CYCLE EMISSIONS (OCE) AND IN - USE EMISSIONS

1.0 APPLICABILITY

This Chapter sets out the performance requirements and prohibition of defeat strategies for engines and vehicles type-approved according to this Part so as to achieve effective control of emissions under a broad range of engine and ambient operating conditions encountered during normal in-use vehicle operation. This Chapter also sets out the test procedures for testing off-cycle emissions during type-approval and in actual use of the vehicle.

2.0 RESERVED

3.0 DEFINITIONS

- 3.1. **"Engine starting"** means the process from the initiation of engine cranking until the engine reaches a speed 150 min^{-1} below the normal, warmed up idle speed (as determined in the drive position for vehicles equipped with an automatic transmission).
- 3.2. **"Engine warm-up"** means sufficient vehicle operation such that the coolant temperature reaches a minimum temperature of at least 70°C .
- 3.3. **"Rated speed"** means the maximum full load speed allowed by the governor as specified by the manufacturer in his sales and service literature, or, if such a governor is not present, the speed at which the maximum power is obtained from the engine, as specified by the manufacturer in his sales and service literature.
- 3.4. **"Regulated emissions"** means "gaseous pollutants" defined as carbon monoxide, hydrocarbons and/or non-methane hydrocarbons (assuming a ratio of $\text{CH}_{1.85}$ for diesel, $\text{CH}_{2.525}$ for LPG and $\text{CH}_{2.93}$ for NG, and an assumed molecule $\text{CH}_3\text{O}_{0.5}$ for ethanol fuelled diesel engines), methane (assuming a ratio of CH_4 for NG) and oxides of nitrogen (expressed in nitrogen dioxide (NO_2) equivalent) and "particulate matter" (PM) defined as any material collected on a specified filter medium after diluting exhaust with clean filtered air to a temperature between 315 K (42°C) and 325 K (52°C), as measured at a point immediately upstream of the filter, this is primarily carbon, condensed hydrocarbons, and sulphates with associated water.

4.0 GENERAL REQUIREMENTS

Any engine system and any element of design liable to affect the emission of regulated pollutants shall be designed, constructed, assembled and installed so as to enable the engine and vehicle to comply with the provisions of this Chapter.

4.1. Prohibition of defeat strategies

Engine systems and vehicles shall not be equipped with a defeat strategy.

4.2. World-harmonized Not-To-Exceed Emission Requirement

This Chapter requires that engine systems and vehicles comply with the WNTe emission limit values described in clause 5.2. of this Chapter. For laboratory based testing according to clause 7.4. of this Chapter, no test result shall exceed the emissions limits specified in clause 5.2. of this Chapter.

5.0 PERFORMANCE REQUIREMENTS

5.1. Emission strategies

Emission strategies shall be designed so as to enable the engine system, in normal use, to comply with the provisions of this Chapter. Normal use is not restricted to the conditions of use as specified in clause 6. of this Chapter.

5.1.1. Requirements for Base Emission Strategies (BES)

A BES shall not discriminate between operation on an applicable type approval or certification test and other operation and provide a lesser level of emission control under conditions not substantially included in the applicable type approval or certification tests.

5.1.2. Requirements for Auxiliary Emission Strategies (AES)

An AES shall not reduce the effectiveness of the emission control relative to a BES under conditions that may reasonably be expected to be encountered in normal vehicle operation and use, unless the AES satisfies one the following specific exceptions:

- (a) Its operation is substantially included in the applicable type-approval tests, including the off-cycle test procedures under clause 7. of this Chapter and the in-service provisions set out in clause 9 of Chapter 1 of this Part;
- (b) It is activated for the purposes of protecting the engine and/or vehicle from damage or accident;
- (c) It is only activated during engine starting or warm up as defined in this Chapter;
- (d) Its operation is used to trade-off the control of one type of regulated emissions in order to maintain control of another type of regulated emissions under specific ambient or operating conditions not substantially included in the type approval or certification tests. The overall effect of such an AES shall be to compensate for the effects of extreme ambient conditions in a manner that provides acceptable control of all regulated emissions.

5.2. World-harmonized Not-To-Exceed (WNTe) limits for gaseous and Particulate Exhaust Emissions

5.2.1. Exhaust emissions shall not exceed the applicable emission limits specified in clause 5.2.2. of this Chapter.

5.2.2. The applicable emission limits shall be as specified in Gazette Notification GSR-889 (E) dated 16th September 2016 published by MoRTH, as amended from time to time

Test cycle	CO mg/kWh	THC mg/kWh	NOx mg/kWh	PM mg/kWh
WNTe	2000	220	600	16

6.0 AMBIENT AND OPERATING CONDITIONS

The WNTe emission limits shall apply at:

- (a) All atmospheric pressures greater than or equal to 82.5 kPa;
- (b) All temperatures less than or equal to the temperature determined by equation 5 at the specified atmospheric pressure:

$$T = -0.4514 \times (101.3 - pb) + 311 \quad (5)$$

Where:

T is the ambient air temperature, K

pb is the atmospheric pressure, kPa

- (c) All engine coolant temperature above 343 K (70°C).

The applicable ambient atmospheric pressure and temperature conditions are shown in Figure 1 below.

WNTe Atmospheric Pressure and Temperature Range

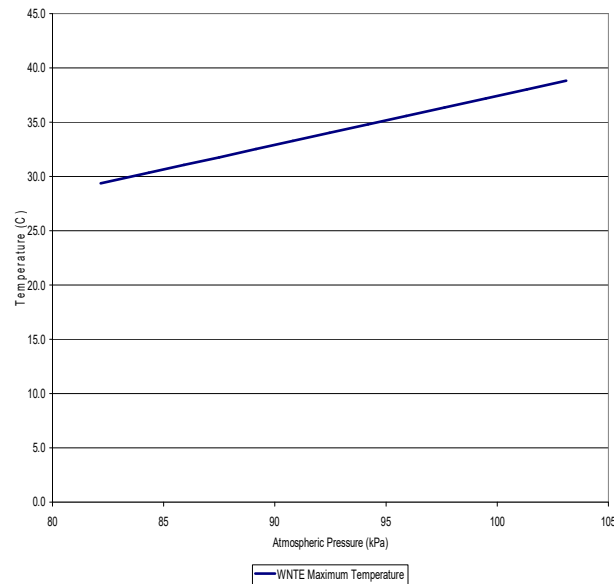


Figure 1
Illustration of Atmospheric Pressure and Temperature Conditions

7.0 OFF-CYCLE LABORATORY TESTING AT TYPE-APPROVAL

The off-cycle laboratory test requirements shall not apply for the type-approval of positive ignition engine under this Part.

7.1. World-harmonized Not-To-Exceed control area

The WNTe control area consists of the engine speed and load points defined in clauses 7.1.1. through 7.1.6. of this Chapter. Figure 2 of this Chapter is an example illustration of the WNTe control area.

7.1.1. Engine Speed Range

The WNTe control area shall include all operating speeds between the 30th percentile cumulative speed distribution over the WHTC test cycle, including idle, (n_{30}) and the highest speed where 70 per cent of the maximum power occurs (n_{hi}). Figure 3 of this Chapter is an example of the WNTe cumulative speed frequency distribution for a specific engine.

7.1.2. Engine Torque Range

The WNTe control area shall include all engine load points with a torque value greater than or equal to 30 per cent of the maximum torque value produced by the engine.

7.1.3. Engine power range

Notwithstanding the provisions of clause 7.1.1. and 7.1.2., speed and load points below 30 per cent of the maximum power value produced by the engine shall be excluded from the WNTe control area for all emissions.

7.1.4. Application of Engine Family Concept

In principal, any engine within a family with a unique torque/power curve will have its individual WNTe control area. For in-use testing, the individual WNTe control area of the respective engine shall apply. For type approval (certification) testing under the engine family concept of the WHDC GTR the manufacturer may optionally apply a single WNTe control area for the engine family under the following provisions:

- (a) A single engine speed range of the WNTe control area may be used; if the measured engine speeds n_{30} and n_{hi} are within ± 3 per cent of the engine speeds as declared by the manufacturer. If the tolerance is exceeded for any of the engine speeds, the measured engine speeds shall be used for determining the WNTe control area;
- (b) A single engine torque/power range of the WNTe control area may be used, if it covers the full range from the highest to the lowest rating of the family. Alternatively, grouping of engine ratings into different WNTe control areas is permitted.

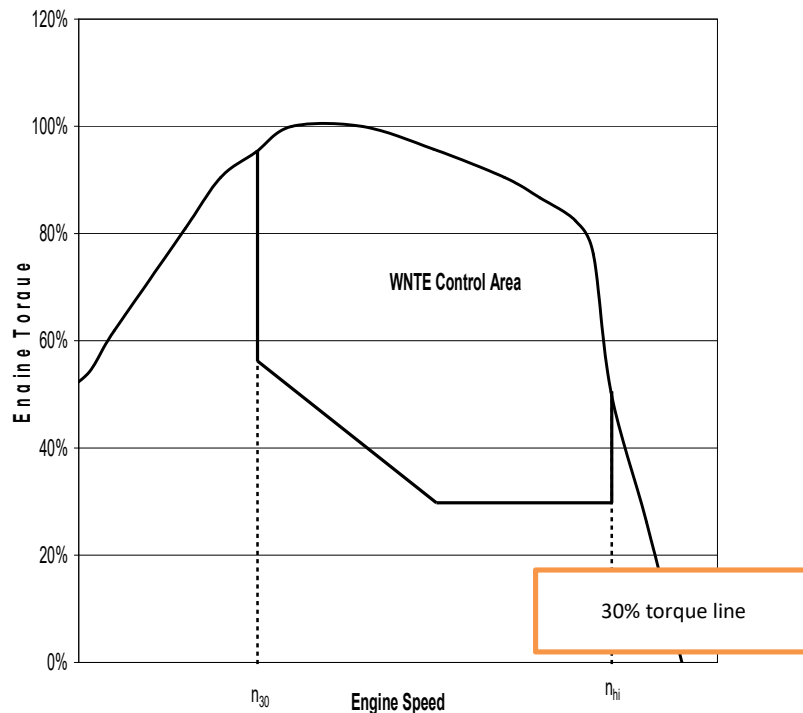


Figure 2
Example WNTe Control Area

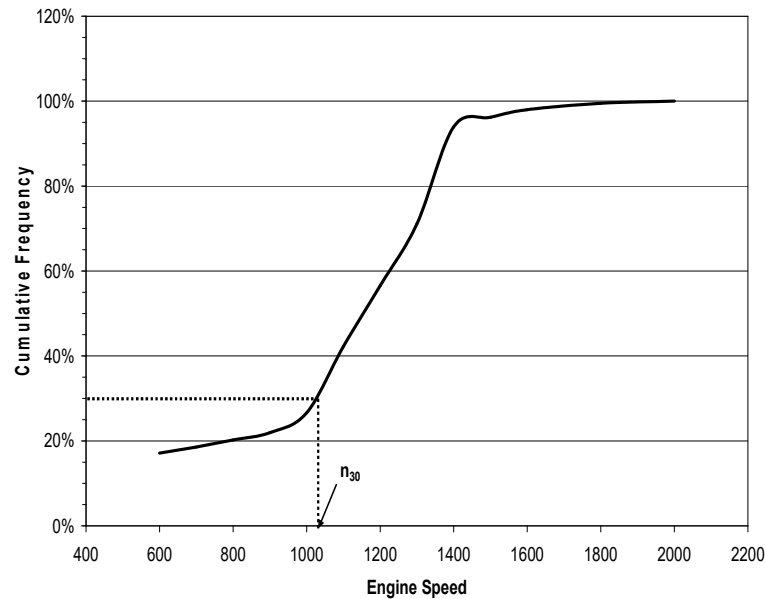


Figure 3
Example of WNTe Cumulative Speed Frequency Distribution

7.1.5. Compliance exclusion from certain WNTe operating points

The manufacturer may request that the Test Agency excludes operating points from the WNTe control area defined in clause 7.1.1 through 7.1.4 of this Chapter during the certification/type approval. The Test Agency may grant this exclusion if the manufacturer can demonstrate that the engine is never capable of operating at such points when used in any vehicle combination.

7.2. Minimum World-harmonized Not-To-Exceed event duration and data sampling frequency

7.2.1. To determine compliance with the WNTe emissions limits specified in clause 5.2. of this Chapter, the engine shall be operated within the WNTe control area defined in clause 7.1. of this Chapter and its emissions shall be measured and integrated over a minimum period of 30 seconds. A WNTe event is defined as a single set of integrated emissions over the period of time. For example, if the engine operates for 65 consecutive seconds within the WNTe control area and ambient conditions this would constitute a single WNTe event and the emissions would be averaged over the full 65 second period. In the case of laboratory testing, the integrating period defined in clause 7.5. of this Chapter shall apply.

7.2.2. For engines equipped with emission controls that include periodic regeneration events, if a regeneration event occurs during the WNTe test, then the averaging period shall be at least as long as the time between the events multiplied by the number of full regeneration events within the sampling period. This requirement only applies for engines that send an electronic signal indicating the start of the regeneration event.

- 7.2.3. A WNTe event is a sequence of data collected at the frequency of at least 1 Hz during engine operation in the WNTe control area for the minimum event duration or longer. The measured emission data shall be averaged over the duration of each WNTe event.

7.3. In-use testing

A PEMS demonstration test shall be performed at type approval by testing the parent engine in a vehicle using the procedure described in Appendix 1 of this Chapter.

- 7.3.1 The manufacturer may select the vehicle that shall be used for testing but the vehicle choice shall be subject to the agreement of the Test Agency. The characteristics of the vehicle used for the PEMS demonstration test shall be representative for the category of vehicle intended for the engine system. The vehicle may be a prototype vehicle.
- 7.3.2 At the request of the Test Agency, an additional engine within the engine family or an equivalent engine representing a different vehicle category may be tested in a vehicle.

7.4. World-harmonized Not-To-Exceed Laboratory Testing

Where the provisions of this Chapter are used as the basis for laboratory testing the following provision shall apply:

- 7.4.1. The specific mass emissions of regulated pollutants shall be determined on the basis of randomly defined test points distributed across the WNTe control area. All the test points shall be contained within 3 randomly selected grid cells imposed over the control area. The grid shall comprise of 9 cells for engines with a rated speed less than 3000 min⁻¹ and 12 cells for engines with a rated speed greater than or equal to 3000 min⁻¹. The grids are defined as follows:
- (a) The outer boundaries of the grid are aligned to the WNTe control area;
 - (b) vertical lines spaced at equal distance between engine speeds n_{30} and n_{hi} for 9 cell grids, or 3 vertical lines spaced at equal distance between engine speeds n_{30} and n_{hi} for 12 cell grids; and
 - (c) lines spaced at equal distance of engine torque ($\frac{1}{3}$) at each vertical line within the WNTe control area.

Examples of the grids applied to specific engines are shown in Figures 5 and 6 of this Chapter.

- 7.4.2. The 3 selected grid cells shall each include 5 random test points, so a total of 15 random points shall be tested within the WNTe control area. Each cell shall be tested sequentially; therefore, all 5 points in one grid cell are tested before transiting to the next grid cell. The test points are combined into a single ramped steady state cycle.

- 7.4.3. The order in which each of the grid cells are tested, and the order of testing the points within the grid cell, shall be randomly determined. The 3 grid cells to be tested, the 15 test points, the order of testing the grid cells, and the order of the points within a grid cell shall be selected by the Test Agency using acknowledged statistical methods of randomization.
- 7.4.4. The average specific mass emissions of regulated gaseous pollutants shall not exceed the WNTe limit values specified in clause 5.2. of this Chapter when measured over any of the cycles in a grid cell with 5 test points.
- 7.4.5. The average specific mass emissions of regulated particulate pollutants shall not exceed the WNTe limit values specified in clause 5.2. of this Chapter when measured over the whole 15 test point cycle.
- 7.5. Laboratory test procedure**
 - 7.5.1. After completion of the WHSC cycle, the engine shall be preconditioned at mode 9 of the WHSC for a period of three minutes. The test sequence shall start immediately after completion of the preconditioning phase.
 - 7.5.2. The engine shall be operated for 2 minutes at each random test point. This time includes the preceding ramp from the previous steady state point. The transitions between the test points shall be linear for engine speed and load and shall last 20 ± 1 seconds.
 - 7.5.3. The total test time from start until finish shall be 30 minutes. The test of each set of 5 selected random points in a grid cell shall be 10 minutes, measured from the start of the entry ramp to the 1st point until the end of the steady state measurement at the 5th point. Figure 5 of this Chapter illustrates the sequence of the test procedure.
 - 7.5.4. The WNTe laboratory test shall meet the validation statistics of clause 7.8.7. of Chapter 3 of this Part.
 - 7.5.5. The measurement of the emissions shall be carried out in accordance with clauses 7.5., 7.7. and 7.8. of Chapter 3 of this Part.
 - 7.5.6. The calculation of the test results shall be carried out in accordance with clause 8 of Chapter 3 of this Part.

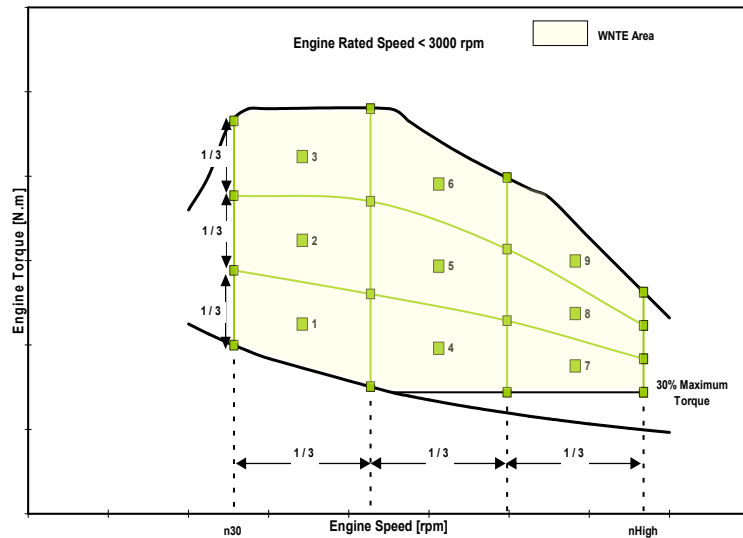


Figure 5
WNTe Test Cycle Grids

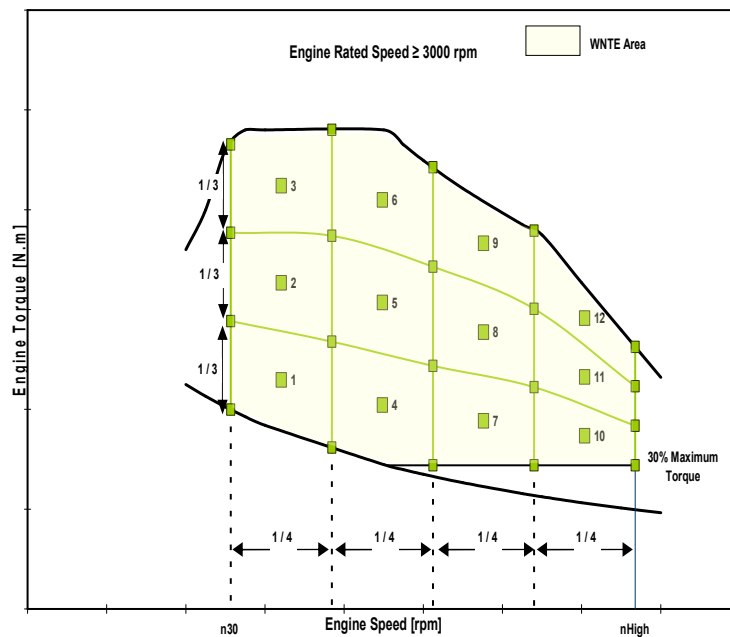


Figure 6
WNTe Test Cycle Grids

7.6. Rounding

Each final test result shall be rounded in one step to the number of places to the right of the decimal point indicated by the applicable WHDC emission standard plus one additional significant figure, in accordance with ASTM E 29-06. No rounding of intermediate values leading to the final brake specific emission result is permitted.

8.0 RESERVED**9.0 RESERVED****10.0 STATEMENT OF OFF-CYCLE EMISSION COMPLIANCE**

In the application for type-approval, the manufacturer shall provide a statement that the engine family or vehicle complies with the requirements of this Part limiting off-cycle emissions. In addition to this statement, compliance with the applicable emission limits and in use requirements shall be verified through additional tests.

10.1 Example statement of off cycle emission compliance

The following is an example compliance statement:

(Name of manufacturer) attests that the engines within this engine family comply with all requirements of this Chapter. (Name of manufacturer) makes this statement in good faith, after having performed an appropriate engineering evaluation of the emissions performance of the engines within the engine family over the applicable range of operating and ambient conditions.

10.2 Basis for off cycle emission compliance statement

The manufacturer shall maintain records at the manufacturer's facility which contain all test data, engineering analyses, and other information which provides the basis for the OCE compliance statement. The manufacturer shall provide such information to the Test Agency upon request.

11.0 DOCUMENTATION

The Test Agency may decide to require that the manufacturer provides a documentation package. This should describe any element of design and emission control strategy of the engine system and the means by which it controls its output variables, whether that control is direct or indirect.

The information may include a full description of the emission control strategy. In addition, this could include information on the operation of all AES and BES, including a description of the parameters that are modified by any AES and the boundary conditions under which the AES operate, and indication of which AES and BES are likely to be active under the conditions of the test procedures in this Chapter.

The documentation package shall be provided according to the provisions of clause 5.1.4.3 of Chapter 1 of this Part

CHAPTER 9 - APPENDIX 1

PEMS DEMONSTRATION TEST AT TYPE APPROVAL

1.1 INTRODUCTION

This Appendix describes the procedure for PEMS demonstration test at type approval.

1.2 TEST VEHICLE

1.2.1 The vehicle used for demonstrating the PEMS demonstration test shall be representative for the vehicle category intended for the installation of the engine system. The vehicle may be a prototype vehicle or an adapted production vehicle.

1.2.2 The availability and conformity of the ECU data-stream information shall be demonstrated (for example following the provision of clause 5 of Chapter 7 of this Part).

1.3 TEST CONDITIONS

1.3.1 The vehicle payload shall be 50-60 per cent of the maximum vehicle payload in accordance with Chapter 7 of this Part.

1.3.2 The test shall be conducted under ambient conditions as described in clause 4.2. of Chapter 7 of this Part.

1.3.3 The engine coolant temperature shall be in accordance with clause 4.3. of Chapter 7 of this Part.

1.3.4 The fuel, lubricating oil and reagent for the exhaust after-treatment system shall follow the provisions of clause 4.4. of Chapter 7 of this Part.

1.3.5 Trip and operational Requirements

The trip and operational requirements shall be those described in clauses 4.5. to 4.6.8. of Chapter 7 of this Part.

1.4 EMISSIONS EVALUATION

1.4.1 The test shall be conducted and the test results calculated in accordance with clause 6. of Chapter 7 of this Part.

1.5 REPORT

A technical report describing the PEMS demonstration test shall show the activities and results and give at least the following information

- (a) General information as described in clause 10.1.1. of Chapter 7 of this Part;

- (b) Explanation as to why the vehicle(s) used for the test can be considered to be representative for the category of vehicles intended for the engine system;
- (c) Information about test equipment and test data as described in clauses 10.1.3. and 10.1.4. of Chapter 7 of this Part;
- (d) Information about the tested engine as described in clause 10.1.5. of Chapter 7 of this Part;
- (e) Information about the vehicle used for the test as described in clause 10.1.6. of Chapter 7 of this Part;
- (f) Information about the route characteristics as described in clause 10.1.7. of Chapter 7 of this Part;
- (g) Information about instantaneous measured and calculated data as described in clause 10.1.8. and 10.1.9. of Chapter 7 of this Part;
- (h) Information about averaged and integrated data as described in clause 10.1.10. of Chapter 7 of this Part;
- (i) Pass-fail results as described in clause 10.1.11. of Chapter 7 of this Part;
- (j) Information about test verifications as described in clause 10.1.12. of Chapter 7 of this Part.

CHAPTER 10

REQUIREMENTS TO ENSURE THE CORRECT OPERATION OF NO_x CONTROL MEASURES

1.0 INTRODUCTION

This Chapter sets out the requirements to ensure the correct operation of NO_x control measures. It includes requirements for vehicles that rely on the use of a reagent in order to reduce emissions.

2.0 GENERAL REQUIREMENTS

Any engine system falling within the scope of this Chapter shall be designed, constructed and installed so as to be capable of meeting these requirements throughout the normal life of the engine under normal conditions of use. In achieving this objective, it is acceptable that engines which have been used in excess of the appropriate durability period referred to in clause 5.4 of Chapter 1 of this Part may show some deterioration in performance and sensitivity of the monitoring system.

2.1. ALTERNATIVE APPROVAL

2.1.1 If requested by the manufacturer for vehicles of categories M2 and N1 for vehicles of categories M1 and N2 for a technically permissible maximum laden mass not exceeding 7.5 tonnes and for vehicles of categories M3 of Type-I and Type-II (as defined in AIS-052) with a permissible mass not exceeding 7.5 tonnes compliance with the requirements of Chapter 16 of AIS-137 (Part 3) shall be considered equivalent to the compliance with this Chapter.

2.1.2 If the alternative approval is used

2.1.2.1 The information related to the correct operation of NO_x control measures in Chapter 2 of this Part is replaced by the information of AIS-137 (Part 3).

2.1.2.2 The following exceptions shall apply regarding the application of the requirements set out in Chapter 16 of AIS-137 (Part 3) and those of this Chapter.

2.1.2.2.1 The provision on reagent quality monitoring set out in clauses 7.1 to 7.1.2 of this Chapter shall apply instead of clauses 4.1 to 4.2 of Chapter 16 of AIS-137 (Part 3).

2.1.2.2.2 The provision on dosing activity monitoring set out in clause 8.4 of this Chapter shall apply instead of clause 5 of Chapter 16 of AIS-137(Part 3).

2.1.2.2.3 The driver warning system referred to in clauses 4, 7 and 8 of this Chapter shall be understood as the driver warning system in clause 3 of Chapter 16 of AIS-137 (Part 3).

- 2.1.2.2.4 Clause 6 of Chapter 16 of AIS-137 (Part 3) shall not apply.
- 2.1.2.2.5 The provision set out in clause 5.2 of this Chapter shall apply in the case of vehicles for use by the rescue services or to vehicles designed and constructed for use by the armed services, civil defence, fire services and forces responsible for maintaining public order.

2.2 REQUIRED INFORMATION

- 2.2.1. Information that fully describes the functional operational characteristics of an engine system covered by this Chapter shall be provided by the manufacturer in the format in Chapter 2 of this Part.
- 2.2.2. In its application for type-approval, the manufacturer shall specify the characteristics of all reagents consumed by any emission control system. This specification shall include types and concentrations, operational temperature conditions, and references to international standards.
- 2.2.3. Detailed written information fully describing the functional operation characteristics of the driver warning system as provided in accordance with clause 4 of this Chapter and of the driver inducement system as provided in accordance with clause 5 of this Chapter shall be submitted to the Test Agency at the time of application for the type-approval.
- 2.2.4. When a manufacturer applies for an approval of an engine or engine family as a separate technical unit, it shall include in the technical specifications (as submitted as per Chapter 2 of this Part). the appropriate requirements that will ensure that the vehicle, when used on the road or elsewhere as appropriate, will comply with the requirements of this Chapter. This documentation shall include the following:
 - (a) The detailed technical requirements including the provisions ensuring the compatibility with the monitoring, warning, and inducement systems present in the engine system for the purpose of complying with the requirements of this Chapter;
 - (b) The verification procedure to be complied with for installation of the engine in the vehicle.

The existence and the adequacy of such installation requirements may be checked during the approval process of the engine system.

The documentation referred to in points (a) and (b) shall not be required if the manufacturer applies for an type approval of a vehicle with regard to emissions.

2.3 OPERATING CONDITIONS

- 2.3.1. Any engine system falling within the scope of this Chapter shall retain its emission control function during all conditions regularly pertaining within the Indian Territory.

2.3.2 The emission control monitoring system shall be operational:

- (a) At ambient temperatures between 273 K and 315 K (0°C and 42°C)
- (b) At all altitudes below 1600 m;
- (c) At engine coolant temperatures above 343 K (70°C).

This clause shall not apply in the case of monitoring for reagent level in the storage tank, where monitoring shall be conducted under all conditions where measurement is technically feasible including all conditions when a liquid reagent is not frozen

2.4 Reagent Freeze protection

2.4.1 The manufacturer may use a heated or a non-heated reagent tank and dosing system, in accordance with the general requirements of clause 2.3.1. of this Chapter A manufacturer shall ensure system meets of clause 2.4.2. of this Chapter. A non-heated system shall meet the requirements of clause 2.4.3. of this Chapter.

2.4.1.1 The use of a non-heated reagent tank and dosing system shall be indicated in written instructions to the owner of the vehicle.

2.4.2. Heated reagent tank and dosing system

2.4.2.1 If the reagent has frozen, the manufacturer shall ensure that reagent is available for use within a maximum of 70 minutes after the start of the vehicle at 266 K (- 7 °C) ambient temperature.

2.4.2.2. Demonstration: Demonstration test at the time of type approval is not mandatory.

2.4.2.2.1. The reagent tank and dosing system shall be soaked at 255 K (-18 °C) for 72 hours or until the bulk of the reagent becomes solid.

2.4.2.2.2. After the soak period provided in clause 2.4.2.2.1. of this Chapter the engine shall be started and operated at 266 K (-7°C) ambient temperature as follows: 10 to 20 minutes idling, followed by up to 50 minutes at no more than 40 per cent load.

2.4.2.2.3 The reagent dosing system shall be fully functional at the end of the test procedures described in clauses 2.4.2.2.1. and 2.4.2.2.2 of this Chapter.

2.4.2.2.4. Demonstration of compliance with the requirements of clause 2.4.2.2. may be done in a cold chamber test cell equipped with an engine or vehicle dynamometer or may be based on vehicle field tests, as approved by the Test Agency

2.4.3 Non-Heated Reagent Tank and Dosing System

2.4.3.1 If the reagent has frozen, the manufacturer shall ensure that reagent is available for use within a maximum of 70 minutes after the start of the vehicle at 273 K (0°C) ambient temperature.

- 2.4.3.2 The driver warning system described in clause 4. of this Chapter shall be activated if no reagent dosing occurs at an ambient temperature $\geq 273 \text{ K}$ ($0 \text{ }^{\circ}\text{C}$).
- 2.4.3.3 The severe inducement system as per clause 5.4 of this Chapter shall be activated if no reagent dosing occurs at an ambient temperature $\geq 273 \text{ K}$ ($0 \text{ }^{\circ}\text{C}$) within a maximum of 70 minutes after vehicle start.
- 2.5 Each separate reagent tank installed on a vehicle shall include a means for taking a sample of any fluid inside the tank and for doing so without the need for information not stored on-board the vehicle. The sampling point shall be easily accessible without the use of any specialized tool or device. Keys or systems which are normally carried on the vehicle for locking access to the tank shall not be considered to be specialized tools or devices for the purpose of this clause.

3.0 MAINTENANCE REQUIREMENTS

- 3.1. The manufacturer shall furnish or cause to be furnished to all owners of new vehicles or new engines type-approved in accordance with this Part written instruction about the emission control system and its correct operation.

Those instructions shall state that if the vehicle emission control system is not functioning correctly the driver will be informed of a problem by the driver warning system, and that operation of the driver inducement system as a consequence of ignoring this warning will result in the vehicle being unable to efficiently conduct its mission.
- 3.2. The instructions shall indicate requirements for the proper use and maintenance of vehicles in order to maintain their emissions performance, including, where relevant, the proper use of consumable reagents.
- 3.3. The instructions shall be written in clear and non-technical language and in the official languages.
- 3.4. The instructions shall specify if consumable reagents have to be refilled by the vehicle operator between normal maintenance intervals. The instructions shall also specify the required reagent quality. They shall indicate how the operator should refill the reagent tank. The information shall also indicate a likely rate of reagent consumption for the type of vehicle and how often it is likely to need to be replenished.
- 3.5. The instructions shall specify that use of, and refilling with, a required reagent of the correct specifications is essential in order for the vehicle to comply with the requirements for the issuing of the fitness certificate for that vehicle type.
- 3.6. The instructions shall state that it may be a criminal offence to use a vehicle that does not consume any reagent if the reagent is required for the reduction of emissions.

- 3.7. The instructions shall explain how the warning system and driver inducement systems work. In addition, the consequences, in terms of vehicle performance and fault logging, of ignoring the warning system and not replenishing the reagent or rectifying a problem shall be explained.

4.0 DRIVER WARNING SYSTEM

- 4.1. The vehicle shall include a driver warning system using visual alarms that informs the driver when a low reagent level, incorrect reagent quality, too low a rate of reagent consumption, or a malfunction, has been detected that may be due to tampering and that will lead to operation of the driver inducement system if not rectified in a timely manner. The warning system shall also be active when the driver inducement system described in clause 5 of this Chapter has been activated.

- 4.2. The vehicle On-Board Diagnostics (OBD) display system described in Chapter 8B of this Part shall not be used for the purpose of providing the visual alarms described in clause 4.1. of this Chapter. The warning shall not be the same as the warning used for the purposes of OBD (that is, the MI – malfunction indicator) or other engine maintenance. It shall not be possible to turn off the warning system or visual alarms by means of a scan-tool if the cause of the warning activation has not been rectified. Conditions for activation and deactivation of the warning system and visual alarms are described in Appendix 2 of this Chapter.

- 4.3. The driver warning system may display short messages, including messages indicating clearly the following:

- (a) The remaining distance or time before activation of the low-level or severe inducements,
- (b) The level of torque reduction,
- (c) The conditions under which vehicle disablement can be cleared.

The system used for displaying the messages referred to in this point may be the same as the one used for OBD or other maintenance purposes.

- 4.4. At the choice of the manufacturer, the warning system may include an audible component to alert the driver. The cancelling of audible warnings by the driver is permitted.
- 4.5. The driver warning system shall be activated as specified in clauses 6.2., 7.2., 8.4., and 9.3. of this Chapter.
- 4.6. The driver warning system shall be deactivated when the conditions for its activation have ceased to exist. The driver warning system shall not be automatically deactivated without the reason for its activation having been remedied.
- 4.7. The warning system may be temporarily interrupted by other warning signals providing important safety-related messages.

- 4.8. A facility to permit the driver to dim the visual alarms provided by the warning system may be provided on vehicles for use by the rescue services or on vehicles designed and constructed for use by the armed services, civil defence, fire services and forces responsible for maintaining public order.
- 4.9. Details of the driver warning system activation and deactivation procedures are specified in Appendix 2 of this Chapter.
- 4.10. As part of the application for type-approval under this Part, the manufacturer shall demonstrate the operation of the driver warning system, as specified in Appendix 1 of this Chapter.

5.0 DRIVER INDUCEMENT SYSTEM

- 5.1. The vehicle shall incorporate a two-stage driver inducement system starting with a low-level inducement (a performance restriction) followed by a severe inducement (effective disablement of vehicle operation).
- 5.2. The requirement for a driver inducement system shall not apply to engines or vehicles for use by the rescue services or to engines or vehicles designed and constructed for use by the armed services, civil defence, fire services and forces responsible for maintaining public order. Permanent deactivation of the driver inducement system shall only be done by the engine or vehicle manufacturer.
- 5.3. **Low-level inducement system**

The low-level inducement system shall reduce the maximum available engine torque across the engine speed range by 25 per cent between the peak torque speed and the governor breakpoint as described in Appendix 3 of this Chapter. The maximum available reduced engine torque below the peak torque speed of the engine before imposition of the torque reduction shall not exceed the reduced torque at that speed.

The low level inducement system shall be activated when the vehicle becomes stationary⁽¹⁾ for the first time after the conditions specified in clause 6.3.,7.3,8.5 and 9.4 below have occurred .

(1) Vehicle shall be considered as stationary at latest 1 minute after the vehicle speed has been reduced to 0 km/hr. The engagement of any device such as park brake ,trailer brake or hand brake shall not be necessary for being stationary .

5.4. Severe inducement system

The vehicle or engine manufacturer shall incorporate at least one of the severe inducement systems described in clauses 5.4.1. to 5.4.3 and the “disable on time limit” system described in clause 5.4.4.

- 5.4.1. A “**disable after restart**” system shall limit the vehicle speed to 20 km/h ("creep mode") after the engine has been shut down at the request of the driver (“key-off”).

- 5.4.2. A “**disable after fueling**” system shall limit the vehicle speed to 20 km/h ("creep mode") after the fuel tank level has risen a measurable amount, which shall not be more than 10 per cent of the fuel tank capacity and shall be approved by the Test Agency based on the technical capabilities of the fuel level meter and a declaration by the manufacturer.
- 5.4.3. A “**disable after parking**” system shall limit the vehicle speed to 20 km/h ("creep mode") after the vehicle has been stationary for more than one hour.
- 5.4.4. A “**disable on time limit**” system shall limit the vehicle speed to 20 km/h (“creep mode”) on the first occasion when the vehicle becomes stationary⁽¹⁾ after eight hours of engine operation if none of the systems described in clauses 5.4.1. to 5.4.3. above has been previously been activated.

(1) Vehicle shall be considered as stationary at latest 1 minute after the vehicle speed has been reduced to 0 km/hr. The engagement of any device such as park brake, trailer brake or hand brake shall not be necessary for being stationary.

- 5.5. The driver inducement system shall be enabled as specified in clauses 6.3., 7.3., 8.5., and 9.4. of this Chapter.
- 5.5.1 When the driver inducement system has determined that the severe inducement system shall be activated, the low-level inducement system shall remain activated until the vehicle speed has been limited to 20 km/h ("creep mode").
- 5.6. The driver inducement system shall be deactivated when the conditions for its activation have ceased to exist. The driver inducement system shall not be automatically deactivated without the reason for its activation having been remedied.
- 5.7. Details of the driver inducement system activation and deactivation procedures are described in Appendix 2 of this Chapter.
- 5.8. As part of the application for type-approval under this Part, the manufacturer shall demonstrate the operation of the driver inducement system, as specified in Appendix 1 of this Chapter.

6.0 REAGENT AVAILABILITY

6.1. Reagent Indicator

The vehicle shall include a specific indicator on the dashboard that clearly informs the driver of the level of reagent in the reagent storage tank. The minimum acceptable performance level for the reagent indicator is that it shall continuously indicate the reagent level whilst the driver warning system referred to in clause 4 of this Chapter is activated to indicate problems with reagent availability. The reagent indicator may be in the form of an analogue or digital display, and may show the level as a proportion of the full tank capacity, the amount of remaining reagent, or the estimated driving distance remaining.

The reagent indicator shall be placed in close proximity to the fuel level indicator.

6.2. Activation of the driver warning system

6.2.1. The driver warning system specified in clause 4 of this Chapter shall be activated when the level of reagent is less than 10 per cent of the capacity of the reagent tank or a higher percentage at the choice of the manufacturer.

6.2.2. The warning provided shall be sufficiently clear for the driver to understand that the reagent level is low. When the warning system includes a message display system, the visual warning shall display a message indicating a low level of reagent. (for example, “urea level low”, “AdBlue level low”, or “reagent low”).

6.2.3. The driver warning system does not initially need to be continuously activated, however activation shall escalate in intensity so that it becomes continuous when the level of the reagent is approaching a very low proportion of the capacity of the reagent tank and the point where the driver inducement system will come into effect is approached. It shall culminate in a driver notification at a level that is at the choice of the manufacturer, but is sufficiently more noticeable than the point where the driver inducement system in clause 6.3. of this Chapter comes into effect.

6.2.4. The continuous warning shall not be easily disabled or ignored. When the warning system includes a message display system, an explicit message shall be displayed (for example. “fill up urea”, “fill up AdBlue”, or “fill up reagent”). The continuous warning may be temporarily interrupted by other warning signals providing important safety related messages.

6.2.5. It shall not be possible to turn off the driver warning system until the reagent has been replenished to a level not requiring its activation.

6.3. Activation of the driver inducement system

6.3.1 The low-level inducement system described in clause 5.3. of this Chapter shall be enabled, and subsequently activated according to the requirements of that clause, if the reagent tank level goes below 2.5 % of its nominally full capacity or a higher percentage at the choice of the manufacturer.

6.3.2. The severe inducement system described in clause 5.4. of this Chapter shall be enabled, and subsequently activated according to the requirements of that clause, if the reagent tank is empty (that is, the dosing system is unable to draw further reagent from the tank) or at any level below 2.5 % of its nominally full capacity at the discretion of the manufacturer.

- 6.3.3. It shall not be possible to turn off the low-level or severe driver inducement system until the reagent has been replenished to a level not requiring their respective activation.

7.0 REAGENT QUALITY MONITORING

- 7.1. The vehicle shall include a means of determining the presence of an incorrect reagent on board a vehicle.

- 7.1.1. The manufacturer shall specify a minimum acceptable reagent concentration CD_{min} , which results in tailpipe emissions not exceeding the limit values specified in clause 5.3 of Chapter 1 of this Part.

- 7.1.1.1. During the OBD-1 period specified in clause 4.10.7 of Chapter 1 of this Part and upon request of the manufacturer for the purpose of clause 7.1.1 of this Chapter the reference to the NOx emission limit specified in Table 3 in clause 5.3 of Chapter 1 of this Part shall be replaced by the value of 900 mg/kWh.

- 7.1.1.2. The value of CD_{min} shall be demonstrated during type approval by the procedure defined in Appendix 6 of this Chapter and recorded in the extended documentation package as specified in clause 5.1.4. of Chapter 1 of this Part.

- 7.1.2 Any reagent concentration lower than CD_{min} shall be detected and be regarded, for the purpose of clause 7.1. of this Chapter, as being incorrect reagent.

- 7.1.3. A specific counter ("the reagent quality counter") shall be attributed to the reagent quality. The reagent quality counter shall count the number of engine operating hours with an incorrect reagent.

- 7.1.4. Details of the reagent quality counter activation and deactivation criteria and mechanisms are described in Appendix 2 of this Chapter.

- 7.1.5. The reagent quality counter information shall be made available in a standardized manner in accordance with the provisions of Appendix 5 of this Chapter.

7.2. Activation of the driver warning system

When the monitoring systems detects or, as appropriate, confirms that the reagent quality is incorrect, the driver warning system described in clause 4 of this Chapter shall be activated. When the warning system includes a message display system, it shall display a message indicating the reason for the warning (for example. "in correct urea detected", "incorrect AdBlue detected", or "incorrect reagent detected").

7.3 Activation of the driver inducement system

- 7.3.1. The low-level inducement system described in clause 5.3. of this Chapter shall be enabled, and subsequently activated according to the requirements of that clause, if the reagent quality is not rectified within 10 engine operating hours after the activation of the driver warning system described in clause 7.2.of this Chapter.

7.3.2. The severe inducement system described in clause 5.4. of this chapter Shall be enabled, and subsequently activated according to the requirements of that clause, if the reagent quality is not rectified within 20 engine operating hours after the activation of the driver warning system described in clause 7.2. of this Chapter.

7.3.3. The number of hours prior to activation of the inducement systems shall be reduced in case of a repetitive occurrence of the malfunction, in accordance with the mechanism described in Appendix 2 of this Chapter.

8.0 REAGENT CONSUMPTION AND DOSING ACTIVITY MONITORING

8.1 The vehicle shall include a means of determining reagent consumption and providing off-board access to consumption information.

8.2. Reagent consumption and dosing activity counters

8.2.1. A specific counter shall be attributed to the reagent consumption (the "reagent consumption counter") and another to the dosing activity (the "dosing activity counter"). These counters shall count the number of engine operating hours which occur with an incorrect reagent consumption and, respectively, an interruption of the reagent dosing activity.

8.2.2. Details of the reagent consumption counter and dosing counter activation and deactivation criteria and mechanisms are described in Appendix 2 of this Chapter.

8.2.3. The reagent consumption counter and the dosing counter information shall be made available in a standardised manner according to the provisions of Appendix 5 of this Chapter.

8.3. Monitoring conditions

8.3.1 The maximum detection period for insufficient reagent consumption is 5 hours or the period equivalent to a demanded reagent consumption of at least 2 liters, whichever is longer., whichever is longer.

8.3.1.1 When the reagent consumption is monitored by using at least one of the following parameters:

- (a) The level of reagent in the on-vehicle storage tank;
- (b) The flow of reagent or quantity of reagent injected at a position as close as technically possible to the point of injection into an exhaust after treatment system.

The maximum detection period for insufficient reagent consumption is extended to 48h or to the period equivalent to a demanded reagent consumption of at least 15 liters, whichever is longer.

8.4. Activation of the driver warning system

8.4.1. The driver warning system described in clause 4 of this Chapter shall be activated if a deviation of more than fifty percent between the average reagent consumption and the average demanded reagent consumption by the engine system over a period to be defined by the manufacturer, which shall not be longer than the maximum period defined in clause 8.3.1, or when applicable, clause 8.3.1.1. of this Chapter, is detected. When the warning system includes a message display system, it shall display a message indicating the reason for the warning (for example, “urea dosing malfunction”, “AdBlue dosing malfunction”, or “reagent dosing malfunction”).

8.4.2. The driver warning system described in clause 4 of this Chapter shall be activated in the case of interruption in reagent dosing. When the warning system includes a message display system, it shall display a message indicating an appropriate warning. This activation shall not be required where the interruption is demanded by the engine ECU because the vehicle operating conditions are such that the vehicle’s emission performance does not require reagent dosing.

8.5. Activation of the driver inducement system

8.5.1. The low-level inducement system described in clause 5.3. of this Chapter shall be enabled, and subsequently activated according to the requirements of that clause, if an error in the reagent consumption or an interruption in reagent dosing is not rectified within 10 engine operating hours after the activation of the driver warning system specified in clauses 8.4.1. and 8.4.2. of this Chapter.

8.5.2. The severe inducement system described in clause 5.4. of this Chapter shall be enabled, and subsequently activated according to the requirements of that clause, if an error in the reagent consumption or an interruption in reagent dosing is not rectified within 20 engine operating hours after the activation of the driver warning system in clauses 8.4.1. and 8.4.2. of this Chapter.

8.5.3. The number of hours prior to activation of the inducement systems shall be reduced in case of a repetitive occurrence of the malfunction in accordance with the mechanism described in Appendix 2 to this Chapter.

9.0 MONITORING FAILURES THAT MAY BE ATTRIBUTED TO TAMPERING

9.1. In addition to the level of reagent in the reagent tank, the reagent quality, and the reagent consumption, the following failures shall be monitored by the anti-tampering system because they may be attributed to tampering:

- (a) Impeding of the EGR valve operation;
- (b) Failures of the anti-tampering monitoring system, as described in clause 9.2.1. of this Chapter.

9.2. Monitoring Requirements

- 9.2.1. The anti-tampering monitoring system shall be monitored for electrical failures and for removal or deactivation of any sensor that prevents it from diagnosing any other failures mentioned in clauses 6 to 8 (component monitoring) of this Chapter.

A non-exhaustive list of sensors that affect the diagnostic capability are those directly measuring NO_x concentration, urea quality sensors, ambient sensors, and sensors used for monitoring reagent dosing activity, reagent level, or reagent consumption.

9.2.2. EGR Valve Counter

- 9.2.2.1. A specific counter shall be attributed to an impeded EGR valve. The EGR valve counter shall count the number of engine operating hours when any DTC associated with an impeded EGR valve is confirmed to be active.

- 9.2.2.2. Details of the EGR valve counter activation and deactivation criteria and mechanisms are described in Appendix 2 of this Chapter.

- 9.2.2.3. The EGR valve counter information shall be made available in a standardized manner in accordance with the provisions of Appendix 5 of this Chapter.

9.2.3. Monitoring System Counters

- 9.2.3.1. A specific counter shall be attributed to each of the monitoring failures considered in point (b) of clause 9.1. of this Chapter. The monitoring system counters shall count the number of engine operating hours when the DTC associated with a malfunction of the monitoring system is confirmed to be active. Grouping of several faults into a single counter is permitted.

- 9.2.3.2. Details of the criteria for activation and deactivation of the monitoring system counters and the associated mechanisms are described in Appendix 2 of this Chapter.

- 9.2.3.3. The monitoring system counter information shall be made available in a standardized manner in accordance with the provisions of Appendix 5 of this Chapter.

9.3 Activation of the driver warning system

The driver warning system described in clause 4 of this Chapter shall be activated in the case where any of the failures specified in clause 9.1. of this Chapter occurs, and shall indicate that an urgent repair is required. When the warning system includes a message display system, it shall display a message indicating either the reason for the warning (for example, "reagent dosing valve disconnected", or "critical emission failure").

- 9.4. **Activation of the driver inducement system**
- 9.4.1. The low-level inducement system described in clause 5.3. of this Chapter shall be enabled, and subsequently activated according to the requirements of that clause, if a failure specified in clause 9.1. of this Chapter is not rectified within 36 engine operating hours after the activation of the driver warning system in clause 9.3. of this Chapter.
- 9.4.2. The severe inducement system described in clause 5.4. of this Chapter shall be enabled, and subsequently activated according to the requirements of that clause, if a failure specified in clause 9.1. of this Chapter is not rectified within 100 engine operating hours after the activation of the driver warning system in clause 9.3. of this Chapter.
- 9.4.3. The number of hours prior to activation of the inducement systems shall be reduced in case of a repetitive occurrence of the malfunction in accordance with the mechanism described in Appendix 2 of this Chapter.

CHAPTER 10 - APPENDIX 1
DEMONSTRATION REQUIREMENTS

A.1.1. GENERAL

A.1.1.1 The manufacturer shall submit to the Test Agency a complete documentation package justifying the compliance of the SCR system with the requirements of this Chapter as regards its capabilities for monitoring and activation of the driver warning and inducement system, which may include:

- (a) Algorithms and decision charts
- (b) Tests and/or simulation results
- (c) Reference to previously approved monitoring systems, etc.

A.1.1.2 Compliance with the requirements of this Chapter shall be demonstrated during type-approval by performing, as illustrated in Table 1 and specified in this Appendix, the following demonstrations:

- (a) a demonstration of the warning system activation.
- (b) a demonstration of the low level inducement system activation.
- (c) a demonstration of the severe inducement system activation.

Table 1

Illustration of the Content of the Demonstration Process in accordance with the Provisions in clauses A.1.3, A.1.4 And A.1.5

Mechanism	Demonstration elements
Warning system activation specified in clause A.1.3.	(a) 4 activation tests (incl. lack of reagent) (b) Supplementary demonstration elements, as appropriate
Low-level inducement activation specified in clause A.1.4	(a) 2 activation tests (incl. lack of reagent) (b) Supplementary demonstration elements. (c) 1 torque reduction test.
Severe inducement activation specified in clause A.1.5	(a) 2 activation tests (incl. lack of reagent) (b) Supplementary demonstration elements, as appropriate (c) Demonstration elements of correct vehicle behavior during inducement.

A.1.2. ENGINE FAMILIES OR OBD ENGINE FAMILIES

The compliance of an engine family or an OBD engine family with the requirements of this Chapter may be demonstrated by testing one of the members of the family under consideration, provided that the manufacturer demonstrates to the Test Agency that the monitoring systems necessary for complying with the requirements of this Chapter are similar within the family.

- A.1.2.1. This demonstration may be performed by presenting to the Test Agencies such elements as algorithms, functional analyses, etc.
- A.1.2.2. The test engine is selected by the manufacturer in agreement with the Test Agency. It may or may not be the parent engine of the considered family.
- A.1.2.3. In the case where engines of an engine family belong to an OBD engine family that has already been type-approved according to clause A.1.2.1 of this Appendix (Figure 1 below), the compliance of that engine family is deemed to be demonstrated without further testing, provided the manufacturer demonstrates to the Test Agency that the monitoring systems necessary for complying with the requirements of this Chapter are similar within the engine and OBD engine families under consideration.

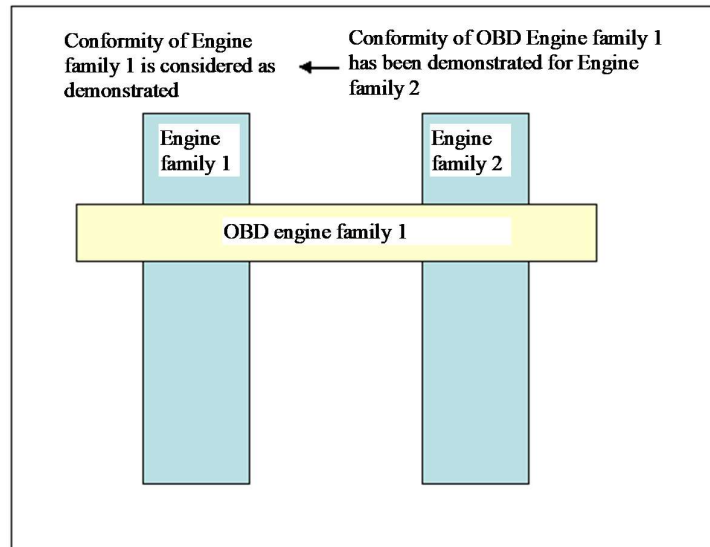


Figure 1
Previously Demonstrated Conformity of
an OBD Engine Family

A.1.3. DEMONSTRATION OF THE WARNING SYSTEM ACTIVATION

A.1.3.1. The compliance of the warning system activation shall be demonstrated by performing one test for each of the failure categories considered in clauses 6 to 9 of this Chapter such as: lack of reagent, low reagent quality, low reagent consumption, failure of components of the monitoring system.

A.1.3.2. Selection of The Failures to be Tested

A.1.3.2.1. For the purpose of demonstrating the activation of the warning system in case of a wrong reagent quality, a reagent shall be selected with a concentration of the active ingredient equal to or higher than the minimum acceptable reagent concentration CD_{min} , communicated by the manufacturer in accordance with the requirements of clause 7.1.1 of this Chapter

A.1.3.2.2. For the purpose of demonstrating the activation of the warning system in the case of an incorrect rate of reagent consumption, it shall be sufficient to arrange an interruption of the dosing activity.

A.1.3.2.2.1. Where activation of the warning system has been demonstrated by interruption of the dosing activity, the manufacturer shall, in addition, present the Test Agency with evidence such as algorithms, functional analyses, the results of previous tests, etc. to show that the warning system will activate correctly in the case of an incorrect rate of reagent consumption due to other causes.

A.1.3.2.3. For the purpose of demonstrating the activation of the warning system in case of failures that may be attributed to tampering, as defined in clause 9 of this Chapter, the selection shall be performed in accordance with the following requirements:

A.1.3.2.3.1. The manufacturer shall provide the Test Agency with a list of such potential failures.

A.1.3.2.3.2. The failure to be considered in the test shall be selected by the Test Agency from this list referred to in clause A.1.3.2.3.1.

A.1.3.3. Demonstration

A.1.3.3.1. For the purposes of this demonstration of the activation of the warning system a separate test shall be performed for each of the failures considered in clause A.1.3.1. of this Appendix.

A.1.3.3.2. During a test, no failure shall be present other than the one addressed by the test.

A.1.3.3.3. Prior to starting a test, all DTC shall have been erased.

A.1.3.3.4. At the request of the manufacturer, and with the agreement of the Test Agency, the failures subject to testing may be simulated.

- A.1.3.3.5. For failures other than lack of reagent, once the failure has been induced or simulated, the detection of that failure shall be performed in accordance with clause 7.1.2.2. of Chapter 8B of this Part.
- A.1.3.3.5.1. The detection sequence shall be stopped once the DTC of the selected failure has got the “confirmed and active” status.
- A.1.3.3.6. For the purpose of demonstrating the activation of the warning system in case of lack of reagent availability, the engine system shall be operated over one or more operating sequences at the discretion of the manufacturer.
- A.1.3.3.6.1. The demonstration shall start with a level of reagent in the tank to be agreed between the manufacturer and the Test Agency but representing not less than 10 per cent of the nominal capacity of the tank.
- A.1.3.3.6.2. The warning system is deemed to have performed in the correct manner if the following conditions are met simultaneously:
 - (a) The warning system has been activated with a reagent availability greater or equal to 10 per cent of the capacity of the reagent tank;
 - (b) The "continuous" warning system has been activated with a reagent availability greater or equal to the value declared by the manufacturer according to the provisions of clause 6 of this Chapter.
- A.1.3.4. The demonstration of the warning system activation is deemed to be accomplished for reagent level events if, at the end of each demonstration test performed according to clause A.1.3.2.1. of this Appendix, the warning system has been properly activated.
- A.1.3.5. The demonstration of the warning system activation is deemed to be accomplished for DTC triggered events if, at the end of each demonstration test performed according to clause A.1.3.2.1 of this Appendix, the warning system has been properly activated and the DTC for the selected failure has got the status shown in Table 1 in Appendix 2 of this Chapter.
- A.1.4. DEMONSTRATION OF THE INDUCEMENT SYSTEM**
- A.1.4.1. The demonstration of the inducement system shall be done by tests performed on an engine test bench.
- A.1.4.1.1. Any additional vehicle components or sub-systems, such as ambient temperature sensors, level sensors, and driver warning and information systems, that are required in order to perform the demonstrations shall be connected to the engine system for that purpose, or shall be simulated, to the satisfaction of the Test Agency.

- A.1.4.1.2. If the manufacturer chooses, and subject to the agreement of the Test Agency, the demonstration tests may be performed on a complete vehicle either by mounting the vehicle on a suitable test bed or by running it on a test track under controlled conditions.
- A.1.4.2. The test sequence shall demonstrate the activation of the inducement system in case of lack of reagent and in case of one of the failures defined in clauses 7, 8, or 9 of this Chapter.
- A.1.4.3. **For the purpose of this demonstration,**
 - (a) the Test Agency shall select, in addition to the lack of reagent, one of the failures defined in clauses 7, 8 or 9 of this Chapter that has been previously used in the demonstration of the warning system,
 - (b) the manufacturer shall be permitted to simulate, in agreement with the Test Agency, the achievement of a certain number of operating hours.
 - (c) The achievement of the torque reduction required for low-inducement may be demonstrated at the same time as the general engine performance approval process performed in accordance with this Part. Separate torque measurement during the inducement system demonstration is not required in this case. The speed limitation required for severe inducement shall be demonstrated in accordance with the requirements of clause 5 of this Chapter.
- A.1.4.4. The manufacturer shall, in addition, demonstrate the operation of the inducement system under those failure conditions defined in clauses 7, 8 or 9 of this Chapter which have not been chosen for use in demonstration tests described in clauses A.1.4.1., A.1.4.2. and A.1.4.3. of this Appendix. These additional demonstrations may be performed by presentation to the Test Agency of a technical case using evidence such as algorithms, functional analyses, and the results of previous tests.
 - A.1.4.4.1. These additional demonstrations shall, in particular, demonstrate to the satisfaction of the Test Agency the inclusion of the correct torque reduction mechanism in the engine ECU.
- A.1.4.5. **Demonstration test of the low level inducement system**
 - A.1.4.5.1. This demonstration starts when the warning system, or when appropriate "continuous" warning system, has been activated as a result of the detection of a failure selected by the Test Agency.
 - A.1.4.5.2. When the system is being checked for its reaction to the case of lack of reagent in the tank, the engine system shall be run until the reagent availability has reached a value of 2.5 per cent of the nominal full capacity of the tank or the value declared by the manufacturer in accordance with clause 6.3.1 of this Chapter at which the low-level inducement system is intended to operate.

- A.1.4.5.2.1. The manufacturer may, with the agreement of the Test Agency, simulate continuous running by extracting reagent from the tank, either whilst the engine is running or whilst it is stopped.
- A.1.4.5.3. When the system is checked for its reaction in the case of a failure other than a lack of reagent in the tank, the engine system shall be run for the relevant number of operating hours indicated in Table 2 of Appendix 2 of this Chapter or, at the choice of the manufacturer, until the relevant counter has reached the value at which the low-level inducement system is activated.
- A.1.4.5.4. The demonstration of the low level inducement system shall be deemed to be accomplished if, at the end of each demonstration test performed in accordance with clauses A.1.4.5.2. and A.1.4.5.3. of this Appendix, the manufacturer has demonstrated to the Test Agency that the engine ECU has activated the torque reduction mechanism.
- A.1.4.6. **Demonstration test of the severe inducement system**
 - A.1.4.6.1. This demonstration shall start from a condition where the low-level inducement system has been previously activated, and may be performed as a continuation of the tests undertaken to demonstrate the low-level inducement system.
 - A.1.4.6.2. When the system is checked for its reaction in the case of lack of reagent in the tank, the engine system shall be run until the reagent tank is empty (that is, until the dosing system cannot draw further reagent from the tank), or has reached the level below 2.5 per cent of nominal full capacity of the tank at which the manufacturer has declared that the severe inducement system will be activated.
 - A.1.4.6.2.1. The manufacturer may, with the agreement of the Test Agency, simulate continuous running by extracting reagent from the tank, either whilst the engine is running or whilst it is stopped.
 - A.1.4.6.3. When the system is checked for its reaction in the case of a failure that is not a lack of reagent in the tank, the engine system shall then be run for the relevant number of operating hours indicated in Table 2 of Appendix 2 of this Chapter or, at the choice of the manufacturer, until the relevant counter has reached the value at which the severe inducement system is activated.
 - A.1.4.6.4. The demonstration of the severe inducement system shall be deemed to be accomplished if, at the end of each demonstration test performed in accordance with A.1.4.6.2 and A.1.4.6.3 the manufacturer has demonstrated to the Test Agency that the required vehicle speed limitation mechanism has been activated.

A.1.5. DEMONSTRATION OF THE VEHICLE SPEED LIMITATION FOLLOWING ACTIVATION OF THE SEVERE INDUCEMENT SYSTEM

- A.1.5.1. The demonstration of the vehicle speed limitation following activation of the severe inducement system shall be performed by the presentation to the Test Agency of a technical case using evidence such as algorithms, functional analyses, and the result of previous tests.
 - A.1.5.1.1. Alternatively, if the manufacturer chooses, and subject to the agreement of the Test Agency, the demonstration of vehicle speed limitation may be performed on a complete vehicle in accordance with the requirements of clause A.1.5.4 of this Appendix, either by mounting the vehicle on a suitable test bed or by running it on a test track under controlled conditions.
- A.1.5.2. When the manufacturer applies for an approval of an engine or engine family as a separate technical unit, the manufacturer shall provide the Test Agency with evidence that the installation documentation package complies with the provisions of clause 2.2.4. of this Chapter concerning the measures to ensure that the vehicle, when used on the road or elsewhere as appropriate, will comply with the requirements of this Chapter regarding severe inducement.
- A.1.5.3. If the Test Agency is not satisfied with the evidence of proper operation of the severe inducement system that is provided by the manufacturer, the Test Agency may request a demonstration on a single representative vehicle in order to confirm proper operation of the system. The vehicle demonstration shall be performed in accordance with the requirements of clause A.1.5.4. of this Appendix.
- A.1.5.4. **Additional demonstration for confirming the effect of activation of the severe inducement system on a vehicle**
 - A.1.5.4.1. This demonstration shall be performed at the request of the Test Agency when it is not satisfied with the evidence of proper operation of the severe inducement system provided by the manufacturer. This demonstration shall be performed at the earliest opportunity in agreement with the Test Agency.
 - A.1.5.4.2. One of the failures defined in clauses 6 to 9 of this Chapter shall be selected by the manufacturer, and shall be introduced or simulated on the engine system, as the manufacturer and the Test Agency agree.
 - A.1.5.4.3. The inducement system shall be brought by the manufacturer to a state where the low-level inducement system has been activated and the severe inducement system has not yet been activated.

- A.1.5.4.4. The vehicle shall be operated until the counter associated with the selected failure has reached the relevant number of operating hours indicated in Table 2 of Appendix 2 or, as appropriate, until either the reagent tank is empty or, has reached the level below 2.5 per cent of nominal full capacity of the tank at which the manufacturer has chosen to activate the severe inducement system.
- A.1.5.4.5. If the manufacturer has opted for the “disable after restart” approach referred to in clause 5.4.1. of this Chapter, the vehicle shall be operated until the end of the current operating sequence, which must include a demonstration that the vehicle is capable of exceeding 20 km/h. After restart, the vehicle speed shall be limited to no more than 20 km/h.
- A.1.5.4.6. If the manufacturer has opted for the “disable after fuelling” approach referred to in clause 5.4.2. of this Chapter, the vehicle shall be operated for a short distance, chosen by the manufacturer, after it has been brought to a state where there is sufficient spare capacity in the tank to permit it to be refuelled with the amount of fuel defined in clause 5.4.2. of this Chapter. The vehicle operation before refueling shall include a demonstration that the vehicle is capable of exceeding 20 km/h. After re-fuelling the vehicle with the amount of fuel defined in clause 5.4.2. of this Chapter the vehicle speed shall be limited to no more than 20 km/h.
- A.1.5.4.7. If the manufacturer has opted for the “disable after parking” approach referred to in clause 5.4.3. of this Chapter, the vehicle shall be stopped after having been run for a short distance, chosen by the manufacturer, which is sufficient to demonstrate that the vehicle is capable of exceeding a speed of 20 km/h. After the vehicle has been stationary for more than one hour, the vehicle speed shall be limited to no more than 20 km/h.

CHAPTER 10 - APPENDIX 2

DESCRIPTION OF THE DRIVER WARNING AND INDUCEMENT ACTIVATION AND DEACTIVATION MECHANISMS

- A.2.1. To complement the requirements specified in this Chapter concerning the driver warning and inducement activation and deactivation mechanisms, this Appendix specifies the technical requirements for an implementation of those activation and deactivation mechanisms consistent with the OBD provisions of Chapter 8B of this Part.

All definitions used in Chapter 8B of this Part are applicable to this Appendix.

- A.2.2. Activation and deactivation mechanisms of the driver warning system

- A.2.2.1. The driver warning system shall be activated when the diagnostic trouble code (DTC) associated with a malfunction justifying its activation has the status defined in Table 1 below.

Table 1
Activation of the Driver Warning System

Failure type	DTC status for activation of the warning system
poor reagent quality	confirmed and active
Low reagent consumption	potential (if detected after 10 hours), potential or confirmed and active otherwise
absence of dosing	confirmed and active
impeded EGR valve	confirmed and active
malfunction of the monitoring system	confirmed and active

- A.2.2.1.1. If the counter associated with the relevant failure is not at zero, and is consequently indicating that the monitor has detected a situation where the malfunction may have occurred for a second or subsequent time, the driver warning system shall be activated when the DTC has the status "potential".
- A.2.2.2. The driver warning system shall be deactivated when the diagnostic system concludes that the malfunction relevant to that warning is no longer present or when the information, including DTCs relative to the failures, justifying its activation is erased by a scan tool.

A.2.2.2.1 Erasing of failure information by means of a scan tool

A.2.2.2.1.1. Erasing of information, including DTCs relative to failures justifying the activation of a driver warning signal and of their associated data, by means of a scan tool shall be performed in accordance with Chapter 8B of this Part.

A.2.2.2.1.2. The erasing of failure information shall only be possible under “engine-off” conditions.

A.2.2.2.1.3. When failure information, including DTCs, is erased, any counter associated with these failures and which is specified in this Chapter as one that must not be erased shall not be erased.

A.2.3. ACTIVATION AND DEACTIVATION MECHANISM OF THE DRIVER INDUCEMENT SYSTEM

A.2.3.1. The driver inducement system shall be activated when the warning system is active and the counter relevant to the type of malfunction justifying its activation has reached the value specified in Table 2 of this Appendix.

A.2.3.2. The driver inducement system shall be deactivated when the system no longer detects a malfunction justifying its activation, or if the information, including the DTCs, relative to the failures justifying its activation has been erased by a scan tool or maintenance tool.

A.2.3.3. The driver warning and inducement systems shall be immediately activated or deactivated as appropriate in accordance with the provisions of clause 6 of this Chapter after assessment of the reagent quantity in the reagent tank. In that case, the activation or deactivation mechanisms shall not depend upon the status of any associated DTC.

A.2.4. COUNTER MECHANISM

A.2.4.1. General

A.2.4.1.1. To comply with the requirements of this Chapter, the system shall separate counters to record the number of hours during which the engine has been operated while the system has detected any of the following:

- (a) An incorrect reagent quality;
- (b) An incorrect reagent consumption;
- (c) An interruption of reagent dosing activity;
- (d) An impeded EGR valve,
- (e) A failure of the monitoring system as defined in point (b) of clause 9.1 of this Chapter.

- A.2.4.1.2. Each of these counters shall count up to the maximum value provided in a 2byte counter with 1-hour resolution, and shall hold that value unless the conditions allowing the counter to be reset to zero are met.
- A.2.4.1.3. A manufacturer may use a single or multiple monitoring system counters.

A single counter may accumulate the number of hours of 2 or more different malfunctions relevant to that type of counter.
- A.2.4.1.3.1. When the manufacturer decides to use multiple monitoring system counters, the system shall be capable of assigning a specific monitoring system counter to each malfunction that is relevant, in accordance with this Chapter, to that type of counter.
- A.2.4.2. **Principle of Counter Mechanisms**
- A.2.4.2.1. **Each of the counters shall operate as follows:**
 - A.2.4.2.1.1. If starting from zero, the counter shall begin counting as soon as a malfunction relevant to that counter is detected and the corresponding diagnostic trouble code (DTC) has the status described in Table 1.
 - A.2.4.2.1.2. The counter shall halt and hold its current value if a single monitoring event occurs and the malfunction that originally activated the counter is no longer detected or if the failure has been erased by a scan tool or a maintenance tool.
 - A.2.4.2.1.2.1. If the counter stops counting when the severe inducement system is active, the counter shall be kept frozen at the value defined in Table 2
 - A.2.4.2.1.2.2. In the case of a single monitoring system counter, that counter shall continue counting if a malfunction relevant to that counter has been detected and its corresponding Diagnostic trouble code (DTC) has the status "confirmed and active". It shall halt and hold the value specified in clause A.2.4.2.1.2, or A.2.4.2.1.2.1 of this Appendix as appropriate, if no malfunction that would justify the counter activation is detected or if all the failures relevant to that counter have been erased by a scan tool or a maintenance tool.

Table 2

Counters and Inducement

	DTC status for first activation of the counter	Counter value for low level inducement	Counter value for severe induce ment	Frozen value held by the counter during the period just after serve inducement
Reagent quality counter	Confirmed and active	10 hours	20 hours	18 hours
Reagent consumption counter	Potential or confirmed and active (see Table 1)	10 hours	20 hours	18 hours
Dosing counter	Confirmed and active	10 hours	20 hours	18 hours
EGR valve counter	Confirmed and active	36 hours	100 hours	95 hours
Monitoring system counter	Confirmed and active	36 hours	100 hours	95 hours

- A.2.4.2.1.3. Once frozen, the counter shall be reset to zero when the monitors relevant to that counter have run at least once to completion of their monitoring cycle without having detected a malfunction and no malfunction relevant to that counter has been detected during 36 engine operating hours since the counter was last held (see Figure 1 below).
- A.2.4.2.1.4. The counter shall continue counting from the point at which it had been held if a malfunction relevant to that counter is detected during a period when the counter is frozen (see Figure 1 below).

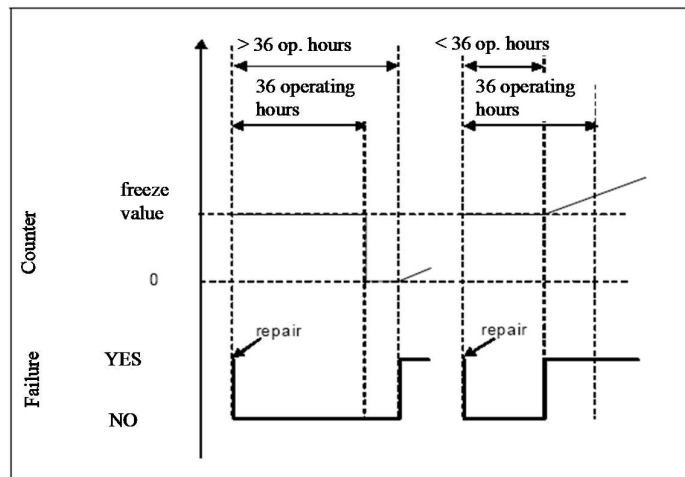


Figure 1

**Reactivation and Resetting to Zero of a Counter
after a Period when its Value has been Frozen**

A.2.5. ILLUSTRATION OF THE ACTIVATION AND DEACTIVATION AND COUNTER MECHANISMS.

A.2.5.1. This clause illustrates the activation and deactivation and counter mechanisms for some typical cases. The figures and descriptions given in clauses A2.5.2, A.2.5.3 and A.2.5.4. of this Appendix are provided solely for the purposes of illustration in this Chapter and should not be referenced as examples of either the requirements of this Part or as definitive statements of the processes involved. For simplification purposes, for example, the fact that the warning system will also be active when the inducement system is active has not been mentioned in the illustrations given.

A.2.5.2. Figure 2 below illustrates the operation of the activation and deactivation mechanisms when monitoring the reagent availability for five cases:

- (a) Use case 1: the driver continues operating the vehicle in spite of the warning until vehicle operation is disabled;
- (b) Repair case 1 ("adequate" refilling): the driver refills the reagent tank so that a level above the 10% threshold is reached. Warning and inducement are de-activated;
- (c) Repair cases 2 and 3 ("inadequate" refilling): The warning system is activated. The level of warning depends on the amount of available reagent;
- (d) Repair case 4 ("very inadequate" refilling): The low-level inducement is activated immediately.

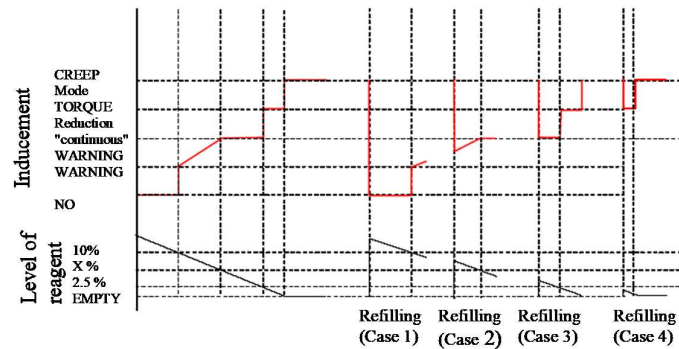


Figure 2
Reagent Availability

A.2.5.3

Figure 3 below illustrates three cases of wrong urea quality:

- (a) Use case 1: the driver continues operating the vehicle in spite of the warning until vehicle operation is disabled.
- (b) Repair case 1 ("bad" or "dishonest" repair): after disablement of the vehicle, the driver changes the quality of the reagent, but, soon after, changes it again for a poor quality one. The inducement system is immediately reactivated and vehicle operation is disabled after 2 engine operating hours.
- (c) Repair case 2 ("good" repair): after disablement of the vehicle, the driver rectifies the quality of the reagent. However, sometime afterwards, he refills again with a poor quality reagent. The warning, inducement, and counting processes restart from zero.

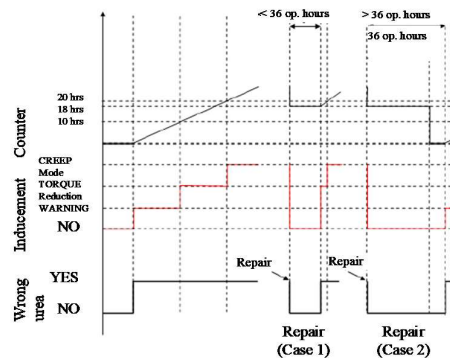


Figure 3
Filling with Poor Reagent Quality

A.2.5.4

Figure 4 below illustrates three cases of failure of the urea dosing system. This figure also illustrates the process that applies in the case of the monitoring failures described in clause 9 of this Chapter.

- (a) Use case 1: the driver continues operating the vehicle in spite of the warning until vehicle operation is disabled.
- (b) Repair case 1 ("good" repair): after disablement of the vehicle, the driver repairs the dosing system. However, sometime afterwards, the dosing system fails again. The warning, inducement, and counting processes restart from zero.
- (c) Repair case 2 ("bad" repair): during the low-level inducement time (torque reduction), the driver repairs the dosing system. Soon after, however, the dosing system fails again. The low-level inducement system is immediately reactivated and the counter restarts from the value it had at the time of repair.

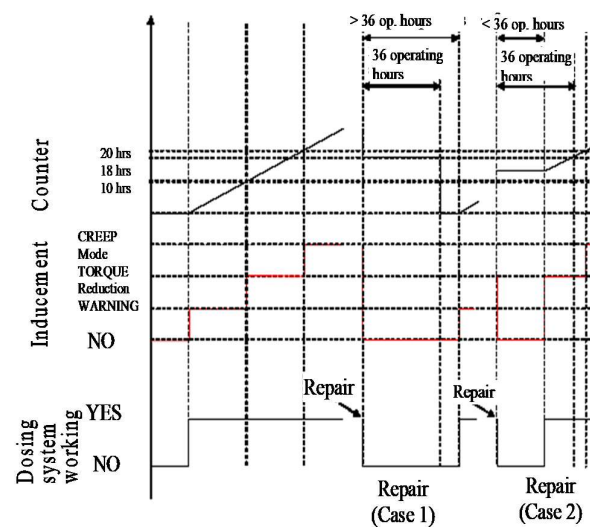
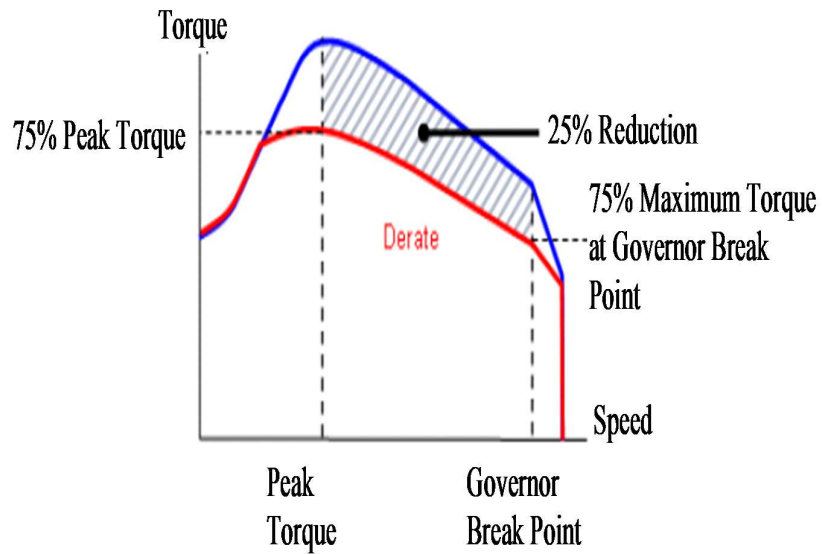


Figure 4
Failure of the Reagent Dosing System

CHAPTER 10 - APPENDIX 3

LOW LEVEL INDUCEMENT TORQUE REDUCTION SCHEME

This diagram illustrates the provisions of clause 5.3 of this Chapter on torque reduction.



CHAPTER 10 - APPENDIX 4**DEMONSTRATION OF CORRECT INSTALLATION ON A VEHICLE
IN THE CASE OF ENGINES TYPE-APPROVED AS A SYSTEM**

This Appendix applies when the vehicle manufacturer requests type-approval of a vehicle with an approved engine with regard to emissions in accordance with this Part.

In this case, and in addition to the installation requirements of clause 6 of Chapter 1 of this Part, a demonstration of the correct installation is required. This demonstration shall be performed by the presentation to the Test Agency of a technical case using evidence such as engineering drawings, functional analyses, and the results of previous tests.

Where appropriate, and if the manufacturer chooses, the evidence presented may include installations of systems or components on real or simulated vehicles, provided that the manufacturer can present evidence that the presented installation properly represents the standard that will be achieved in production.

The demonstration shall address the conformity of the following elements to the requirements of this Chapter:

- (a) The installation on board the vehicle as regards its compatibility with the engine system (hardware, software and communication);
- (b) The warning and inducement systems (for example, pictograms, activation schemes, etc.);
- (c) The reagent tank and the elements (for example, sensors) mounted on the vehicle for the purpose of complying with this Chapter.

Correct activation of the warning and inducement systems, and of the information storage and on-board and off-board communication systems, may be checked. No check of these systems shall require the dismounting of the engine system or components, nor shall it generate unnecessary testing burden by requiring processes such as changing of the urea quality or running of the vehicle or engine for long periods of time. In order to minimize the burden upon the vehicle manufacturer, electric disconnections and simulation of counters with high operating hours shall be selected as checks on these systems if possible.

CHAPTER 10 - APPENDIX 5
ACCESS TO "NO_x CONTROL INFORMATION"

- 5.1.** This Appendix describes the specifications permitting access to information required in order to check the status of the vehicle with regard to the correct operation of the NO_x control system ("NO_x control information").

5.2. ACCESS METHODS

- 5.2.1. The "NO_x control information" shall be provided only in accordance with the standard or standards used in association with the retrieval of engine system information from the OBD system.
- 5.2.2. Access to the "NO_x control information" shall not be dependent on any access code or other device or method obtainable only from the manufacturer or the manufacturer's suppliers. Interpretation of that information shall not require any specialized or unique decoding information, unless that information is publicly available.
- 5.2.3. It shall be possible to retrieve all "NO_x control information" from the system using the access method that is used to retrieve OBD information in accordance with Chapter 8A of this Part.
- 5.2.4. It shall be possible to retrieve all "NO_x control information" information from the system using the test equipment that is used to retrieve OBD information in accordance with Chapter 8A of this Part.
- 5.2.5. The "NO_x control information" shall be available through "read-only" access (that is, it shall not be possible to clear, reset, erase, or modify any of the data).

5.3. INFORMATION CONTENT

- 5.3.1. The "NO_x control information" shall contain at least the following information:
- (a) The VIN (vehicle identification number);
 - (b) The status of the warning system (active; non-active);
 - (c) The status of the low-level inducement system (active; enabled; non-active);
 - (d) The status of the severe inducement system (active; enabled; non-active);
 - (e) Number of warm-up cycles and number of engine operating hours since recorded "NO_x control information" was cleared due to service or repair;

- (f) The types of the counters relevant to this Chapter (reagent quality, reagent consumption, dosing system, EGR valve, monitoring system) and the number of engine operating hours indicated by each of these counters; in the case of multiple counters being used, the value to be considered for the purposes of the "NOx control information" is the value of each of the counters relative to the failure under consideration having the highest value;
- (g) The DTCs associated with the malfunctions relevant to this Chapter and when their status is 'potential' or 'confirmed and active';

CHAPTER 10 - APPENDIX 6
DEMONSTRATION OF THE MINIMUM ACCEPTABLE
REAGENT CONCENTRATION CD_{min}

- 1.0** The manufacturer shall demonstrate the correct value of the minimum acceptable reagent quality CD_{min} during type approval by performing the hot part of the WHTC cycle, in accordance with the provisions of Chapter 3 of this Part, using a reagent with the concentration CD_{min} .
- 2.0** The test shall follow the appropriate pre-conditioning cycle, permitting a closed loop NOx control system to perform adaptation to the quality of the reagent with the concentration CD_{min} .
- 3.0** The pollutant emissions resulting from this test shall be lower than the emission limits specified in clauses 7.1.1 or 7.1.1.1 of this Chapter.

CHAPTER 11

CO₂ EMISSIONS AND FUEL CONSUMPTION

1.0 INTRODUCTION

- 1.1 This Chapter sets out the provisions and test procedures for reporting CO₂ emissions and fuel consumption.

2.0 GENERAL REQUIREMENTS

- 2.1. CO₂ emissions and fuel consumption shall be determined over the WHTC and WHSC test cycles in accordance with clauses 7.2 to 7.8 of Chapter 3 of this Part.
- 2.2. The test results shall be reported as cycle averaged brake specific values and expressed in the unit of g/kWh.

3.0 DETERMINATION OF CO₂ EMISSIONS

3.1. Raw measurement

This clause shall apply, if CO₂ is measured in the raw exhaust gas.

3.1.1. Measurement

CO₂ in the raw exhaust gas emitted by the engine submitted for testing shall be measured with a non-dispersive infrared (NDIR) analyzer in accordance with clause 9.3.2.3 and Appendix 2 of Chapter 3 of this Part.

The measurement system shall meet the linearity requirements of clause 9.2. and Table 7 of Chapter 3 of this Part.

The measurement system shall meet the requirements of clauses 9.3.1., 9.3.4. and 9.3.5. of Chapter 3 of this Part.

3.1.2. Data Evaluation

The relevant data shall be recorded and stored in accordance with clause 7.6.6. of Chapter 3 of this Part. The traces of the recorded concentrations and the trace of the exhaust gas mass flow rate shall be time aligned with the transformation time as defined in clause 3.1. of Chapter 3 of this Part.

3.1.3. Calculation of cycle Averaged Emission

If measured on a dry basis, the dry/wet correction according to clause 8.1. of Chapter 3 of this Part. shall be applied to the instantaneous concentration values before any further calculation is done.

The mass of CO₂ (g/test) shall be determined by calculating the instantaneous mass emissions from the raw CO₂ concentration and the exhaust gas mass flow, aligned with respect to their transformation times as determined in accordance with clause 8.4.2.2. of Chapter 3

of this Part. integrating the instantaneous values over the cycle, and multiplying the integrated value with the u values of CO₂ from Table 5 of Chapter 3 of this Part.

The following equation shall be applied:

$$m_{CO_2} = \sum_{i=1}^{i=n} u_{CO_2} \times c_{CO_2,i} \times q_{mew,i} \times \frac{1}{f} \text{ (in g/test)}$$

where:

u_{CO_2} is the ratio between CO₂ density and density of the exhaust gas

$c_{CO_2,i}$ is the instantaneous CO₂ concentration in the exhaust gas, ppm

$q_{mew,i}$ is the instantaneous exhaust mass flow, kg/s

f is the data sampling rate, Hz

n is the number of measurements

Optionally, the CO₂ mass may be calculated in accordance with clause 8.4.2.4. of Chapter 3 of this Part by using a CO₂ molar mass (M_{CO_2}) of 44.01 g/mol.

3.2. Dilute measurement

This clause applies, if CO₂ is measured in the dilute exhaust gas.

3.2.1. Measurement

CO₂ in the dilute exhaust gas emitted by the engine submitted for testing shall be measured with a non-dispersive infrared (NDIR) analyzer in accordance with clause 9.3.2.3 and Appendix 2 of Chapter 3 of this Part. Dilution of the exhaust shall be done with filtered ambient air, synthetic air or nitrogen. The flow capacity of the full flow system shall be large enough to completely eliminate water condensation in the dilution and sampling systems.

The measurement system shall meet the linearity requirements of clause 9.2. and Table 7 of Chapter 3 of this Part.

The measurement system shall meet the requirements of clauses 9.3.1., 9.3.4. and 9.3.5. of Chapter 3 of this Part.

3.2.2. Data evaluation

The relevant data shall be recorded and stored in accordance with clause 7.6.6. of Chapter 3 of this Part.

3.2.3. Calculation of cycle averaged emission

If measured on a dry basis, the dry/wet correction according to clause 8.1. of Chapter 3 shall be applied.

For systems with constant mass flow (with heat exchanger), the mass of CO₂ (g/test) shall be determined with the following equation:

$$m_{CO_2} = 0.001519 \times c_{CO_2} \times m_{ed} \text{ (in g/test)}$$

Where:

c_{CO_2} is the average background corrected CO₂ concentration

0.001519 is the ratio between CO₂ density and density of air (u factor)

m_{ed} is the total diluted exhaust mass over the cycle, kg

For systems with flow compensation (without heat exchanger), the mass of CO₂ (g/test) shall be determined by calculating the instantaneous mass emissions and integrating the instantaneous values over the cycle. Also, the background correction shall be applied directly to the instantaneous concentration values. The following equation shall be applied:

$$M_{CO_2} = \sum_{i=1}^n [(m_{ed,i} \times c_{CO_2,e} \times 0.001519)] - [(m_{ed} \times c_{CO_2,d} \times (1 - 1/D) \times 0.001519)]$$

where:

$c_{CO_2,e}$ is the CO₂ concentration measured in the diluted exhaust gas, ppm

$c_{CO_2,d}$ is the CO₂ concentration measured in the dilution air, ppm

0.001519 is the ratio between CO₂ density and density of air (u factor)

$m_{ed,i}$ is the instantaneous mass of the diluted exhaust gas, kg

m_{ed} is the total mass of diluted exhaust gas over the cycle, kg

D is the dilution factor

Optionally, the u factor may be calculated with equation 57 in clause 8.5.2.3.1. of Chapter 3 of this Part by using a CO₂ molar mass (M_{CO_2}) of 44.01 g/mol.

CO₂ background correction shall be applied in accordance with clause 8.5.2.3.2. of Chapter 3 of this Part.

3.3 Calculation of Brake Specific Emissions

The cycle work needed for the calculation of brake specific CO₂ emissions shall be determined in accordance with clause 7.8.6. of Chapter 3 of this Part.

3.3.1 WHTC

The brake specific emissions e_{CO_2} (g/kWh) shall be calculated as follows.

$$e_{CO_2} = \frac{(0.14 \times m_{CO_2, cold}) + (0.86 \times m_{CO_2, hot})}{(0.14 \times W_{act, cold}) + (0.86 \times W_{act, hot})}$$

Where:

$m_{CO_2, cold}$ is the CO₂ mass emissions of the cold start test, g/test

$m_{CO_2, hot}$ is the CO₂ mass emissions of the hot start test, g/test

$W_{act, cold}$ is the actual cycle work of the cold start test, kWh

$W_{act, hot}$ is the actual cycle work of the hot start test, kWh

3.3.2 WHSC

The brake specific emissions e_{CO_2} (g/kWh) shall be calculated as follows:

$$e_{CO_2} = \frac{m_{CO_2}}{W_{act}}$$

Where:

m_{CO_2} is the CO₂ mass emissions, g/test

W_{act} is the actual cycle work, kWh

4.0 DETERMINATION OF FUEL CONSUMPTION

4.1 Measurement

Measurement of the instantaneous fuel flow shall be done by systems that preferably measure mass directly such as the following:

- (a) Mass flow sensor
- (b) Fuel weighing
- (c) Coriolis meter

The fuel flow measurement system shall have the following:

- (a) An accuracy of ± 2 per cent of the reading or ± 0.3 per cent of full scale whichever is better;
- (b) A precision of ± 1 per cent of full scale or better;
- (c) A rise time that does not exceed 5 s.

The fuel flow measurement system shall meet the linearity requirements of clause 9.2. And Table 7 of Chapter 3 of this Part.

Precautions shall be taken to avoid measurement errors. Such precautions shall at least include the following:

- (a) The careful installation of the device according to the instrument manufacturers' recommendations and to good engineering practice,
- (b) Flow conditioning as needed to prevent wakes, eddies, circulating flows, or flow pulsations that affect accuracy or precision of the fuel flow system,
- (c) Account for any fuel that bypasses the engine or returns from the engine to the fuel storage tank.

4.2 Data Evaluation

The relevant data shall be recorded and stored in accordance with clause 7.6.6. of Chapter 3 of this Part.

4.3 Calculation of cycle averaged fuel consumption.

The mass of fuel (g/test) shall be determined by the sum of the instantaneous values over the cycle, as follows:

$$q_{mf} = \sum_{i=1}^{i=n} q_{mf,i} \times \frac{1}{f} \times 1000$$

where:

$q_{mf,i}$ is the instantaneous fuel flow, kg/s

f is the data sampling rate, Hz

n is the number of measurements

4.4 Calculation of brake specific fuel consumption

The cycle work needed for the calculation of the brake specific fuel consumption shall be determined in accordance with clause 7.8.6. of Chapter 3 of this Part.

4.4.1. WHTC

The brake specific fuel consumption e_f (g/kWh) shall be calculated as follows:

$$e_f = \frac{(0.14 \times q_{mf,cold}) + (0.86 \times q_{mf,hot})}{(0.14 \times W_{act,cold}) + (0.86 \times W_{act,hot})}$$

Where:

$q_{mf, cold}$ is the fuel mass of the cold start test, g/test

$q_{mf, hot}$ is the fuel mass of the hot start test, g/test

$W_{act, cold}$ is the actual cycle work of the cold start test, kWh

$W_{act, hot}$ is the actual cycle work of the hot start test, kWh

4.4.2 WHSC

The brake specific fuel consumption e_f (g/kWh) shall be calculated as follows:

$$e_f = \frac{q_{mf}}{W_{act}}$$

Where:

q_{mf} is the fuel mass, g/test

W_{act} is the actual cycle work, kWh

CHAPTER 11 - APPENDIX 1

PROVISIONS ON CO₂ EMISSIONS AND FUEL CONSUMPTION FOR EXTENSION OF A TYPE APPROVAL FOR A VEHICLE TYPE APPROVED UNDER THIS PART WITH A REFERENCE MASS EXCEEDING 2,380 kg BUT NOT EXCEEDING 2,610 kg

A.1.1. INTRODUCTION

A.1.1.1. This Appendix sets out the provisions and test procedures for reporting CO₂ emissions and fuel consumption for extension of type approval for a vehicle type approved under this Part to a vehicle with a reference mass exceeding 2,380 kg but not exceeding 2,610 kg.

A.1.2. GENERAL REQUIREMENTS

A.1.2.1. In order to receive an extension of an type-approval for a vehicle in respect of its engine type approved under this Part to a vehicle with a reference mass exceeding 2,380 kg but not exceeding 2,610kg the manufacturer shall meet the requirements of Chapter 19 of AIS-137 (Part 3) with the exceptions specified below.

A.1.2.1.2. Chapter 19 of AIS-137 (Part 3) shall be understood as follows:

- (1) Density: measured on the test fuel according to ISO 3675 or an equivalent method. For petrol, diesel, ethanol (E85) and ethanol for dedicated C.I. engines (ED95) the density measured at 288 K (15°C) will be used; for LPG and natural gas/biomethane a reference density shall be used, as follows:

0.538kg/L for LPG

0.654 kg/m³ for NG

- (2) Hydrogen-carbon-oxygen ratio: fixed values shall be used which are:

C₁H_{1,93}O_{0,032} for petrol (E10),

C₁H_{1,86}O_{0,006} for diesel (B7),

C₁H_{2,525} for LPG (liquefied petroleum gas),

CH₄ for NG (natural gas) and biomethane,

C₁H_{2,74}O_{0,385} for ethanol (E85),

C₁H_{2,92}O_{0,46} for ethanol for dedicated C.I. engines (ED95)

A 1.2.1.3 Chapter 19 of AIS-137 (Part 3) shall be understood as follows:

- (a) for vehicles with a positive ignition engine fuelled with petrol (E10):

$$FC = (0.120/D) \cdot [(0.831 \cdot HC) + (0.429 \cdot CO) + (0.273 \cdot CO_2)]$$

(b) for vehicles with a positive ignition engine fuelled with LPG:

$$FC_{\text{norm}} = (0.1212/0.538) \cdot [(0.825 \cdot HC) + (0.429 \cdot CO) + (0.273 \cdot CO_2)]$$

If the composition of the fuel used for the test differs from the composition that is assumed for the calculation of the normalised consumption, on the manufacturer's request a correction factor cf may be applied, as follows

$$FC_{\text{norm}} = (0.1212/0.538) \cdot (cf) \cdot [(0.825 \cdot HC) + (0.429 \cdot CO) + (0.273 \cdot CO_2)]$$

The correction factor cf, which may be applied, is determined as follows:

$$cf = 0.825 + 0.0693 n_{\text{actual}}$$

where:

n_{actual} is the actual H/C ratio of the fuel used

(c) for vehicles with a positive ignition engine fuelled with NG/biomethane:

$$FC_{\text{norm}} = (0.1336/0.654) \cdot [(0.749 \cdot HC) + (0.429 \cdot CO) + (0.273 \cdot CO_2)]$$

(d) for vehicles with a positive ignition engine fuelled with ethanol (E85):

$$FC = (0.1742/D) \cdot [(0.574 \cdot HC) + (0.429 \cdot CO) + (0.273 \cdot CO_2)]$$

(e) for vehicles with a compression ignition engine fuelled with diesel (B7):

$$FC = (0.1165/D) \cdot [(0.859 \cdot HC) + (0.429 \cdot CO) + (0.273 \cdot CO_2)]$$

(f) for vehicles with a dedicated compression ignition engine fuelled with ethanol (ED95)

$$FC = (0.186/D) \cdot [(0.538 \cdot HC) + (0.429 \cdot CO) + (0.273 \cdot CO_2)]$$

In these formulae:

FC is the fuel consumption in litre per 100 km (in the case of petrol, ethanol, LPG, diesel or biodiesel) or in m³ per 100 km (in the case of natural gas)

HC is the measured emission of hydrocarbons in g/km

CO is the measured emission of carbon monoxide in g/km

CO₂ is the measured emission of carbon dioxide in g/km

D is the density of the test fuel

In case of gaseous fuels this is the density at 288K (15°C)

CHATER 12

TYPE APPROVAL OF REPLACEMENT POLLUTION CONTROL DEVICES AS SEPARATE TECHNICAL UNIT

1.0 INTRODUCTION

1.1. This Chapter contains additional requirements for the type approval of replacement pollution control devices as separate technical units.

1.2. Definition

1.2.1. "Type of pollution control device" means catalytic converters and particulate filters which do not differ in any of the following essential aspects:

- (a) Number of substrates, structure and material;
- (b) Type of activity of each substrate;
- (c) Volume, ratio of frontal area and substrate length;
- (d) Catalyst material content;
- (e) Catalyst material ratio;
- (f) Cell density;
- (g) Dimensions and shape;
- (h) Thermal protection.

2.0 GENERAL REQUIREMENTS

2.1. Marking

2.1.1. Each replacement pollution control device shall bear at least the following identifications:

- (a) The manufacturer's name or trade mark;
- (b) The make and identifying part number of the replacement pollution control device as recorded in the information document issued in accordance with the model set out in Appendix 1 of this Chapter.

2.1.2. Each original replacement pollution control device shall bear at least the following identifications:

- (a) The vehicle or engine manufacturer's name or trade mark;
- (b) The make and identifying part number of the original replacement pollution control device as recorded in the information referred to in clause 2.3 of this Chapter.

2.2 Documentation

2.2.1 Each replacement pollution control device shall be accompanied by the following information:

- (a) The manufacturer's name or trade mark;
- (b) The make and identifying part number of the replacement pollution control device as recorded in the information document issued in accordance with the model set out in Appendix 1 of this Chapter;
- (c) The vehicles or engines including year of manufacture for which the replacement pollution control device is approved, including, where applicable, a marking to identify if the replacement pollution control device is suitable for fitting to a vehicle that is equipped with an onboard diagnostic (OBD) system;
- (d) Installation instructions.

The information referred to in this point shall be available in the product catalogue distributed to points of sale by the manufacturer of replacement pollution control devices.

2.2.2 Each original replacement pollution control device shall be accompanied by the following information:

- (a) The vehicle or engine manufacturer's name or trade mark;
- (b) The make and identifying part number of the original replacement pollution control device as recorded in the information mentioned in clause 2.3.below;
- (c) The vehicles or engines for which the original replacement pollution control device is of a type covered by Chapter 2 of this Part including, where applicable, a marking to identify if the original replacement pollution control device is suitable for fitting to a vehicle that is equipped with an on-board diagnostic (OBD) system;
- (d) Installation instructions.

This information referred to in this point shall be available in the product catalogue distributed to points of sale by the vehicle or engine manufacturer.

2.3 For an original replacement pollution control device, the vehicle or engine manufacturer shall provide to the Test Agency the necessary information in electronic format which makes the link between the relevant part numbers and the type approval documentation.

This information shall contain the following:

- (a) Make(s) and type(s) of vehicle or engine;

- (b) Make(s) and type(s) of original replacement pollution control device;
- (c) Part number(s) of original replacement pollution control device;
- (d) Type approval number of the relevant engine or vehicle type(s).

3.0 SEPARATE TECHNICAL UNIT TYPE APPROVAL MARK

- 3.1. Every replacement pollution control device conforming to the type approved under this Part as a separate technical unit shall bear a type approval mark.

4.0 TECHNICAL REQUIREMENTS

4.1. General requirements

- 4.1.1. The replacement pollution control device shall be designed, constructed and capable of being mounted so as to enable the engine and vehicle to comply with the rules with which it was originally in compliance and that pollutant emissions are effectively limited throughout the normal life of the vehicle under normal conditions of use.
- 4.1.2. The installation of the replacement pollution control device shall be at the exact position of the original equipment pollution control device, and the position on the exhaust line of the exhaust gas, temperature and pressure sensors shall not be modified.
- 4.1.3. If the original equipment pollution control device includes thermal protections, the replacement pollution control device shall include equivalent protections.
- 4.1.4. Upon request of the applicant for the type approval of the replacement component, the Test Agency that granted the original type approval of the engine system shall make available on a non-discriminatory basis, the information referred to in clauses 3.2.12.2.6.8.1.1. and 3.2.12.2.6.8.2.1. in the information document contained in Chapter 2 of this Part for each engine to be tested.

4.2 General Durability Requirements

The replacement pollution control device shall be durable, that is designed, constructed and capable of being mounted so that reasonable resistance to the corrosion and oxidation phenomena to which it is exposed is obtained, having regard to the conditions of use of the vehicle.

The design of the replacement pollution control device shall be such that the elements active in controlling emissions are adequately protected from mechanical shock so as to ensure that pollutant emissions are effectively limited throughout the normal life of the vehicle under normal conditions of use.

The applicant for type approval shall provide to the Test Agency details of the test used to establish robustness to mechanical shock and the results of that test.

4.3 Requirements Regarding Emission

4.3.1 Outline of procedure for evaluation of emissions

The engines indicated in clause 3.4.4. (a) of Chapter 1 of this Part equipped with a complete emissions control system including the replacement pollution control device of the type for which approval is requested, shall be subjected to tests appropriate for the intended application as described in Chapter 3 of this Part, in order to compare its performance with the original emissions control system according to the procedure described below.

4.3.1.1 Where the replacement pollution control device does not comprise the complete emissions control system, only new original equipment or new original replacement pollution control components shall be used to provide a complete system.

4.3.1.2 The emissions control system shall be aged according to the procedure described in clause 4.3.2.4. of this Chapter and retested to establish the durability of its emissions performance.

The durability of a replacement pollution control device is determined from a comparison of the 2 successive sets of exhaust gas emissions tests.

(a) The first set is that made with the replacement pollution control device which has been run in with 12 WHSC cycles;

(b) The second set is that made with the replacement pollution control device which has been aged by the procedures detailed below.

Where approval is applied for different types of engines from the same engine manufacturer, and provided that these different types of engines are fitted with an identical original equipment pollution control system, the testing may be limited to at least two engines selected after agreement with the Test Agency

4.3.2 Procedure for evaluation of emissions performance of a replacement pollution control device.

4.3.2.1 The engine or engines shall be fitted with a new original equipment pollution control device according to clause 4.11.4. of Chapter 1 of this Part.

The exhaust after-treatment system shall be preconditioned with 12 WHSC cycles. After this preconditioning, the engines shall be tested according to the WHDC test procedures specified in Chapter 3 of this Part. Three exhaust gas tests of each appropriate type shall be performed.

The test engines with the original exhaust after-treatment system or original replacement exhaust after-treatment system shall comply with the limit values according to the type approval of the engine or vehicle.

4.3.2.2 Exhaust Gas Test with Replacement Pollution Control Device

The replacement pollution control device to be evaluated shall be fitted to the exhaust after-treatment system tested according to the requirements of clause 4.3.2.1., replacing the relevant original equipment exhaust after treatment device.

The exhaust after-treatment system incorporating the replacement pollution control device shall then be preconditioned with 12 WHSC cycles. After this preconditioning, the engines shall be tested according to the WHDC procedures described in Chapter 3 of this Part. Three exhaust gas tests of each appropriate type shall be performed.

4.3.2.3 Initial evaluation of the emission of pollutants of engines equipped with replacement pollution control devices.

The requirements regarding emissions of the engines equipped with the replacement pollution control device shall be deemed to be fulfilled if the results for each regulated pollutant (CO, HC, NMHC, methane, NO_x, NH₃, particulate mass and particle number as appropriate for the type approval of the engine) meet the following conditions:

$$(1) \quad M \leq 0.85S + 0.4G$$

$$(2) \quad M \leq G$$

Where:

M: mean value of the emissions of one pollutant obtained from the three tests with the replacement pollution control device;

S: mean value of the emissions of one pollutant obtained from the three tests with the original or original replacement pollution control device;

G: limit value of the emissions of one pollutant according to the type approval of the vehicle.

4.3.2.4 Durability of Emissions Performance

The exhaust after-treatment system tested in clause 4.3.2.2. and incorporating the replacement pollution control device shall be subjected to the durability procedures described in Appendix 4 of this Chapter.

4.3.2.5 Exhaust gas test with aged replacement pollution control device

The aged exhaust after-treatment system incorporating the aged replacement control device shall then be fitted to the test engine used in clause 4.3.2.1. and 4.3.2.2.

The aged exhaust after-treatment systems shall be preconditioned with 12 WHSC cycles and subsequently tested using the WHDC procedures described in Chapter 3 of this Part. Three exhaust gas tests of each appropriate type shall be performed

4.3.2.6 **Determination of ageing factor for the replacement pollution control device**

The ageing factor for each pollutant shall be the ratio of the applied emission values at the useful life end point and at the start of the service accumulation. (e.g. if the emissions of pollutant A at the useful life end point are 1.50 g/kWh and those at the start of the service accumulation are 1.82 g/kWh, the ageing factor is $1.82/1.50 = 1.21$).

4.3.2.7 **Evaluation of the emission of pollutants of engines equipped with replacement pollution control devices**

The requirements regarding emissions of the engines equipped with the aged replacement pollution control device (as described in clause 4.3.2.5.) shall be deemed to be fulfilled if the results for each regulated pollutant (CO, HC, NMHC, methane, NO_x, NH₃, particulate mass and particle number as appropriate for the type approval of the engine) meet the following condition:

$$M * AF \leq G$$

Where:

M: mean value of the emissions of one pollutant obtained from the three tests with the preconditioned replacement pollution control device before ageing (i.e. results from clause 4.3.2.);

AF: the ageing factor for one pollutant;

G: limit value of the emissions of one pollutant according to the type approval of the vehicle(s).

4.3.3 **Replacement Pollution Control Device Technology Family**

The manufacturer may identify a replacement pollution control device technology family, to be identified by basic characteristics which shall be common to devices within the family. To belong to the same replacement pollution control device technology family, the replacement pollution control devices shall have the following:

- (a) The same emissions control mechanism (oxidation catalyst, three-way catalyst, particulate filter, selective catalytic reduction for NO_x etc.);
- (b) The same substrate material (same type of ceramic, or same type of metal);
- (c) The same substrate type and cell density;
- (d) The same catalytically active materials and, where more than one, the same ratio of catalytically active materials;
- (e) The same total charge of catalytically active materials;
- (f) The same type of wash coat applied by the same process.

- 4.3.4 Assessment of the durability of emissions performance of a replacement pollution control device by use of a technology family ageing factor.

Where the manufacturer has identified a replacement pollution control technology family, the procedures described in clause 4.3.2. may be used to determine the ageing factors for each pollutant for the parent of that family. The engine on which these tests are conducted shall have a minimum engine displacement of 0.75 dm³ per cylinder.

4.3.4.1 **Determination of Durability Performance of Family Members**

A replacement pollution control device A within a family and intended to be mounted on an engine of displacement CA may be considered to have the same ageing factors as the parent replacement pollution control device P, determined on an engine of displacement CP, if the following conditions are fulfilled:

$$VA/CA \geq VP/CP$$

Where:

VA: Substrate volume (in dm³) of replacement pollution control device A

VP: Substrate volume (in dm³) of the parent replacement pollution control device P of the same family and both engines use the same method for regeneration of any emissions control devices incorporated in the original exhaust after-treatment system. This requirement shall apply only where devices requiring regeneration are incorporated in the original exhaust after-treatment system.

If these conditions are fulfilled, the emissions durability performance of other members of the family may be determined from the emissions results (S) of that family member determined according to the requirements set out in clauses 4.3.2.1., 4.3.2.2. and 4.3.2.3. and using the ageing factors determined for the parent of that family.

4.4 **Requirements regarding exhaust back-pressure**

The back pressure shall not cause the complete exhaust system to exceed the value specified according to clause 6.1.2. of Chapter 1 of this Part.

- 4.5. Requirements regarding OBD compatibility (applicable only to replacement pollution control devices intended to be fitted to vehicles equipped with an OBD system)

- 4.5.1. OBD compatibility demonstration is required only when the original pollution control device was monitored in the original configuration.

- 4.5.2. The compatibility of the replacement pollution control device with the OBD system shall be demonstrated by using the procedures described in Chapter 8B of this Part for replacement pollution control devices intended to be fitted to engines or vehicles type-approved in accordance with this Part.
- 4.5.3. The provisions in this Part applicable to components other than pollution control devices shall not apply.
- 4.5.4. The replacement pollution control device manufacturer may use the same preconditioning and test procedure as used during the original type approval. In this case, the Test Agency which granted original type approval of an engine of a vehicle shall provide, on request and on a non-discriminatory basis, information on test conditions in Chapter 2 of this Part, which contains the number and type of preconditioning cycles and the type of test cycle used by the original equipment manufacturer for OBD testing of the pollution control device.
- 4.5.5. In order to verify the correct installation and functioning of all other components monitored by the OBD system, the OBD system shall indicate no malfunction and have no stored fault codes prior to the installation of any of the replacement pollution control device. An evaluation of the status of the OBD system at the end of the tests described in clauses 4.3.2. to 4.3.2.7 of this Chapter. may be used for this purpose.
- 4.5.6. The malfunction indicator shall not activate during vehicle operation required by clauses 4.3.2. to 4.3.2.7 of this Chapter.

5.0 CONFORMITY OF PRODUCTION

- 5.1. Measures to ensure the conformity of production shall be taken in accordance with clause 8. of Chapter 1 of this Part.
- 5.2. **Special provisions**
 - 5.2.1. For the application of clause 8. of Chapter 1 of this Part, the tests described in clause 4.3. of this Chapter (requirements regarding emissions) may be carried out. In this case, the holder of the approval may request, as an alternative, to use as a basis for comparison not the original equipment pollution control device, but the replacement pollution control device which was used during the type approval tests (or another sample that has been proven to conform to the approved type). Emissions values measured with the sample under verification shall then on average not exceed by more than 15 per cent the mean values measured with the sample used for reference.

CHAPTER 12 - APPENDIX 1

MODEL INFORMATION DOCUMENT

Information document No ...

Relating to the type approval of replacement pollution control devices

The following information shall be supplied in triplicate and include a list of contents. Any drawings shall be supplied in appropriate scale and sufficient detail on size A4 or on a folder of A4 format. Photographs, if any, shall show sufficient detail.

If the systems, components or separate technical units have electronic controls, information concerning their performance shall be supplied.

- 0. General
- 0.1 Make (trade name of manufacturer):
- 0.2. Type:
- 0.2.1. Commercial name(s) (if available):
- 0.3. Means of identification of type:
- 0.5. Name and address of manufacturer:
- 0.7. In the case of components and separate technical units, location and method of affixing of the approval mark:
- 0.8. Name(s) and address (es) of assembly plant(s):
- 0.9 Name and address of the manufacturer's authorised representative (if any): ...
- 1.0 Description of the device
- 1.1. Type of the replacement pollution control device: (oxidation catalyst, three-way catalyst, SCR catalyst, particulate filter etc.):
.....
- 1.2. Drawings of the replacement pollution control device, identifying in particular all the characteristics referred to under "type of pollution control device" in clause 1.2.1. of this Chapter:
- 1.3. Description of the engine and vehicle type or types for which the replacement pollution control device is intended:
- 1.3.1. Number(s) and/or symbol(s) characterising the engine and vehicle type(s):
- 1.3.2. Number(s) and/or symbol(s) characterising the original pollution control device(s) which the replacement pollution control device is intended to replace:
- 1.3.3. Is the replacement pollution control device intended to be compatible with OBD requirements? (Yes/No) ⁽¹⁾
- 1.3.4. Is the replacement pollution control device compatible with existing vehicle/engine control systems? (Yes/No) ⁽¹⁾
- 1.4. Description and drawings showing the position of the replacement pollution control device relative to the engine exhaust manifold(s):
.....

(1) Delete where not applicable.

CHAPTER 12 - APPENDIX 2

COMMUNICATION CONCERNING THE APPROVAL OF A REPLACEMENT POLLUTION CONTROL DEVICE PURSUANT TO THIS PART AND ITS AMENDMENTS

SECTION 1

- 0.1. Make (trade name of manufacturer):
- 0.2. Type-.....
- 0.3. Means of identification of type marked on the component/separate technical unit⁽¹⁾ (Identifying Part Number):
.....
- 0.3.1. Location of that marking:
- 0.4. Name and address of manufacturer:
- 0.5. In the case of components and separate technical units, location and method of affixing of the approval mark:
- 0.6. Name and address(es) of assembly plant(s):
- 0.7. Name and address of manufacturer's representative:

SECTION II

- 1. Additional information
- 1.1. Make and type of the replacement pollution control device: (oxidation catalyst, three-way catalyst, SCR catalyst, particulate filter etc.....
- 1.2. Engine and vehicle type(s) for which the pollution control device type-.....
- 1.3. Type(s) of engine on which the replacement pollution control device has been tested.....
- 1.3.1. Has the replacement pollution control device demonstrated compatibility with OBD requirements (Yes/No) ⁽²⁾
- 2. Test Agency responsible for carrying out the tests:
- 3. Date of test report:
- 4. Number of test report:
- 5. Remarks:
- 6. Place:.....
- 7. Date:.....
- 8. Signature:.....

Attachments : Information Package

Test Report.

(1) If the means of identification of type contains characters not relevant to describe the vehicle, component or separate technical unit types covered by this type approval certificate such characters shall be represented in the document by the symbol:"?" (e.g. ABC??123??).

(2) Delete where not applicable

CHAPTER 12 - APPENDIX 3
AGEING PROCEDURE FOR
EVALUATION OF DURABILITY

- 1.0 This Appendix set out the procedures for ageing a replacement pollution control device for the purpose of evaluating the durability.
- 2.0 For demonstrating the durability, the replacement pollution control device shall be subject to the requirements set out in clauses 1. to 3.4.2. of Chapter 6 of this Part
- 2.1 For the purpose of demonstrating durability of the replacement pollution control device the minimum service accumulation periods as set out in Chapter 6 of this Part

Table 1
Minimum Service Accumulation Period

Category of vehicle in which engine will be installed	Minimum service accumulation period
Category N ₁ vehicles	
Category N ₂ vehicles	
Category N ₃ vehicles with a maximum technically permissible mass not exceeding 16 tonnes	
Category N ₃ vehicles with a maximum technically permissible mass exceeding 16 tonnes	
Category M ₁ vehicles	
Category M ₂ vehicles	
Category M ₃ vehicles with a maximum technically permissible mass not exceeding 7.5 tonnes	
Category M ₃ vehicles with a maximum technically permissible mass exceeding 7.5 tonnes	

CHAPTER 13**ACCESS TO VEHICLE OBD INFORMATION****1.0 ACCESS TO OBD INFORMATION**

- 1.1. Applications for type approval or amendment of a type approval shall be accompanied by the relevant information concerning the engine or vehicle OBD system. This relevant information shall enable manufacturers of replacement or retrofit components to make the parts they manufacture compatible with the vehicle OBD system with a view to fault-free operation assuring the vehicle user against malfunctions. Similarly, such relevant information shall enable the manufacturers of diagnostic tools and test equipment to make tools and equipment that provide for effective and accurate diagnosis of engine or vehicle emission control systems.
- 1.2. Upon request, the Test Agency shall make clause 2.1 of this Chapter containing the relevant information on the OBD system available to any interested components, diagnostic tools or test equipment manufacturer on a non-discriminatory basis.
- 1.3. If a Test Agency receives a request from any interested components, diagnostic tools or test equipment manufacturer for information on the OBD system of an engine system or vehicle that has been type approved to this Part:
 - The Test Agency shall, within 30 days, request the manufacturer of the vehicle in question to make available the information required in clause 2.1. of this Chapter:
 - The manufacturer shall submit this information to the test agency within two months of the request;
 - The Test Agency shall attach this information to test report
- 1.4. This requirement shall not invalidate any approval previously granted pursuant to this Part nor prevent extensions to such approvals under the terms of the Part under which they were originally granted.
- 1.5. Information can only be requested for replacement or service components that are subject to CMVR type approval, or for components that form part of a system that is subject to CMVR type approval.
- 1.6. The request for information shall identify the exact specification of the engine system or vehicle model for which the information is required. It shall confirm that the information is required for the development of replacement or retrofit parts or components or diagnostic tools or test equipment.

2.0 OBD DATA

2.1. The following additional information shall be provided by the engine or vehicle manufacturer for the purposes of enabling the manufacture of OBD compatible replacement or service parts and diagnostic tools and test equipment, unless such information is covered by intellectual property rights or constitutes specific know-how of the manufacturer or the OEM supplier(s).

2.1.1. A description of the type and number of the pre-conditioning cycles used for the original type approval of the engine or vehicle.

2.1.2. A description of the type of the OBD demonstration cycle used for the original type approval of the engine or vehicle for the component monitored by the OBD system.

2.1.3. A comprehensive document describing all sensed components with the strategy for fault detection and MI activation (fixed number of driving cycles or statistical method), including a list of relevant secondary sensed parameters for each component monitored by the OBD system and a list of all OBD output codes and format used (with an explanation of each code and format) associated with individual emission-related power-train components and individual non-emission related components, where monitoring of the component is used to determine MI activation. In particular, in the case of vehicle types that use a communication link in accordance with ISO 15765-4 "Road vehicles — Diagnostics on Controller Area Network (CAN) - Part 4: Requirements for emissions-related systems", a comprehensive explanation for the data given in service \$ 05 Test ID \$ 21 to FF and the data given in service \$ 06, and a comprehensive explanation for the data given in service \$06 Test ID \$ 00 to FF, for each OBD monitor ID supported, shall be provided.

In case other communication protocols standards are used, equivalent comprehensive explanation shall be provided.

2.1.4. The information required by this clause may, for example, be defined by completing a Table as follows:

component	FAULT CODE	Monitoring strategy	Fault detection criteria	MI activation criteria	Secondary parameter	Preconditioning	Demonstration test
SCR catalyst	P20EE	NOx sensor 1 and 2 signals	Difference between sensor 1 and sensor 2 signals	2 nd cycle	Engine speed, engine load, catalyst temperature, reagent activity, exhaust mass flow	One OBD test cycle (WHTC, hot part)	OBD test cycle (WHTC, hot Part)

CHAPTER 14

ADDITIONAL TECHNICAL REQUIREMENTS FOR DIESEL-
GAS DUAL-FUEL ENGINES AND VEHICLES

1.0 SCOPE

This Chapter shall apply to dual-fuel engines and dual-fuel vehicles.

2.0 DEFINITIONS AND ABBREVIATIONS

- 2.1. **"Gas Energy Ratio (GER)"** means in case of a dual-fuel engine the ratio (expressed as a percentage) of the energy content of the gaseous fuel ⁽¹⁾ over the energy content of both fuels (diesel and gaseous).
- 2.2. **"Average gas ratio"** means the average gas energy ratio calculated over a specific operating sequence.
- 2.3. **"Heavy-Duty Dual-Fuel (HDDF) Type 1A engine"** means a dual-fuel engine that operates over the hot part of the WHTC test-cycle with an average gas ratio that is not lower than 90 per cent ($GER_{WHTC} \geq 90 \%$), and that does not idle using exclusively diesel fuel, and that has no diesel mode.
- 2.4. **"Heavy-Duty Dual-Fuel (HDDF) Type 1B engine"** means a Dual-Fuel engine that operates over the hot part of the WHTC test-cycle with an average gas ratio that is not lower than 90 per cent ($GER_{WHTC} \geq 90 \%$), and that does not idle using exclusively diesel fuel in dual-fuel mode, and that has a diesel mode.
- 2.5. **"Heavy-Duty Dual-Fuel (HDDF) Type 2A engine"** means a Dual-Fuel engine that operates over the hot part of the WHTC test-cycle with an average gas ratio between 10 per cent and 90 per cent ($10 \% < GER_{WHTC} < 90 \%$) and that has no diesel mode or that operates over the hot part of the WHTC test-cycle with an average gas ratio that is not lower than 90 per cent ($GER_{WHTC} \geq 90 \%$), but that idles using exclusively diesel fuel, and that has no diesel mode.
- 2.6. **"Heavy-Duty Dual-Fuel (HDDF) Type 2B engine"** means a Dual-Fuel engine that operates over the hot part of the WHTC test-cycle with an average gas ratio between 10 per cent and 90 per cent ($10 \% < GER_{WHTC} < 90 \%$) and that has a diesel mode or that operates over the hot part of the WHTC test-cycle with an average gas ratio that is not lower than 90 per cent ($GER_{WHTC} \geq 90 \%$), but that can idle using exclusively diesel fuel in dual-fuel mode, and that has a diesel mode.
- 2.7. **"Heavy-Duty Dual-Fuel (HDDF) Type 3B engine"**⁽²⁾ means a dual-fuel engine that operates over the hot part of the WHTC test-cycle with an average gas ratio that does not exceed 10 per cent ($GER_{WHTC} \leq 10 \%$) and that has a diesel mode.

(1) Based on the lower heating value.

(2) HDDF Type 3A are neither defined nor allowed by this Part.

3.0 DUAL-FUEL SPECIFIC ADDITIONAL APPROVAL REQUIREMENTS

3.1. Dual-Fuel-Engine Family

3.1.1. Criteria for belonging to a dual-fuel engine family:

All engines within a dual-fuel engine family shall belong to the same type of dual-fuel engines defined in clause 2.⁽¹⁾ of this Chapter and operate with the same types of fuel or when appropriate with fuels declared according to this Part as being of the same range(s).

All engines within a dual-fuel engine family shall meet the criteria defined by this Part for belonging to a compression ignition engine family.

The difference between the highest and the lowest GER_{WHTC} (i.e. the highest GER_{WHTC} minus the lowest GER_{WHTC}) within a dual-fuel engine family shall not exceed 30 per cent.

(1) For example HDDF Type 1A or HDDF Type 2B etc.

3.1.2. Selection of the parent engine

The parent engine of a dual-fuel engine family shall be selected according to the criteria defined by this Part for selecting the parent engine of a compression ignition engine family.

4.0 GENERAL REQUIREMENTS

4.1. Operating Modes of Dual-Fuel Engines and Vehicles

4.1.1. Conditions for a dual-fuel engine to operate in diesel mode

A dual-fuel engine may only operate in diesel mode if, when operating in diesel mode, it has been certified according to all the requirements of this Part concerning diesel engines.

When a dual-fuel engine is developed from an already certified diesel engine, then re-certification is required in the diesel mode.

4.1.2. Conditions for a HDDF engine to idle using diesel fuel exclusively

4.1.2.1. HDDF Type 1A engines shall not idle using diesel fuel exclusively except under the conditions defined in clause 4.1.3. for warm-up and start.

4.1.2.2. HDDF Type 1B engines shall not idle using diesel fuel exclusively in dual fuel mode.

4.1.2.3. HDDF Types 2A, 2B and 3B engines may idle using diesel fuel exclusively.

4.1.3. Conditions for a HDDF engine to warm-up or start using diesel fuel solely

- 4.1.3.1. A Type 1B, Type 2B, or Type 3B dual-fuel engine may warm-up or start using diesel fuel solely. However, in that case, it shall operate in diesel mode.
- 4.1.3.2. A Type 1A or Type 2A dual-fuel engine may warm-up or start using diesel fuel solely. However, in that case, the strategy shall be declared as an AES and the following additional requirements shall be met:
 - 4.1.3.2.1. The strategy shall cease to be active when the coolant temperature has reached a temperature of 343 K (70 °C), or within 15 minutes after it has been activated, whichever occurs first; and
 - 4.1.3.2.2. The service mode shall be activated while the strategy is active.

4.2. Service Mode

- 4.2.1. Conditions for dual-fuel engines and vehicles to operate in service mode

When its engine is operating in service mode, a dual-fuel vehicle is subject to an operability restriction and is temporarily exempted from complying with the requirements related to exhaust emissions, OBD and NOx control described in this Part.

4.2.2. Operability Restriction in Service Mode

The operability restriction applicable to dual-fuel vehicles when they operate in service mode is the one activated by the "severe inducement system" specified in Chapter 10 of this Part. The operability restriction shall not be deactivated by either the activation or deactivation of the warning and inducement systems specified in Chapter 10 of this Part. The activation and the deactivation of the service mode shall not activate or deactivate the warning and inducement systems specified in Chapter 10 of this Part. Illustrations of the operability restriction requirements are given in Appendix 2 of this Chapter.

4.2.2.1. Activation of the operability restriction

The operability restriction shall be automatically activated when the service mode is activated.

In the case where the service mode is activated according to clause 4.2.3. of this Chapter because of a malfunction of the gas supply system or because of an abnormality of gas consumption, the operability restriction shall become active after the next time the vehicle is stationary or within 30 minutes operating time after the service mode is activated, whichever comes first.

In the case where the service mode is activated because of an empty gas tank, the operability restriction shall become active as soon as the service mode is activated.

4.2.2.2. **Deactivation of the operability restriction**

In case of an empty gas tank, the operability restriction in dual fuel mode due to a lack of gaseous fuel, shall be deactivated as soon as the gas tank is refilled above the critical level.

4.2.2.3 **Repair and maintenance of LNG type A Dual fuel engines and vehicles**

In the case of LNG Type A Dual fuel engines and vehicles the manufacturer may instead of limiting the speed at 20 km/h opt for limiting the power of the engine to 20% of the declared maximum power in dual fuel mode and this at any engine speed when the service mode is activated during a repair or maintenance operation

4.2.2.3.1 The power limitation option may only be activated if the system concludes that the gas tank is empty not later than 5 min after engine cranking, the engine being at idle.

4.2.2.3.2 The power limitation option shall not be activated when the system concludes that gas tank is empty from a previous driving cycle and the gas tank has not been filled.

4.2.2.3.3 The manufacturer shall demonstrate at type approval that the power limitation option can be activated during a repair or maintenance operation.

4.2.3. **Unavailability of gaseous fuel when operating in a dual-fuel mode**

In order to permit the vehicle to keep moving and eventually to move out of the main-stream traffic, upon detection of an empty gaseous fuel tank, or of a malfunctioning gas supply system according to clause 7.2. of this Chapter, or of an abnormality of gas consumption in dual-fuel mode according to clause 7.3. of this Chapter:

- (a) Dual-fuel engines of Types 1A and 2A shall activate the service mode
- (b) Dual-fuel engines of Types 1B, 2B and 3B shall operate in diesel mode.

4.2.3.1. **Unavailability of gaseous fuel – empty gaseous fuel tank**

In the case of an empty gaseous fuel tank, the service mode or, as appropriate according to clause 4.2.3. of this Chapter, the diesel mode shall be activated as soon as the engine system has detected that the tank is empty.

When the gas availability in the tank again reaches the level that justified the activation of the empty tank warning system specified in clause 4.3.2. of this Chapter, the service mode may be deactivated, or, when appropriate, the dual-fuel mode may be reactivated.

4.2.3.2. **Unavailability of gaseous fuel – malfunctioning gas supply**

In the case of a malfunctioning gas supply system according to 7.2. of this Chapter, the service mode or, as appropriate according to clause 4.2.3. of this Chapter, the diesel mode shall be activated when the DTC relevant to that malfunction has the confirmed and active status.

As soon as the diagnostic system concludes that the malfunction is no longer present or when the information, including DTCs relative to the failures, justifying its activation is erased by a scan tool, the service mode may be deactivated, or, when appropriate, the dual-fuel mode may be reactivated.

- 4.2.3.2.1 If the counter specified in clause 4.4. of this Chapter and associated with a malfunctioning gas supply system is not at zero, and is consequently indicating that the monitor has detected a situation when the malfunction may have occurred for a second or subsequent time, the service mode or, as appropriate, the diesel mode shall be activated when the DTC has the status "potential".

4.2.3.3. **Unavailability of gaseous fuel – abnormality of gas consumption**

In case of an abnormality of gas consumption in dual-fuel mode according to clause 7.3. of this Chapter, the service mode or, as appropriate according to clause 4.2.3., the diesel mode shall be activated when the DTC relevant to that malfunction has reached the potential status.

As soon as the diagnostic system concludes that the malfunction is no longer present or when the information, including DTCs relative to the failures, justifying its activation is erased by a scan tool, the service mode may be deactivated, or, when appropriate, the dual-fuel mode may be reactivated.

4.3. **Dual-fuel Indicators**

4.3.1 **Dual-fuel operating mode indicator**

Dual-fuel engines and vehicles shall provide to the driver a visual indication of the mode under which the engine operates (dual-fuel mode, diesel mode, or service mode).

The characteristics and the location of this indicator are left to the decision of the manufacturer and may be part of an already existing visual indication system

This indicator may be completed by a message display. The system used for displaying the messages referred to in this clause may be the same as the ones used for OBD, correct operation of NOx control measures, or other maintenance purposes.

The visual element of the dual-fuel operating mode indicator shall not be the same as the one used for the purposes of OBD (that is, the MI – malfunction indicator), for the purpose of ensuring the correct operation of NOx control measures, or for other engine maintenance purposes.

Safety alerts always have display priority over the operating mode indication.

- 4.3.1.1. The dual-fuel mode indicator shall be set to service mode as soon as the service mode is activated (i.e. before it becomes actually active) and the indication shall remain as long as the service mode is active.

- 4.3.1.2. The dual-fuel mode indicator shall be set for at least one minute on dual-fuel mode or diesel mode as soon as the engine operating mode is changed from diesel to dual-fuel vice-versa. This indication is also required at key-on for at least 1 minute or at the request of the manufacturer at engine cranking. The indication shall also be given upon driver's request.

- 4.3.2. Empty gaseous fuel tank warning system (dual-fuel warning system)

A dual-fuel vehicle shall be equipped with a dual-fuel warning system that alerts the driver that the gaseous fuel tank will soon become empty.

The dual-fuel warning system shall remain active until the tank is refuelled to a level above which the warning system is activated.

The dual-fuel warning system may be temporarily interrupted by other warning signals providing important safety-related messages.

It shall not be possible to turn off the dual-fuel warning system by means of a scan-tool as long as the cause of the warning activation has not been rectified.

- 4.3.2.1. Characteristics of the dual-fuel warning system

The dual-fuel warning system shall consist of a visual alert system (icon, pictogram, etc.) left to the choice of the manufacturer.

It may include, at the choice of the manufacturer, an audible component. In that case, the cancelling of that component by the driver is permitted.

The visual element of the dual-fuel warning system shall not be the same as the one used for the OBD system (that is, the MI – malfunction indicator), for the purpose of ensuring the correct operation of NOx control measures, or for other engine maintenance purposes.

In addition, the dual-fuel warning system may display short messages, including messages indicating clearly the remaining distance or time before the activation of the operability restriction.

The system used for displaying the messages referred to in this clause may be the same as the one used for displaying additional OBD messages, messages related to correct operation of NOx control measures, or messages for other maintenance purposes.

A facility to permit the driver to dim the visual alarms provided by the warning system may be provided on vehicles for use by the rescue services or on vehicles designed and constructed for use by the armed services, civil defense, fire services and forces responsible for maintaining public order.

4.4. Malfunctioning Gas Supply Counter

The system shall contain a counting system to record the number of hours during which the engine has been operated while the system has detected a malfunctioning gas supply system according to clause 7.2 of this Chapter

- 4.4.1. The activation and deactivation criteria and mechanisms of the counter shall comply with the specifications of Appendix 2 of this Chapter.
- 4.4.2. It is not required to have a counter as specified in clause 4.4., when the manufacturer can demonstrate to the Test Agency (e.g. by means of a strategy description, experimental elements, etc...) that the dual-fuel engine automatically switches to diesel mode in case malfunction is detected.

4.5 Demonstration of the dual-fuel indicators and operability restriction

- 4.5.1 As part of the application for type-approval under this Part, the manufacturer shall demonstrate the operation of dual-fuel indicators and of the operability restriction in accordance with the provisions of Appendix 3 of this Chapter.

4.6. Communicated Torque

- 4.6.1. Communicated torque when a dual-fuel engine operates in dual-fuel mode

When a dual-fuel engine operates in dual-fuel mode:

- (a) The reference torque curve retrievable according to the requirements related to data stream information specified in Chapter 8B of this Part and referred to by Chapter 7 of this Part shall be the one obtained according to Chapter 3 of this Part when that engine is tested on an engine test bench in the dual-fuel mode;
- (b) The recorded actual torques (indicated torque and friction torque) shall be the result of the dual-fuel combustion and not the one obtained when operating with diesel fuel exclusively.

4.6.2. Communicated torque when a dual-fuel engine operates in diesel mode

When a dual-fuel engine operates in diesel mode, the reference torque curve retrievable according to the requirements related to data stream information specified in Chapter 8B of this Part and referred to by Chapter 7 of this Part shall be the one obtained according to Chapter 3 of this Part when the engine is tested on an engine test bench in diesel mode.

4.7. Requirements to limit Off-Cycle Emissions (OCE) and in-use emissions

Dual-fuel engines shall be subject to the requirements of Chapter 9 of this Part, whether operating in dual-fuel mode or in the case of Type 1B, Type 2B, and Type 3B in diesel mode.

4.7.1. PEMS Tests at Certification

The PEMS demonstration test at type-approval required in Chapter 9 of this Part shall be performed by testing the parent engine of a dual-fuel engine family when operating in dual-fuel mode.

4.7.1.1. In the case of Type 1B, Type 2B and Type 3B dual-fuel engines, an additional PEMS test shall be performed in diesel mode on the same engine and vehicle immediately after or before the PEMS demonstration test performed in dual-fuel mode.

In that case, certification can only be granted if both the PEMS demonstration test in dual-fuel mode and the PEMS demonstration test in diesel mode have concluded to a pass.

4.7.2. Additional Requirements

4.7.2.1. Adaptive strategies of a dual-fuel engine are allowed, provided that:

- (a) The engine always remains in the HDDF type (that is Type 1A, Type 2B, etc.) that has been declared for type-approval; and
- (b) In case of a Type 2 engine, the resulting difference between the highest and the lowest GER_{WHTC} within the family shall never exceed the percentage specified in clause 3.1.1 of this Chapter.; and
- (c) These strategies are declared and satisfy the requirements of Chapter 9 of this Part.

5.0 PERFORMANCE REQUIREMENTS

5.1 Emission limits applicable to HDDF Type 1A and Type 1B engines

5.1.1. The emission limits applicable to HDDF Type 1A engines and HDDF Type 1B engines operating in dual-fuel mode are those defined for PI engines in clause 5.3. of Chapter 1 of this Part.

- 5.1.2. The emission limits applicable to HDDF Type 1B engines operating in diesel mode are those defined for CI engines in clause 5.3. of Chapter 1 of this Part.
- 5.2. Emission limits applicable to HDDF Type 2A and Type 2B engines**
 - 5.2.1. Emission limits applicable over the WHSC test-cycle**
 - 5.2.1.1. For HDDF Type 2A and Type 2B engines, the exhaust emission limits (incl. the PM number limit) over the WHSC test-cycle applicable to HDDF Type 2A engines and HDDF Type 2B engines operating in dual-fuel mode are those applicable to CI engines over the WHSC test-cycle and defined in the Table of clause 5.3. of Chapter 1 of this Part.
 - 5.2.1.2. The emission limits (incl. the PM number limit) over the WHSC test-cycle applicable to HDDF Type 2B engines operating in diesel mode are those defined for CI engines in clause 5.3. of Chapter 1 of this Part.
 - 5.2.2. Emission limits applicable over the WHTC test-cycle**
 - 5.2.2.1 Emission Limits for CO, NO_x, NH₃ and PM mass

The CO, NO_x, NH₃ and PM mass emission limits over the WHTC test-cycle applicable to HDDF Type 2A engines and HDDF Type 2B engines operating in dual-fuel mode are those applicable to both CI and PI engines over the WHTC test-cycle and defined in clause 5.3. of Chapter 1 of this Part.
 - 5.2.2.2. Emission Limits for Hydrocarbons**
 - 5.2.2.2.1 NG Engines**

The THC, NMHC and CH₄ emission limits over the WHTC test-cycle applicable to HDDF Type 2A engines and HDDF Type 2B engines operating with Natural Gas in dual-fuel mode are calculated from those applicable to CI and PI engines over the WHTC test-cycle and defined in clause 5.3. of Chapter 1 of this Part. The calculation procedure is specified in clause 5.2.3 of this Chapter.
 - 5.2.2.2.2. LPG Engines**

The THC emission limits over the WHTC test-cycle applicable to HDDF Type 2A engines and HDDF Type 2B engines operating with LPG in dual fuel mode are those applicable to CI engines over the WHTC test-cycle and defined in clause 5.3. of Chapter 1 of this Part.
 - 5.2.2.3 Emission Limits for PM Number**
 - 5.2.2.3.1 The PM number limit over the WHTC test-cycle applicable to HDDF Type 2A engines and HDDF Type 2B engines operating in dual-fuel mode are those applicable to CI engines over the WHTC test-cycle and defined in clause 5.3. of Chapter 1 of this Part. In the case a PM number limit applicable to PI engines over the WHTC test-cycle would be

defined in clause 5.3. of Chapter 1 of this Part, then the requirements of clause 5.2.4. of this Chapter shall apply for calculating the limit applicable to HDDF Type 2A engines and HDDF Type 2B engines over that cycle.

- 5.2.2.3.2 The emission limits (incl. the PM number limit) over the WHTC test-cycle applicable to HDDF Type 2B engines operating in diesel mode are those defined for CI engines in clause 5.3 of Chapter 1 of this Part.

- 5.2.3 Hydrocarbon limits (in mg/kWh) applicable to HDDF Type 2A engines and to HDDF Type 2B engines operating in dual-fuel mode during the WHTC test cycle.

The following calculation procedure applies for HDDF Type 2A and HDDF Type 2B engines tested in the WHTC cycle while operating in dual-fuel mode:

Calculate the average gas ratio GER_{WHTC} over the hot part of the WHTC test cycle.

Calculate a corresponding THC_{GER} in mg/kWh using the following formula:

$$THC_{GER} = NMHC_{PI} + (CH4_{PI} * GER_{WHTC})$$

Determine the applicable THC limit in mg/kWh using the following method:

If $THC_{GER} \leq CH4_{PI}$, then

- (a) THC limit value = THC_{GER} ; and
- (b) No applicable CH_4 and $NMHC$ limit value

If $THC_{GER} > CH4_{PI}$, then

- (a) No applicable THC limit value; and
- (b) Both the $NMHC_{PI}$ and $CH4_{PI}$ limit values are applicable.

In this procedure:

$NMHC_{PI}$ is the $NMHC$ emission limit over the WHTC test-cycle and made applicable to PI engine by clause 5.3 of Chapter 1 of this Part ;

$CH4_{PI}$ is the CH_4 emission limit over the WHTC test-cycle and applicable to PI engine by clause 5.3. of Chapter 1 of this Part.

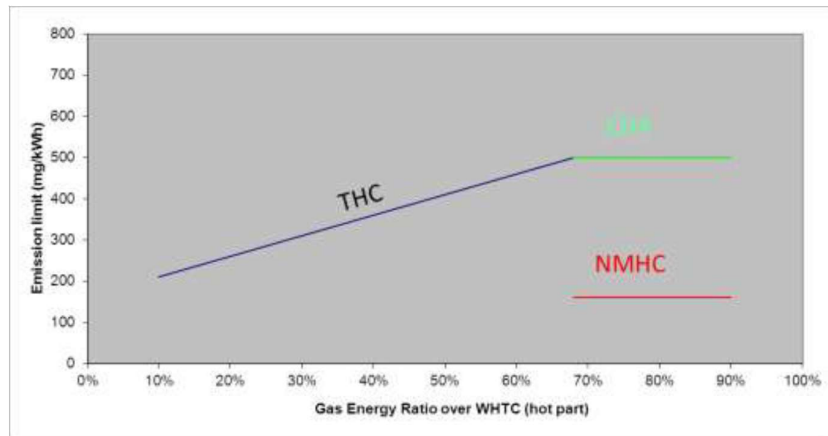


Figure 1:

Illustration of the HC Limits in the case of a HDDF Type 2 Engine Operating in Dual-Fuel Mode During the WHTC Cycle (Natural Gas Dual-Fuel Engines)

5.2.4 PM number limit (in #/kWh) applicable to HDDF Type 2A engines and to HDDF Type 2B engines operating in dual-fuel mode during the WHTC test cycle.

In the case a PM number limit applicable to PI engines over the WHTC test cycle would be defined in clause 5.3. of Chapter 1 of this Part, the following calculation procedure shall apply to HDDF Type 1A engines, to HDDF Type 1B engines, to HDDF Type 2A engines, to HDDF Type 2A and to HDDF Type 2B engines tested in the WHTC cycle while operating in dual fuel mode:

Calculate the average gas ratio GER_{WHTC} over the hot part of the WHTC test cycle, then

Calculate the PM number limit values PN limit WHTC in #/kWh applicable over the WHTC test-cycle using the following formula (linear interpolation between the CI and PI PM number limit values):

$$PN \text{ limit }_{WHTC} = PN \text{ limit }_{CI/WHTC} + (PN \text{ limit }_{PI/WHTC} - PN \text{ limit }_{CI/WHTC}) * GER_{WHTC}$$

Where:

PN limit $_{PI/WHTC}$ is the PM number limit applicable to PI engines over the WHTC test cycle;

PN limit $_{CI/WHTC}$ is the PM number limit applicable to CI engines over the WHTC test cycle.

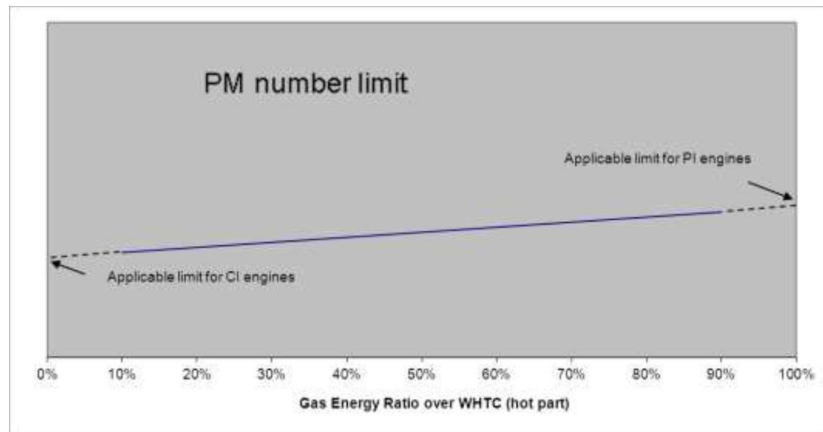


Figure 2

Illustration of the PN Limits in the case of a HDDF Type 2 Engine Operating in Dual-Fuel Mode During The WHTC Cycle

5.3 Emission limits applicable to HDDF Type 3B engines operating in dual-fuel mode

The emissions limits applicable to HDDF Type 3B engines whether operating in dual-fuel mode or in diesel mode are the exhaust emission limits applicable to CI engines.

5.4 Conformity Factors

Principally, the emission limit applicable for applying the conformity factor used when performing a PEMS test, whether a PEMS test at certification or a PEMS test when checking and demonstrating the conformity of in-service engines and vehicles, should be determined on the basis of the actual GER calculated from the fuel consumption measured over the on-road test.

However, in absence of a robust way to measure the gas or the diesel fuel consumption, the manufacturer is allowed to use the GER_{WHTC} determined on the hot part of the WHTC and calculated according to this Chapter.

6.0 DEMONSTRATION REQUIREMENTS

6.1. Dual-fuel engines shall be subject to the laboratory tests specified in Table. 1 below

Table 1
Laboratory tests to be performed by a dual-fuel engine

	Type 1A	Type 1B	Type 2A	Type 2B	Type 3B
WHTC	NMHC; CH ₄ ; CO; NO _x ; PM; PN; NH ₃	Dual-fuel mode: NMHC; CH ₄ ; CO; NO _x ; PM; PN; NH ₃	THC; NMHC; CH ₄ ; CO; NO _x ; PM; PN; NH ₃	Dual-fuel mode: THC; NMHC; CH ₄ ; CO; NO _x ; PM; PN; NH ₃	THC; CO; NO _x ; PM; PN; NH ₃
		Diesel mode: THC; CO; NO _x ; PM; PN; NH ₃		Diesel mode: THC; CO;NO _x ; PM; PN; NH ₃	
WHSC	NO TEST	NO TEST	NMHC; CO; NO _x ; PM; PN; NH ₃	Dual-fuel mode: NMHC; CO; NO _x ; PM; PN; NH ₃	THC; CO; NO _x ; PM; PN; NH ₃
		Diesel mode: THC; CO; NO _x ; PM; PN; NH ₃		Diesel mode: THC; CO; NO _x ; PM; PN; NH ₃	
WNT Laboratory test	No test	Dual-fuel mode: no test	[HC]; CO; NO _x ; PM	Dual-fuel mode: [HC]; CO;NO _x ; PM	THC; CO; NO _x ; PM
		Diesel mode: THC; CO; NO _x ; PM		Diesel mode: THC; CO;NO _x ; PM	

6.2 Demonstrations in case of installation of type-approved HDDF engines

In addition to the requirements of this Part related to the installation of an engine that is type-approved as separate technical unit, a demonstration of the correct installation on a vehicle of a dual-fuel engine shall be done on the basis of appropriate elements of design, results of verification tests, etc. It shall address the conformity of the following elements to the requirements of this Chapter:

- (a) The dual-fuel indicators and warnings as specified in this Chapter (pictogram, activation schemes, etc.);
- (b) The fuel storage system;
- (c) The performance of the vehicle in service mode.

Correct indicator illumination and warning system activation will be checked. But any check shall not force dismantling the engine system (e.g. an electric disconnection may be selected).

6.3. Demonstration requirements in case of a Type 2 Engine

The manufacturer shall present the Test Agency with evidence showing that the GER_{WHTC} span of all members of the dual-fuel engine family remains within the percentage specified in clause 3.1.1. of this Chapter (for example, through algorithms, functional analyses, calculations, simulations, results of previous tests, etc.).

6.4. Additional demonstration requirements in case of a universal fuel range Type Approval

On request of the manufacturer and with approval of the Test Agency, a maximum of two times the last 10 minutes of the WHTC may be added to the adaptation run between the demonstration tests.

6.5. Requirements for demonstrating the durability of a dual-fuel Engine

Provisions of Chapter 6 of this Part shall apply

7.0 OBD REQUIREMENTS

7.1 General OBD Requirements

All dual-fuel engines and vehicles shall comply with the requirements specified in Chapter 8A of this Part and applicable to diesel engines, independent whether operating in dual-fuel or diesel mode.

In case a dual-fuel engine system is equipped with oxygen sensor(s), the requirements applicable to gas engines in item 13. in Appendix 3 of Chapter 8B of this Part shall apply.

In case a dual-fuel engine system is equipped with a 3-way catalyst, the requirements applicable to gas engines in items 7., 10., and 15. in Appendix 3 of Chapter 8 B of this Part shall apply.

- 7.1.1. Additional general OBD requirements in case of Type 1B, Type 2B and Type 3B dual-fuel engines and vehicles.
 - 7.1.1.1. In the case of malfunctions, the detection of which does not depend on the operation mode of the engine, the mechanisms specified in Chapter 8B of this Part that are associated with the DTC status shall not depend on the operation mode of the engine (for example, if a DTC reached the potential status in dual-fuel mode, it will get the confirmed and active status the next time the failure is detected, even in diesel mode).
 - 7.1.1.2. In the case of malfunctions where the detection depends on the operation mode of the engine, DTCs shall not get a previously active status in a different mode than the mode in which they reached the confirmed and active status.
 - 7.1.1.3. A change of the mode of operation (dual-fuel to diesel or vice-versa) shall not stop nor reset the OBD mechanisms (counters, etc.). However, in the case of failures the detection of which depends on the actual operation mode, the counters associated with these malfunctions may, at the request of the manufacturer and upon approval of the Test Agency:
 - (a) Halt and, when applicable, hold their present value when the operation mode changes;
 - (b) Restart and, when applicable, continue counting from the point at which they have been held when the operation mode changes back to the other operation mode.
 - 7.1.1.4. A possible influence of the mode of operation on the malfunction detection shall not be used to extend the time until an operability restriction becomes active.
 - 7.1.1.5. In case of a Type 1B, Type 2B, or Type 3B dual-fuel engine, the manufacturer shall specify which malfunctions are operation mode dependent. This information shall be included in the information package required in clause 8.1. (a) of Chapter 8B of this Part. The justification for operation mode dependency shall be included in the information package required in clause 8.1. (b) of Chapter 8B of this Part.

7.2. Monitoring of The Gas Supply System

HDDF engines and vehicles shall monitor the gas supply system within the engine system (incl. the signals coming from outside of the engine system) according to the specifications of item 1. in Appendix 3 of Chapter 8B of this Part – component monitoring.

7.3. Monitoring of The Gaseous Fuel Consumption

Dual-fuel vehicles shall include a means of determining gas fuel consumption and providing off-board access to consumption information. Abnormality of the gaseous fuel consumption (e.g. a deviation of 50 per cent of the normal gaseous fuel consumption) shall be monitored – performance monitoring.

The monitor for insufficient gaseous fuel consumption shall run continuously whenever in dual-fuel mode, however the maximum detection period is 48 hours of operation in dual-fuel mode.

The monitor shall not be subject to the "IUPR" requirements.

7.4 OBD Deficiencies

The deficiency rules specified in Chapter 8B of this Part and applicable to diesel engines shall apply to dual-fuel engines.

A deficiency that is present both in diesel mode and in dual-fuel mode shall not be counted for each mode separately.

7.5. Erasing of failure information by means of a scan-tool

7.5.1. Erasing of information by means of a scan tool, including DTCs relative to the malfunctions considered in this Chapter shall be performed in accordance with Chapter 8B of this Part.

7.5.2. The erasing of failure information shall only be possible under "engine-off" conditions.

7.5.3. When failure information related to the gas supply system as specified in clause 7.2 of this Chapter including the DTC, is erased, the counter associated with this failure shall not be erased.

8.0 REQUIREMENTS TO ENSURE THE CORRECT OPERATION OF NO_x CONTROL MEASURES

8.1. Chapter 10 of this Part (on correct operation of NO_x control measures) shall apply to HDDF engines and vehicles, whether operating in dual-fuel or diesel mode.

8.2. Additional general OBD requirements in case of Type 1B, Type 2B and Type 3B dual-fuel engines and vehicles

8.2.1. In case of HDDF Type 1B, Type 2B and Type 3B, the torque considered to apply low level inducement defined in Chapter 10 of this Part shall be the lowest of the torques obtained in diesel mode and in dual-fuel mode.

8.2.2. The requirements of clause 7.1.1 of this Chapter concerning additional general OBD requirements in case of Type 1B, Type 2B and Type 3B dual-fuel engines and vehicles shall also apply to the diagnostic system related to the correct operation of NO_x control systems.

In particular :

- 8.2.2.1. A possible influence of the mode of operation on the malfunction detection shall not be used to extend the time until an operability restriction becomes active.
- 8.2.2.2. A change of the mode of operation (dual-fuel to diesel or vice-versa) shall not stop nor does reset the mechanisms implemented to comply with the specification of Chapter 10 (counter, etc.) of this Part. However, in the case where one of these mechanisms (for example a diagnostic system) depends on the actual operation mode the counter associated with that mechanism may, at the request of the manufacturer and upon approval of the Test Agency:
 - (a) Halt and, when applicable, hold their present value when the operation mode changes;
 - (b) Restart and, when applicable, continue counting from the point at which they have been held when the operation mode changes backs to the other operation mode.

9.0 CONFORMITY OF IN-SERVICE ENGINES OR VEHICLES/ ENGINES

The conformity of in-service dual-fuel engines and vehicles shall be performed according to the requirements specified in Chapter 7 of this Part.

The PEMS tests shall be performed in dual-fuel mode.

- 9.1. In the case of Type 1B, Type 2B and Type 3B dual-fuel engines, an additional PEMS test shall be performed in Diesel mode on the same engine and vehicle immediately after, or before, a PEMS test is performed in dual- fuel mode.

In that case the pass or fail decision of the lot considered in the statistical procedure specified in Chapter 8 of this Part shall be based on the following:

- (a) A pass decision is reached for an individual vehicle if both the PEMS test in dual-fuel mode and the PEMS test in Diesel mode have concluded a pass;
- (b) A fail decision is reached for an individual vehicle if either the PEMS test in dual-fuel mode or the PEMS test in Diesel mode has concluded a fail.

10.0 ADDITIONAL TEST PROCEDURES

- 10.1. Additional emission test procedure requirements for dual-fuel engines

- 10.1.1. Dual-fuel engines shall comply with the requirements of Appendix 4 of this Chapter in addition to the requirements of this Part (incl. Chapter 3) when performing an emission test.

10.2. Additional PEMS emission test procedure requirements for dual-fuel engines

10.2.1. When subject to a PEMS test, dual-fuel engines shall comply with the requirements of Appendix 5 of this Chapter in addition to the other PEMS requirements of this Part.

10.2.2. Torque correction

When necessary, for instance because of variation of the gas fuel composition, the manufacturer may decide to correct the ECU torque signal. In that case the following requirements shall apply.

10.2.2.1. Correction of the PEMS torque signal

The manufacturer shall submit to the Test Agency a description of the relationship permitting to extrapolate the real torque from the torques obtained during emission testing with the 2 appropriate reference fuels and from the actually retrievable torque in the ECU.

10.2.2.1.1 In the case when the torques obtained with the two reference fuels may be considered of the same magnitude (that is within the 7 per cent considered in clause 9.4.2.5. of Chapter 1 of this Part) the use of the corrected ECU value is not necessary,

10.2.2.2. Torque value to consider in a PEMS test

For PEMS test (work based window) the corrected torque value shall result from that interpolation

10.2.2.3. Conformity of the ECU torque-signal

The "Maximum torque" method specified in Appendix 4 of Chapter 7 of this Part shall be understood as demonstrating that a point between the reference maximum torque curves obtained at a certain engine speed when testing with the 2 applicable reference fuels has been reached during vehicle testing.

The value of that point shall be estimated with the agreement of the Test Agency on the basis of the actual fuel composition sampled as close as possible to the engine and the power curves obtained with each of the reference fuels during the emission certification test.

10.3 Additional dual-fuel specific CO₂ determination provisions

Clause 3.1. of Chapter 11 of this Part regarding the determination of CO₂ emissions in case of raw measurement is not applicable to dual-fuel engines. Instead the following provisions shall apply:

The measured test-averaged fuel consumption according to clause 4.3. of Chapter 11 of this Part shall be used as the base for calculating the test averaged CO₂ emissions.

The mass of each fuel consumed shall be used to determine, according to clause A.6.4. of Appendix 6 of this Chapter, the molar hydrogen ratio and the mass fractions of the fuel mix in the test.

The total fuel mass shall be determined according to equations 23 and 24:

$$m_{\text{fuel,corr}} = m_{\text{fuel}} - \left(m_{\text{THC}} + \frac{A_C + \alpha \times A_H}{M_{\text{CO}}} \times m_{\text{CO}} + \frac{W_{\text{GAM}} + W_{\text{DEL}} + W_{\text{EPS}}}{100} \times m_{\text{fuel}} \right) \quad (23)$$

$$m_{\text{CO}_2, \text{fuel}} = \frac{M_{\text{CO}_2}}{A_C + \alpha \times A_H} \times m_{\text{fuel,corr}} \quad (24)$$

Where:

$m_{\text{fuel,corr}}$	is the corrected fuel mass of both fuels, g/test
m_{fuel}	total fuel mass of both fuels, g/test
m_{THC}	mass of total hydrocarbon emissions in the exhaust gas, g/test
m_{CO}	mass of carbon monoxide emissions in the exhaust gas, g/test
$m_{\text{CO}_2, \text{fuel}}$	CO ₂ mass emission coming from the fuel, g/test
W_{GAM}	Sulphur content of the fuels, per cent mass
W_{DEL}	nitrogen content of the fuels, per cent mass
W_{EPS}	oxygen content of the fuels, per cent mass
α	molar hydrogen ratio of the fuels (H/C)
A_C	is the Atomic mass of Carbon: 12.011 g/mol
A_H	is the Atomic mass of Hydrogen: 1.0079 g/mol
M_{CO}	is the Molecular mass of Carbon monoxide: 28.011 g/mol
M_{CO_2}	is the Molecular mass of Carbon dioxide: 44.01 g/mol

The CO₂ emission resulting from urea shall be calculated with equation 25:

$$m_{\text{CO}_2, \text{urea}} = (c_{\text{urea}}/100) \times (m_{\text{CO}_2} / M_{\text{CO(NH}_2)_2}) \times m_{\text{urea}} \quad (25)$$

Where:

$m_{\text{CO}_2, \text{urea}}$	CO ₂ mass emission resulting from urea, g/test
c_{urea}	urea concentration, per cent
M_{urea}	total urea mass consumption, g/test
$M_{\text{CO(NH}_2)_2}$	is the Molecular mass of urea: 60.056 g/mol

Then the total CO₂ emission shall be calculated with equation 26:

$$m_{CO_2} = m_{CO_2, fuel} + m_{CO_2, urea} \quad (26)$$

The brake specific CO₂ emissions, e_{CO_2} shall then be calculated according to clause 3.3. of Chapter 11 of this Part.

11.0 DOCUMENTATION REQUIREMENTS

11.1. Documentation for installing in a vehicle a type approved HDDF engine

The manufacturer of a dual-fuel engine type-approved as separate technical unit shall include in the installation documents of its engine system the appropriate requirements that will ensure that the vehicle, when used on the road or elsewhere as appropriate, will comply with the requirements of this Chapter. This documentation shall include but is not limited to:

- (a) The detailed technical requirements, including the provisions ensuring the compatibility with the OBD system of the engine system;
- (b) The verification procedure to be completed.

The existence and the adequacy of such installation requirements may be checked during the approval process of the engine system.

- 11.1.1. In the case when the vehicle manufacturer who applies for approval of the installation of the engine system on the vehicle is the same manufacturer who received the type-approval of the dual-fuel engine as a separate technical unit, the documentation specified in clause 11.1 of this Chapter is not required.

12.0 APPENDICES

- Appendix 1 Types of HDDF engines and vehicles - illustration of the definitions and requirements
- Appendix 2 Activation and deactivation mechanisms of the counter(s), warning system, operability restriction, service mode in case of dual fuel engines and vehicles- Description and illustrations
- Appendix 3 HDDF dual-fuel indicator, warning system, operability restriction - Demonstration requirements
- Appendix 4 Additional emission test procedure requirements for dual-fuel engines
- Appendix 5 Additional PEMS emission test procedure requirements for dual-fuel engines
- Appendix 6 Determination of molar component ratios and u_{gas} values for dual-fuel engines

CHAPTER 14 - APPENDIX 1

TYPES OF HDDF ENGINES AND VEHICLES - ILLUSTRATION OF
THE DEFINITIONS AND MAIN REQUIREMENTS

	GER_{WHTC}^1	<i>Idle on diesel</i>	<i>Warm-up on diesel</i>	<i>Operation on diesel solely</i>	<i>Operation in absence of gas</i>	<i>Comments</i>
Type 1A	$GER_{WHTC} \geq 90 \%$	NOT Allowed	Allowed only on service mode	Allowed only on service mode	Service mode	
Type 1B	$GER_{WHTC} \geq 90 \%$	Allowed only on Diesel mode	Allowed only on diesel mode	Allowed only on diesel & service modes	Diesel mode	
Type 2A	$10 \% < GER_{WHTC} < 90 \%$	Allowed	Allowed only on service mode	Allowed only on service mode	Service mode	$GER_{WHTC} \geq 90 \%$ allowed
Type 2B	$10 \% < GER_{WHTC} < 90 \%$	Allowed	Allowed only on diesel mode	Allowed only on diesel & service modes	Diesel mode	$GER_{WHTC} \geq 90 \%$ allowed
Type 3A	NEITHER DEFINED NOR ALLOWED					
Type 3B	$GER_{WHTC} \leq 10 \%$	Allowed	Allowed only on diesel mode	Allowed only on diesel & service modes	Diesel mode	

¹ This average Gas Energy Ratio GER_{WHTC} is calculated over the hot part of the WHTC test-cycle

CHAPTER 14 - APPENDIX 2

**ACTIVATION AND DEACTIVATION MECHANISMS
OF THE COUNTER(S), WARNING SYSTEM,
OPERABILITY RESTRICTION, SERVICE MODE IN
CASE OF DUAL FUEL ENGINES AND VEHICLES-
DESCRIPTION AND ILLUSTRATIONS**

A.2.1. DESCRIPTION OF THE COUNTER MECHANISM**A.2.1.1. General**

A.2.1.1.1. To comply with the requirements of this Chapter, the system shall contain a counter to record the number of hours during which the engine has been operated while the system has detected a malfunctioning gas supply.

A.2.1.1.2. This counter shall be capable of counting up to 30 minutes operating time. The counter intervals shall be no longer than 3 minutes. When reaching its maximum value permitted by the system, it shall hold that value unless the conditions allowing the counter to be reset to zero are met.

A.2.1.2. Principle of the Counter Mechanism

A.2.1.2.1. The counters shall operate as follows:

A.2.1.2.1.1. If starting from zero, the counter shall begin counting as soon as a malfunctioning gas supply is detected according to clause 7.2 of this Chapter and the corresponding diagnostic trouble code (DTC) has the status confirmed and active.

A.2.1.2.1.2. The counter shall halt and hold its current value if a single monitoring event occurs and the malfunction that originally activated the counter is no longer detected or if the failure has been erased by a scan tool or a maintenance tool.

A.2.1.2.1.2.1. The counter shall also halt and hold its current value when the service mode becomes active.

A.2.1.2.1.3. Once frozen, the counter shall be reset to zero and restart counting if a malfunction relevant to that counter is detected and the service mode activated.

A.2.1.2.1.3.1. Once frozen, the counter shall also be reset to zero when the monitors relevant to that counter have run at least once to completion of their monitoring cycle without having detected a malfunction and no malfunction relevant to that counter has been detected during 36 engine operating hours since the counter was last held.

A.2.1.3. Illustration of the Counter Mechanism

Figures 1 to 3 of this Appendix give via three use-cases an illustration of the counter mechanism

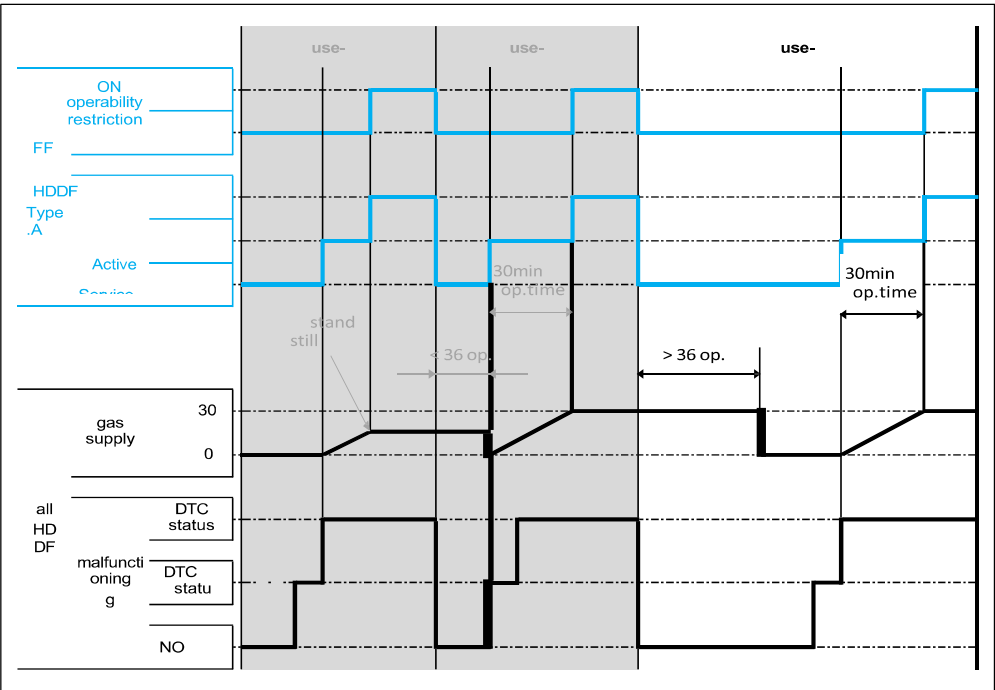


Figure 1
Illustration of the Gas Supply Counter Mechanism
(Type A HDDF) - Use-Case 1

A malfunction of the gas supply is detected for the very first time.

The service mode is activated and the counter starts counting once the DTC gets the "confirmed and active" status (2nd detection).

The vehicle encounters a stand-still situation before reaching 30 minutes operating time after the service mode is activated.

The service mode becomes active and the vehicle speed is limited to 20 km/h (see clause 4.2.2.1. of this Chapter). The counter freezes at its present value.

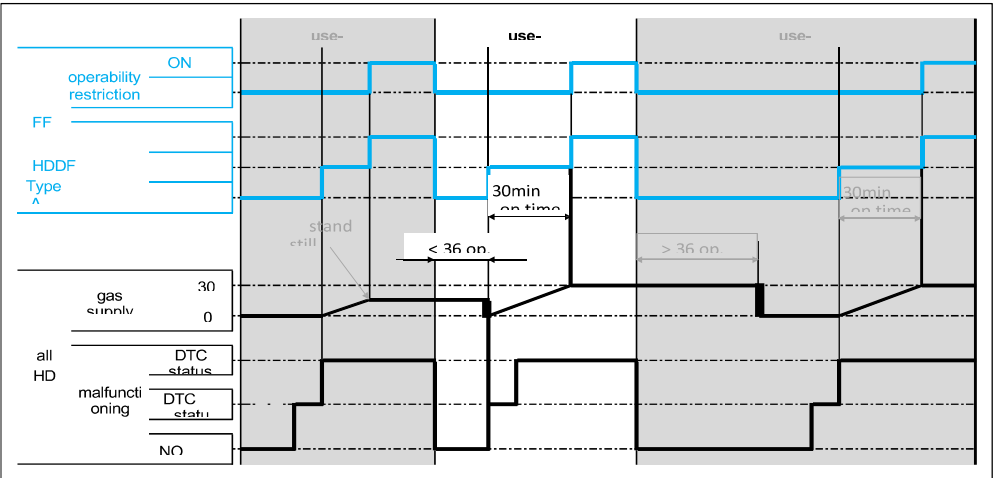


Figure 2
Illustration of the Gas Supply Counter Mechanism
(Type A HDDF) - Use-Case 2

A malfunction of the gas supply is detected while the gas supply malfunction counter is not at zero (in this use-case it indicates the value it reached in use-case 1 when the vehicle became standstill).

The service mode is activated and the counter restarts counting from zero as soon as the DTC gets the "potential" status (1st detection: see clause 4.2.3.2.1. of this Chapter).

After 30 minutes of operation without a standstill situation, the service mode becomes active and the vehicle speed is limited to 20 km/h (see clause 4.2.2.1 of this Chapter).

The counter freezes at a value of 30 minutes operating time.

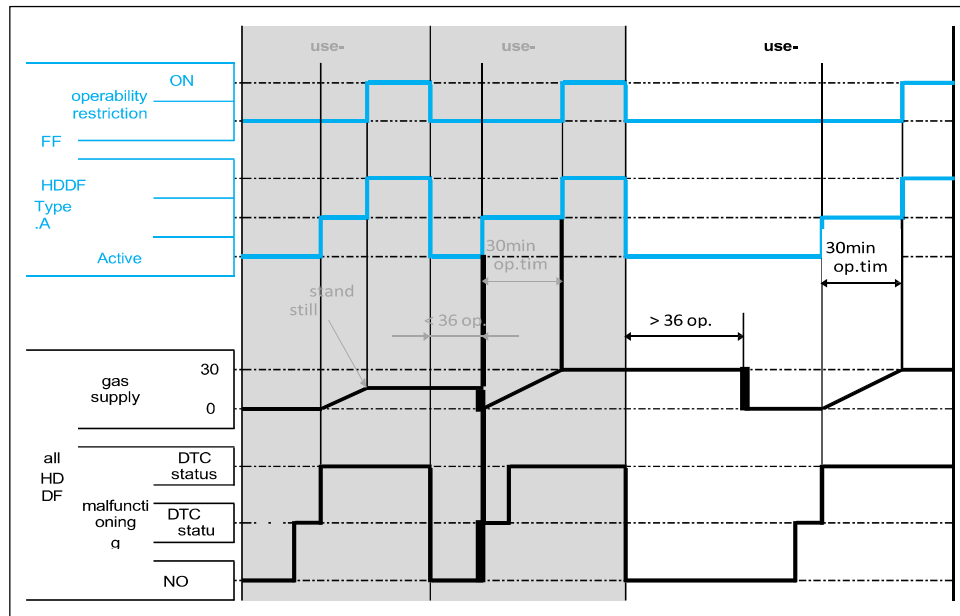


Figure 3
Illustration of the Gas Supply Counter Mechanism
(Type A HDDF) - Use-Case 3

After 36 operating hours without detection of a malfunction of the gas supply, the counter is reset to zero (see A.2.1.2.1.3.1 of this Appendix).

A malfunction of the gas supply is again detected while the gas supply malfunction counter is at zero (1st detection).

The service mode is activated and the counter starts counting once the DTC gets the "confirmed and active" status (2nd detection).

After 30 minutes of operation without a standstill situation, the service mode becomes active and the vehicle speed is limited to 20 km/h (see clause 4.2.2.1 of this Chapter).

The counter freezes at a value of 30 minutes operating time.

A.2.2. Illustration of the other activation and deactivation mechanisms

A.2.2.1. Empty gas tank

Figure 4 of this Appendix gives an illustration of the events occurring in the case of a HDDF vehicle when a gas tank becomes empty through one typical use-case.

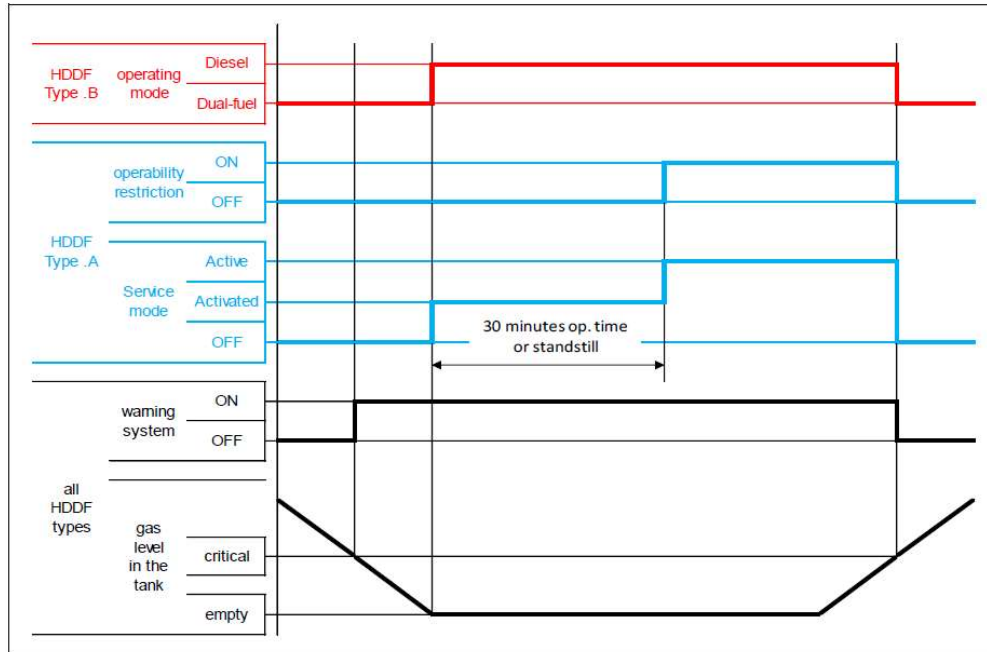


Figure 4
Illustration of the Events Occurring in case of an Empty Gas Tank
(Types A and B HDDF)

In that use case:

- (a) The warning system specified in clause 4.3.2. of this Chapter of becomes active when the level of gas reaches the critical level defined by the manufacturer;
- (b) The service mode is activated (in the case of a Type A HDDF) or the engine switches to Diesel mode (in the case of a Type B HDDF).

In the case of a Type A HDDF, the service mode becomes active and the vehicle speed is limited to 20 km/h after the next time the vehicle is stationary or after 30 minutes operating time without standstill (see clause 4.2.2.1. of this Chapter).

The gas tank is refilled.

The vehicle operates again in dual-fuel mode as soon as the tank is refilled above the critical level.

A.2.2.2 MALFUNCTIONING GAS SUPPLY

Figure 5 of this Appendix gives via one typical use-case an illustration of the events occurring in the case of a malfunction of the gas supply system. This illustration should be understood as complementary to that given in clause A.2.1 and dealing with the counter mechanism.

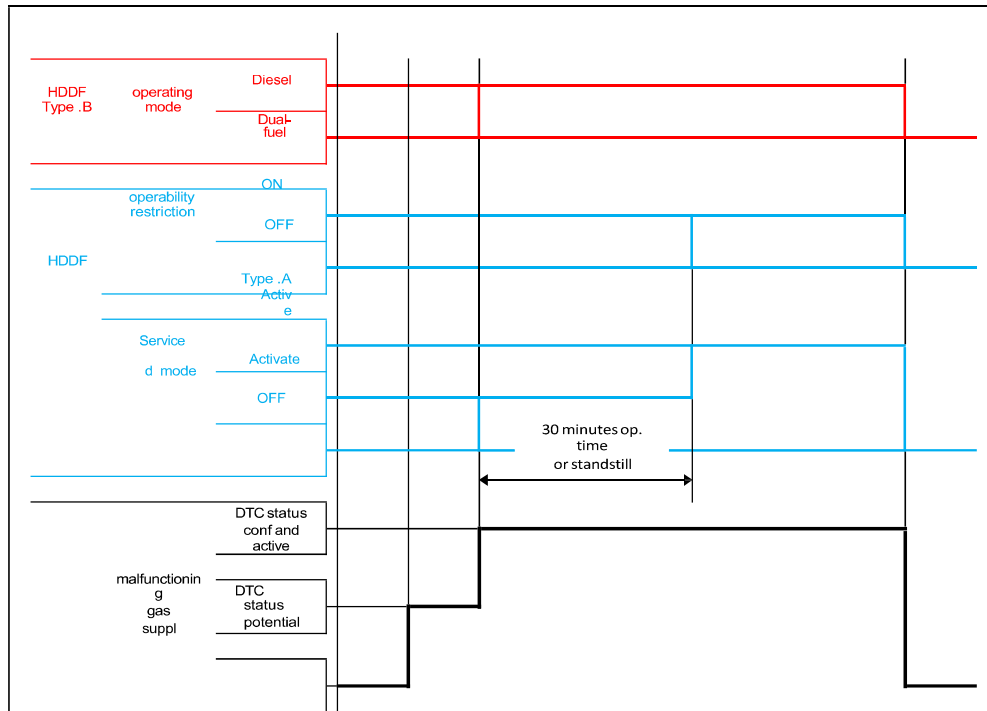


Figure 5
Illustration of the Events Occurring in case of a Malfunctioning Gas Supply System (Types A And B HDDF)

In that use case:

- (a) The failure of the gas supply system occurs for the very first time. The DTC gets the potential status (1st detection);
- (b) The service mode is activated (in the case of a Type A HDDF) or the engine switches to Diesel mode (in the case of a Type B HDDF) as soon as the DTC gets the “confirmed and active” status (2nd detection).

In the case of a Type A HDDF, the service mode becomes active and the vehicle speed is limited to 20 km/h after the next time the vehicle is stationary or after 30 minutes operating time without standstill (see clause 4.2.2.1 of this Chapter).

The vehicle operates again in dual-fuel mode as soon as the failure is repaired.

A.2.2.3. **Abnormality of the Gas Consumption**

Figure 6 of this Appendix gives via one typical use-case an illustration of the events occurring in the case of an abnormality of the gas consumption.

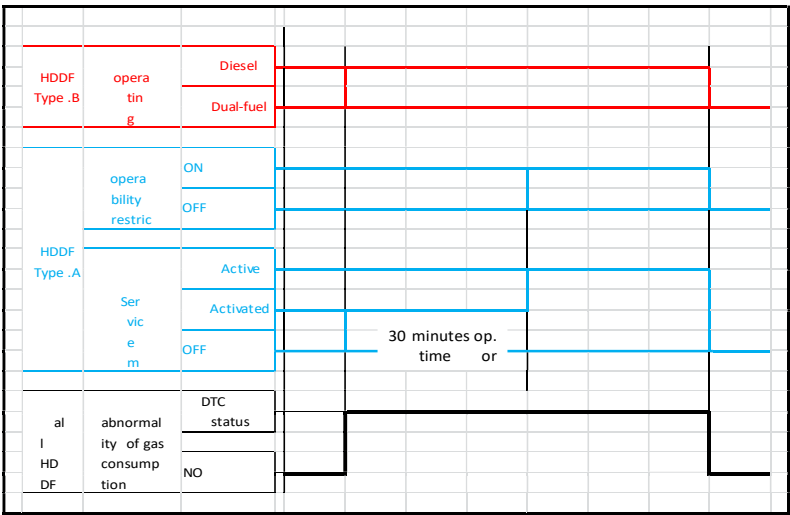


Figure 6
Illustration of the Events Occurring in case of Abnormality of Gas Consumption (Type A And Type B HDDF)

In that use case the service mode is activated (in the case of a Type A HDDF) or the engine switches to Diesel mode (in the case of a Type B HDDF) as soon as the DTC gets the "potential" status (1st detection).

In the case of a Type A HDDF, the service mode becomes active and the vehicle speed is limited to 20 km/h after the next time the vehicle is stationary or after 30 minutes operating time without standstill (see clause 4.2.2.1. of this Chapter).

The vehicle operates again in dual-fuel mode as soon as the abnormality is rectified.

CHAPTER 14 - APPENDIX 3

**HDDF DUAL-FUEL INDICATOR, WARNING SYSTEM,
OPERABILITY RESTRICTION - DEMONSTRATION
REQUIREMENTS**

A.3.1. DUAL-FUEL INDICATORS**A.3.1.1. Dual-Fuel Mode Indicator**

In the case where a dual-fuel engine is type approved as a separate technical unit, the ability of the engine system to command the activation of the dual-fuel mode indicator when operating in dual-fuel mode shall be demonstrated at type-approval.

In the case where a dual-fuel vehicle is type approved as regards to its emissions, the activation of the dual-fuel mode indicator when operating in dual-fuel mode shall be demonstrated at type-approval.

Note: Installation requirements related to the dual-fuel mode indicator of an approved dual-fuel engine are specified in clause 6.2. of this Chapter.

A.3.1.2. Diesel Mode Indicator

In the case where a dual-fuel engine of Type 1B, Type 2B, or Type 3B is type approved as a separate technical unit, the ability of the engine system to command the activation of the diesel mode indicator when operating in diesel mode shall be demonstrated at type-approval.

In the case where a dual-fuel vehicle of Type 1B, Type 2B, or Type 3B is type approved as regards to its emissions, the activation of the diesel mode indicator when operating in diesel mode shall be demonstrated at type-approval.

Note: Installation requirements related to the diesel mode indicator of an approved Type 1B, Type 2B, or Type 3B dual-fuel engine are specified in clause 6.2. of this Chapter.

A.3.1.3. Service Mode Indicator

In the case where a dual-fuel engine is type approved as a separate technical unit, the ability of the engine system to command the activation of the service mode indicator when operating in service mode shall be demonstrated at type-approval.

In the case where a dual-fuel vehicle is type approved with regard to its emissions, the activation of the service mode indicator when operating in service mode shall be demonstrated at type-approval.

Note: Installation requirements related to the service mode indicator of an approved dual-fuel engine are specified in clause 6.2. of this Chapter.

- A.3.1.3.1** When so-equipped it is sufficient to perform the demonstration related to the service mode indicator by activating a service mode activation switch and to present the Test Agency with evidence showing that the activation occurs when the service mode is commanded by the engine system itself (for example, through algorithms, simulations, result of in-house tests, etc).

A.3.2. WARNING SYSTEM

In the case where a dual-fuel engine is type approved as a separate technical unit, the ability of the engine system to command the activation of the warning system in the case that the amount of gas in the tank is below the warning level, shall be demonstrated at type-approval.

In the case where a dual-fuel vehicle is type-approved as regards to its emissions the activation of the warning system in the case that the amount of gas in the tank is below the warning level, shall be demonstrated at type- approval. For that purpose, at the request of the manufacturer and with the approval of the Test Agency, the actual amount of gas may be simulated.

Note: Installation requirements related to the warning system of an approved dual-fuel engine are specified in clause 6.2. of this Chapter.

A.3.3. OPERABILITY RESTRICTION

In the case where a Type 1A or Type 2A dual-fuel engine is type approved as a separate technical unit, the ability of the engine system to command the activation of the operability restriction upon detection of an empty gaseous fuel tank, of a malfunctioning gas supply system, and of an abnormality of gas consumption in dual-fuel mode shall be demonstrated at type-approval.

In the case where a Type 1A or Type 2A dual-fuel vehicle is type approved as regards to its emissions, the activation of the operability restriction upon detection of an empty gaseous fuel tank, of a malfunctioning gas supply system, and of an abnormality of gas consumption in dual-fuel mode shall be demonstrated at type-approval.

Note: Installation requirements related to the operability restriction of an approved dual-fuel engine are specified in clause 6.2. of this Chapter

- A.3.3.1. The malfunctioning of the gas supply and the abnormality of gas consumption may be simulated at the request of the manufacturer and with the approval of the Test Agency.

In the case where a Type 1A or Type 2A dual-fuel engine is type approved as a separate technical unit, the ability of the engine system to command the activation of the operability restriction upon detection of an empty gaseous fuel tank, of a malfunctioning gas supply system, and of an abnormality of gas consumption in dual-fuel shall be demonstrated at type-approval.

In the case where a Type 1A or Type 2A dual-fuel vehicle is type approved as regards to its emissions, the activation of the operability restriction upon detection of an empty gaseous fuel tank, of a malfunctioning gas supply system, and of an abnormality of gas consumption in dual-fuel mode shall be demonstrated at type-approval.

Note: Installation requirements related to the operability restriction of an approved dual-fuel engine are specified in clause 6.2. of this Chapter.

- A.3.3.1. The malfunctioning of the gas supply and the abnormality of gas consumption may be simulated at the request of the manufacturer and with the approval of the Test Agency
- A.3.3.2. It is sufficient to perform the demonstration in a typical use-case selected with the agreement of the Test Agency and to present that Test Agency with evidence showing that the operability restriction occurs in the other possible use- cases (for example, through algorithms, simulations, result of in-house tests, etc.

CHAPTER 14 - APPENDIX 4**ADDITIONAL EMISSION TEST PROCEDURE
REQUIREMENTS FOR DUAL- FUEL ENGINES****A.4.1. GENERAL**

This Appendix defines the additional requirements and exceptions to Chapter 3 of this Part to enable emission testing of dual-fuel engines independent whether these emissions are solely exhaust emissions or also crankcase emissions added to the exhaust emissions according to clause 6.10. of Chapter 3 of this Part.

Emission testing of a dual-fuel engine is complicated by the fact that the fuel used by the engine can vary between pure diesel fuel and a combination of mainly gaseous fuel with only a small amount of diesel fuel as an ignition source. The ratio between the fuels used by a dual-fuel engine can also change dynamically depending of the operating condition of the engine. As a result special precautions and restrictions are necessary to enable emission testing of these engines.

A.4.2. TEST CONDITIONS (CHAPTER 3 OF THIS PART)**A.4.2.1. Laboratory test conditions (Chapter 3 of this Part)**

The parameter f_a for dual-fuel engines shall be determined with formula (a)(2) in clause 6.1. of Chapter 3 of this Part.

A.4.3. TEST PROCEDURES (CHAPTER 3, CLAUSE 7.)**A.4.3.1. Measurement procedures (Chapter 3, clause 7.1.3.)**

The recommended measurement procedure for dual-fuel engines is procedure (b) listed in clause 7.1.3. of Chapter 3 of this Part (CVS system).

This measurement procedure ensures that the variation of the fuel composition during the test will only influence the hydrocarbon measurement results. This shall be compensated via one of the methods described in clause A 4.4.

Other measurement methods such as method (a) listed in clause 7.1.3. of Chapter 3 of this Part (raw gaseous/partial flow measurement) can be used with some precautions regarding exhaust mass flow determination and calculation methods. Fixed values for fuel parameters and u_{gas} -values shall be applied as described in Appendix 6 of this Chapter.

A.4.4. EMISSION CALCULATION (CHAPTER 3, CLAUSE 8.)

The emissions calculation on a molar basis, in accordance with Annex 7 of GTR No. 11 concerning the exhaust emission test protocol for Non-Road Mobile Machinery (NRMM), is not permitted.

A.4.4.1. Dry/Wet Correction (Chapter 3, Clause 8.1.)**A.4.4.1.1. Raw exhaust gas (Chapter 3, clause 8.1.1.)**

Equations 15 and 17 in Chapter 3, clause 8.1.1. shall be used to calculate the dry/wet correction.

The fuel specific parameters shall be determined according to clauses A.6.2. and A.6.3. of Appendix 6 of this Chapter.

A.4.4.1.2. Diluted exhaust gas (Chapter 3, clause 8.1.2)

Equations 19 and 20 in Chapter 3, clause 8.1.2. shall be used to calculate the wet/dry correction.

The molar hydrogen ratio α of the combination of the two fuels shall be used for the dry/wet correction. This molar hydrogen ratio shall be calculated from the fuel consumption measurement values of both fuels according to clause A.6.4. of Appendix 6 of this Chapter.

A.4.4.2. NOx correction for humidity (Chapter 3, clause 8.2.)

The NOx humidity correction for compression ignition engines as specified in clause 8.2.1. of Chapter 3 of this Part shall be used to determine the NOx humidity correction for dual-fuel engines.

$$k_{h,D} = (15.698 \times H_a) / 1000 + 0.832$$

where:

H_a is the intake air humidity, g water per kg dry air

A.4.4.3. Partial flow dilution (PFS) and raw gaseous measurement (Chapter 3, clause 8.4.)**A.4.4.3.1. Determination of exhaust gas mass flow (Chapter 3, clause 8.4.1.)**

The exhaust mass flow shall be determined according to the direct measurement method as described in clause 8.4.1.3.

Alternatively, the airflow and air to fuel ratio measurement method according to clause 8.4.1.6. (Equations 30, 31 and 32) may be used only if α , γ , δ and ε values are determined according to clauses A.6.2. and A.6.3. of Appendix 6 of this Chapter. The use of a zirconia-type sensor to determine the air fuel ratio is not allowed.

A.4.4.3.2. Determination of the gaseous components (Chapter 3, clause 8.4.2.)

The calculations shall be performed according to Chapter 3, clause 8. but the u_{gas} -values and molar ratios as described in clause A.6.2. and A.6.3. of Appendix 6 of this Chapter shall be used

A.4.4.3.3. Particulate determination (Chapter 3, clause 8.4.3.)

For the determination of particulate emissions with the partial dilution measurement method the calculation shall be performed according to Chapter 3, clause 8.4.3.2.

For controlling the dilution ratio one of the following two methods may be used:

- The direct mass flow measurement as described in clause 8.4.1.3.
- The airflow and air to fuel ratio measurement method according to clause 8.4.1.6. (equations 30, 31 and 32) may only be used when this is combined with the look ahead method described in clause 8.4.1.2. and if α , γ , δ and ε values are determined according to clause A.6.2. and A.6.3. of Appendix 6 this Chapter.

The quality check according to clause 9.4.6.1 of Chapter 3 of this Part shall be performed for each measurement

A.4.4.3.4. Additional requirements regarding the exhaust gas mass flow meter

The flow meter referred to in clause A.4.4.3.1. and A.4.4.3.3. shall not be sensitive to the changes in exhaust gas composition and density. The small errors of e.g. pitot tube or orifice-type of measurement (equivalent with the square root of the exhaust density) may be neglected.

A.4.4.4. Full Flow Dilution Measurement (CVS) (Chapter 3, clause 8.5.)

The possible variation of the fuel composition will only influence the hydrocarbons measurement results calculation. For all other components the appropriate equations from clause 8.5.2. of Chapter 3 of this Part shall be used.

The exact equations shall be applied for the calculation of the hydrocarbon emissions using the molar component ratios determined from the fuel consumption measurements of both fuels according to clause A.6.4. of Appendix 6 of this Chapter.

A.4.4.4.1. Determination of The Background Corrected Concentrations

(Chapter 3, clause 8.5.2.3.2)

To determine the stoichiometric factor, the molar hydrogen ratio α of the fuel shall be calculated as the average molar hydrogen ratio of the fuel mix during the test according to clause A.6.4. of Appendix 6 of this Chapter.

Alternatively the F_s value of the gaseous fuel may be used in equation 59 or 60 of Chapter 3 of this Part

**A.4.5. EQUIPMENT SPECIFICATION AND VERIFICATION
(CHAPTER 3, CLAUSE 9.)**

A.4.5.1. Oxygen Interference Check Gases (Chapter 3, clause 9.3.3.4.)

The oxygen concentrations required for dual-fuel engines are equal to those required for compression ignition engines listed in Table 8 in clause 9.3.3.4. of Chapter 3 of this Part.

A.4.5.2. Oxygen Interference Check (Chapter 3, clause 9.3.7.3.)

Instruments used to measure dual-fuel engines shall be checked using the same procedures as those used to measure compression ignition engines. The 21 per cent oxygen blend shall be used under item (b) in clause 9.3.7.3. of Chapter 3 of this Part.

A.4.5.3. Water Quench Check (Chapter 3, clause 9.3.9.2.2.)

The water quench checks in clause 9.3.9.2.2. of Chapter 3 to this Part applies to wet NO_x concentration measurements only. For dual-fuel engines fuelled with natural gas this check should be performed with an assumed H/C ratio of 4 (Methane). In that case $H_m = 2 \times A$. For dual-fuel engines fuelled with LPG this check should be performed with an assumed H/C ratio of 2.525. In that case $H_m = 1.25 \times A$

CHAPTER NO 14 - APPENDIX 5

**ADDITIONAL PEMS EMISSION TEST PROCEDURE
REQUIRMENTS FOR DUAL-FUEL ENGINES**

A 5.1 GENREAL

This Appendix defines the additional requirements and exceptions to Chapter 7 of this Part to enable PEMS emission testing of dual-fuel engines.

Emission testing of a dual-fuel engine is complicated by the fact that the fuel used by the engine can vary between pure diesel fuel and a combination of mainly gaseous fuel with only a small amount of diesel fuel as an ignition source. The ratio between the fuels used by a dual-fuel engine can also change dynamically depending of the operating condition of the engine. As a result, special precautions and restrictions are necessary to enable emission testing of these engines.

A.5.2. The following amendments to Appendix 1 of Chapter 7 of this Part shall apply:**A.5.2.1. Note (2) of Table 1 in clause A.1.2.2. shall read:**

(2) Only for engines fuelled with natural gas

A.5.2.2. Clause A.1.3.3. "Dry-Wet correction" shall read:

If the concentration is measured on a dry basis, it shall be converted to a wet basis according to clause 8.1. of Chapter 3 of this Part and clause A.4.4.1 of Appendix 4 of Chapter 14 of this Part.

A.5.2.3. Clause A.1.3.5. "Calculation of the instantaneous gaseous emissions" shall read:

The mass emissions shall be determined as described in clause 8.4.2.3. of Chapter 3 of this Part.

The u_{gas} values shall be determined according to clause A.6.2. and A.6.3. of Appendix 6 of Chapter 14 of this Part.

CHAPTER NO 14 - APPENDIX 6

**DETERMINATION OF MOLAR COMPONENT RATIOS
AND U_{GAS} VALUES FOR DUAL-FUEL ENGINES**

A.6.1. GENERAL

This Appendix defines the determination of molar component ratios and u_{gas} values for the dry-wet factor and emissions calculations for emission testing of dual-fuel engines.

A.6.2. OPERATION IN DUAL-FUEL MODE

A.6.2.1. For Type 1A or 1B dual-fuel engines operating in dual-fuel mode the molar component ratios and the u_{gas} values of the gaseous fuel shall be used.

A.6.2.2. For Type 2A or 2B dual-fuel engines operating in dual-fuel mode the molar component ratios and the u_{gas} values from Tables 1 and 2 below shall be used.

Table 1

**Molar Component Ratios for a Mixture of 50% Gaseous Fuel
and 50% Diesel Fuel (Mass %)**

Gaseous Fuel	α	γ	δ	ε
CH ₄	2.8681	0	0	0.0040
G _R	2.7676	0	0	0.0040
G ₂₃	2.7986	0	0.0703	0.0043
G ₂₅	2.7377	0	0.1319	0.0045
Propane	2.2633	0	0	0.0039
Butane	2.1837	0	0	0.0038
LPG	2.1957	0	0	0.0038
LPG Fuel A	2.1740	0	0	0.0038
LPG Fuel B	2.2402	0	0	0.0039

Table 2

**Raw Exhaust Gas Ugas Values and Component Densities for
a Mixture of 50% Gaseous Fuel and 50% Diesel Fuel (Mass %)**

Gaseous Fuel	ρ_e	Gas					
		NO _x	CO	HC	CO ₂	O ₂	CH ₄
		ρ_{gas} [kg/m ³]					
		2.053	1.250	a)	1.9636	1.4277	0.716
		u_{gas} ^{b)}					
CNG/LNG ^{c)}	1.2786	0.001606	0.000978	0.000528 ^{d)}	0.001536	0.001117	0.000560
Propane	1.2869	0.001596	0.000972	0.000510	0.001527	0.001110	0.000556
Butane	1.2883	0.001594	0.000971	0.000503	0.001525	0.001109	0.000556
LPG ^{e)}	1.2881	0.001594	0.000971	0.000506	0.001525	0.001109	0.000556
a) depending on fuel b) at $\lambda = 2$, dry air, 273 K, 101.3 kPa c) u accurate within 0.2 % for mass composition of: C = 58 - 76 %; H = 19 - 25 %; N = 0 - 14 % (CH ₄ , G ₂₀ , G _R , G ₂₃ and G ₂₅) d) NMHC on the basis of CH _{2.93} (for total HC the u_{gas} coefficient of CH ₄ shall be used) e) u accurate within 0.2 % for mass composition of: C3 = 27 - 90 %; C4 = 10 - 73 % (LPG Fuels A and B)							

A.6.2.3. For Type 3B dual-fuel engines operating in dual-fuel mode the molar component ratios and the u_{gas} values of diesel fuel shall be used.

A.6.2.4. For the calculation of the hydrocarbon emissions of all types of dual-fuel engines operating in dual-fuel mode, the following shall apply:

- For the calculation of the THC emissions, the u_{gas} value of the gaseous fuel shall be used.
- For the calculation of the NMHC emissions, the u_{gas} value on the basis of CH_{2.93} shall be used.
- For the calculation of the CH₄ emissions, the u_{gas} value of CH₄ shall be used.

A.6.3. OPERATION IN DIESEL MODE

For Type 1B, 2B or 3B dual-fuel engines operating in diesel mode, the molar component ratios and the u_{gas} values of diesel fuel shall be used.

A.6.4. DETERMINATION OF THE MOLAR COMPONENT RATIOS WHEN THE FUEL MIX IS KNOWN

A.6.4.1 Calculation of the Fuel Mixture Components

$$w_{ALF} = \frac{w_{ALF1} \times q_{mf1} + w_{ALF2} \times q_{mf2}}{q_{mf1} + q_{mf2}} \quad (A6.1)$$

$$w_{BET} = \frac{w_{BET1} \times q_{mf1} + w_{BET2} \times q_{mf2}}{q_{mf1} + q_{mf2}} \quad (A6.2)$$

$$w_{GAM} = \frac{w_{GAM1} \times q_{mf1} + w_{GAM2} \times q_{mf2}}{q_{mf1} + q_{mf2}} \quad (A6.3)$$

$$w_{DEL} = \frac{w_{DEL1} \times q_{mf1} + w_{DEL2} \times q_{mf2}}{q_{mf1} + q_{mf2}} \quad (A6.4)$$

$$w_{EPS} = \frac{w_{EPS1} \times q_{mf1} + w_{EPS2} \times q_{mf2}}{q_{mf1} + q_{mf2}} \quad (A6.5)$$

where:

q_{mf1} fuel mass flow rate of fuel1, kg/s

q_{mf2} fuel mass flow rate of fuel2, kg/s

w_{ALF} hydrogen content of fuel, per cent mass

w_{BET} carbon content of fuel, per cent mass

w_{GAM} sulphur content of fuel, per cent mass

w_{DEL} nitrogen content of fuel, per cent mass

w_{EPS} oxygen content of fuel, per cent mass

A 6.4.2 Calculation of the molar ratios of H, C, S, N and O related to C for the fuel mixture (according to ISO 8178-1, Annex A-A2.2.2)

$$\alpha = 11.9164 \times (W_{ALF} \div W_{BET}) \quad (A6.6)$$

$$\gamma = 0.37464 \times \frac{W_{GAM}}{W_{BET}} \quad (A6.7)$$

$$\delta = 0.85752 \times \frac{W_{DEL}}{W_{BET}} \quad (A6.8)$$

$$\varepsilon = 0.75072 \times \frac{W_{EPS}}{W_{BET}} \quad (A6.9)$$

Where:

W_{ALF}	hydrogen content of fuel, per cent mass
W_{BET}	carbon content of fuel, per cent mass
W_{GAM}	sulphur content of fuel, per cent mass
W_{DEL}	nitrogen content of fuel, per cent mass
W_{EPS}	oxygen content of fuel, per cent mass
α	molar hydrogen ratio (H/C)
γ	molar sulphur ratio (S/C)
δ	molar nitrogen ratio (N/C)
ε	molar oxygen ratio (O/C)

A 6.4.3 Calculation of the u_{gas} values for a fuel mixture

The raw exhaust gas u_{gas} values for a fuel mixture can be calculated with the exact equations in clause 8.4.2.4. of Chapter 3 of this Part and the molar ratios calculated according to clause A.6.4.2.

For systems with constant mass flow, equation 57 in clause 8.5.2.3.1. of Chapter 3 of this Part is needed to calculate the diluted exhaust gas u_{gas} values.

ANNEXURE 1

(See Introduction)

**COMPOSITION OF A COMMITTEE FOR FORMULATION OF THIS STANDARD
AS PER MORTH OFFICE MEMORANDUM NO. RT-11035/31/2015-MVL DATED 6th OCTOBER, 2015**

Chairperson	
Capt. (Dr.) Rajendra B. Saner Patil Director	Central Institute of Road Transport (CIRT), Pune
Co-ordinator and Member Secretary	
Representative from	Central Institute of Road Transport (CIRT), Pune
Members	Representing
Representative from	The Automotive Research Association of India (ARAI), Pune
Representative from	International Centre for Automotive Technology (ICAT), Manesar, Gurgaon
Representative from	Society of Indian Automobile Manufacturers (SIAM), New Delhi
Representative from	Ministry of Petroleum & Natural Gas (MoPNG), New Delhi
Representative from	Emission Control Manufacturers Association (ECMA), New Delhi
Representative from	Automotive Components Manufacturers Association of India (ACMA), New Delhi
Representative from	Vehicles Research and Development Establishment (VRDE), Ahmednagar
Representative from	Indian Institute of Petroleum (IIP), Dehra Dun
Representative from	Ministry of Road Transport and Highways (MoRTH), New Delhi

ANNEXURE 2
(See Introduction)

COMMITTEE COMPOSITION*
Automotive Industry Standards Committee

Chairperson	
Mrs. Rashmi Urdhwareshe	Director The Automotive Research Association of India, Pune
Members	Representing
Representative from	Ministry of Road Transport and Highways (Dept. of Road Transport and Highways), New Delhi
Representative from	Ministry of Heavy Industries and Public Enterprises (Department of Heavy Industry), New Delhi
Shri S. M. Ahuja	Office of the Development Commissioner, MSME, Ministry of Micro, Small and Medium Enterprises, New Delhi
Shri Shrikant R. Marathe	Former Chairman, AISC
Shri R.R. Singh	Bureau of Indian Standards, New Delhi
Director	Central Institute of Road Transport, Pune
Director	Global Automotive Research Centre
Director	International Centre for Automotive Technology, Manesar
Director	Indian Institute of Petroleum, Dehra Dun
Director	Vehicles Research and Development Establishment, Ahmednagar
Director	Indian Rubber Manufacturers Research Association
Representatives from	Society of Indian Automobile Manufacturers
Shri R. P. Vasudevan	Tractor Manufacturers Association, New Delhi
Shri Uday Harite	Automotive Components Manufacturers Association of India, New Delhi

Member Secretary
Shri Vikram Tandon
Dy. General Manager
The Automotive Research Association of India, Pune

* At the time of approval of this Automotive Industry Standard (AIS)